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ESTIMATION OF CAVING VOLUMETRIC- FLOW USING THE ULTRASONIC DOPPLER METHOD

■ ESTIMACIÓN DEL FLUJO VOLUMÉTRICO DE RECORTES Y DERRUMBES DE PERFORACIÓN (CAVINGS) A PARTIR DE LA APLICACIÓN DEL EFECTO DOPPLER

Ramirez-Silva, Luis-Fernando^a; Carvajal-Jiménez, Jenny-Mabel^{b*}; Ramirez, Ana B.^a

ABSTRACT

Estimating the volumetric flow of cuttings and cavings that are extracted and transported by the drilling mud into the flow line while drilling a well is of major interest to for drillers so that they can understand the drilling conditions and maintain the wellbore stability. In this paper, a new method to estimate the volumetric flow of cavings via the Doppler effect is proposed. The proposed method is a non-invasive method that uses two piezo-electric acoustic sensors located on the flow line, one acting as an emitter and the other acting as a receiver. The system device estimates cavings and cuttings by measuring the mud and solids flow on a real-time basis. Results obtained at a laboratory experimental level reflected a maximum volumetric-flow error of 10.5% for small-sized cavings and 34,7% for large-sized cavings. According to those results, the method may be suitable for estimating caving volumetric-flow with acoustical techniques at the flow line while drilling and it might be used as a real-time operation method to evaluate wellbore stability.

RESUMEN

La estimación del flujo volumétrico de recortes y derrumbes de perforación (cavings) que son extraídos y transportados por el lodo de perforación a través de las líneas de flujo hacia la superficie durante la perforación de un pozo petrolero, es de interés para los perforadores ya que permite entender las condiciones de perforación que son requeridas para mantener la estabilidad del pozo perforado. En este artículo se presenta un nuevo método para estimar el flujo volumétrico de cavings y cuttings o ripios de perforación a partir de la aplicación del Efecto Doppler; el método propuesto es una técnica no invasiva que utiliza dos sensores piezo-eléctricos acústicos de ultrasonido ubicados en la línea de flujo del pozo conocida como flow line; uno de los sensores actúa como emisor y el otro es un receptor de la señal acústica; los resultados obtenidos en las pruebas de laboratorio evidenciaron un error máximo de 10.5% para los cavings de tamaño pequeño y de 34.7% para los cavings de tamaño grande. De acuerdo con estos resultados, el método puede ser aplicado a nivel industrial para estimación del flujo volumétrico de cavings con el objeto de evaluar la estabilidad del pozo perforado en tiempo real.

KEYWORDS / PALABRAS CLAVE

Geomechanics | Acoustics | Flow line | Drilling | Wellbore Wellbore stability.

Geomecánica | Acústica | Línea de Flujo de perforación Perforación | Pozo | Estabilidad de la perforación.

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1. INTRODUCTION

While drilling, the bit cuts the rock from the subsurface and drilling mud transports those drill cuts (called cuttings) from the bottom to the surface. The size of a cutting varies from a few microns to a few millimeters (usually less than 5). Usually, if the borehole starts to fail, it produces cavings and those cavings are rock masses that are larger than 5 mm and can be as big as 30 cm in length (with a mass of more than 2kg). Due to the size and amount of cavings produced, the drilled well might be lost and it can result in a great deal of unexpected expenditure, time and other resources for the drilling company. Due to these reasons, cavings and cuttings must be measured during the drilling process in order to prevent wellbore instability, keep drilling operations under control and maintain costs within the operating window.

Geomechanics experts use information regarding the amount of rock per time-unit to establish the wellbore stability [1]. In particular, an estimate of the caving volumetric-flow in bbl/min (barrels per minute) indicates the stability status of the wellbore. A high level of volumetric flow can indicate instability in the hole, and corrective actions should be taken before an accident occurs [2].

Traditional methods used to estimate cavings flow use a manual technique in which people take samples at the shaker during a time interval and compute cavings and cuttings flow using theoretical data on wellbore geometry and measured weights of samples. In recent years in Colombia, a mechanical instrument known as MAC (*Medidor Automático de Cavings*, as it is called in Spanish) is used to measure the amount of rock that is extracted from a wellbore in a typical well-drilling process [3]. The MAC has a reception device where the rocks are collected after the mud is filtered, and it collects such rocks during a time lapse and measures the weight of the rocks collected. Afterwards, a gate is opened, so that the rock is released, and the weighing process starts again. This system measures the weight of the rock transported by the drilling mud, but this method is not exact because the rock is impregnated with drilling mud. Some rock mass can be lost between two consecutive measurements and part of the drilling mud stays in the measurement equipment, thus altering the weight of rock mass to be measured. **Figure 1** shows the MAC instrument installed in a wellbore while drilling operations are performed.

The measurement of the volumetric flow of cuttings and cavings obtained with the MAC instrument has delivered good results when compared with the measurements of the size and shape of a borehole, registered by the caliper log. However, the maintenance of the instrument is particularly laborious because the drilling mud attaches to the gate, thus not allowing the container to be opened to release the rock. Additionally, different types of shakers require different adaptations of this instrument, so that it fits precisely for each type of shaker.

The proposed system is a non-invasive method that measures caving and cutting volumetric-flow in such a way that maintenance issues and the design restrictions of the MAC instrument can be avoided. The proposed measurement mechanism uses a piezo-electric transducer configuration in the flow line, such that the amount of rock per minute (in terms of cubic meters per time unit) can be estimated using the Doppler effect. The Doppler effect states that if an object emitting an acoustic source is moving, then an observer perceives changes of the wave frequency of the source due to its relative velocity with respect to the emitter [4]. This phenomenon makes it possible to estimate the velocity of the mud and particles of rock that are passing through a cross-section of the pipeline. Knowing the velocity of propagation of the mud and particles, we can generate a model that relates the frequency change with the volumetric flow of rocks. This model is different for different sizes of rock transported inside the mud in the pipeline. Thus, a geomechanics expert can use this model to determine the amount of rock (per time unit) that is being transported, and identify whether there is a risk of the wellbore collapsing.



Figure 1. MAC Operation while drilling. Example of a MAC installed at the shaker. The container collects rocks before opening a gate to release them, and start a new time lapse for rock collection. Afterwards, the volume of rock is calculated using density and weight of the samples collected, and volumetric flow corresponds to this volume per time unit.

In order to experimentally test the proposed strategy for volumetric-flow estimation, an experimental system that emulates the rock transport by the drilling mud through the flow line was built, and two different sizes of rock were tested. The frequency shift observed in the acoustic sensors for different quantities of rock was measured in the experiments, to thus obtain a model of frequency change as a function of the volumetric flow of rock. This model was validated using additional experiments in which a known amount of rock was inserted into the flow line and the volumetric flow was measured and compared with the values given by the model.

2. THEORETICAL FRAME

The theory behind the proposed method for measuring volumetric flow of rock through the flow line is the acoustic-wave propagation phenomena, in which the acoustic wave is propagating through a medium that contains solids traveling at a certain velocity. Acoustic signals have been widely used in many applications to estimate flow [5], for instance, in the estimation of fluids-flow velocity in industrial pipelines [6]-[8], or to understand the blood flow in veins and arteries in medical applications [9] and [10]. A traditional method used for the estimation of the volumetric flow is the Doppler effect. In addition to the Doppler effect, other techniques (such as those based on the arrival time of the acoustic signals, or the cross-correlation between emitted and received signals) can also be used for volumetric flow estimation.

DOPPLER EFFECT

The Doppler effect states that a particle (source), which is moving through a specific medium, produces a frequency change for an observer who is moving with a relative velocity with respect to the emitter. Thus, determining the change in frequency makes it possible to establish the relative velocity between emitter and observer.

Assume that a particle E with a specific speed v is moving towards an observer R_1 , and away of an observer R_2 (See Figure 2-left). The moving particle E (or source) emits a continuous pressure signal, which travels with a speed c , depending on the medium. The observer R_1 detects a pressure signal having a frequency that is larger than the one detected by the observer R_2 [11]. This phenomenon is known as Doppler effect and it is given by

$$f_d = f_o - f_e = -\frac{v}{c} f_e \quad (1)$$

Where f_o is the frequency of the pressure signal at the observer, f_e is the frequency of the emitted pressure signal, f_d is the change in frequency and C is the speed of light in a vacuum.

Now, if a particle is traveling through a pipeline (see Figure 2-right), then the particle becomes an emitter when a piezo-electric crystal emits a signal that reaches the particle. Assuming that the crystal is emitting a pressure signal at point F and the receiver transducer is located at R_1 . Then, the pressure generated by exciting the crystal in F, travels through the medium reaching the particle E and this becomes a source by scattering a pressure signal that reaches the receiver transducer in R_1 . Since the particle is moving in the pipeline with a specific speed v , then the signal that is measured at the receiver is shifted in frequency, in comparison to the transmitted signal. For this case, the geometry given by the location of the

transducers should be included in the equation and the change in frequency is given by [11]:

$$f_d = \frac{2f_e v}{c} \cos(\alpha) \quad (2)$$

where α is the angle between the straight line along which the particle is moving, and the straight line between particle and receiver. Note in Eq. (2) that when the change in frequency and the frequency of the emitted signal are known, then the velocity of the particle can be found as

$$v = \frac{f_d c}{2f_e \cos(\alpha)} \quad (3)$$

Furthermore, the volumetric flow of particles Q , that are traveling through a given cross-section of the pipeline is given by

$$Q = vA \quad (4)$$

where A is the area of the cross-section of the pipeline.

FREQUENCY OF AN ACOUSTIC WAVE

As seen previously in the equations that govern the estimation of the volumetric flow using the Doppler effect, the correct estimation of the frequency change becomes a major issue, and a small error in the estimated frequency may lead to an error in the velocity of the particle in the order of hundreds of meters per second. The frequency resolution obtained during the experiment is given by

$$f = \frac{T}{N} \quad (5)$$

Where N and T is the number of acquired samples and period respectively, the maximum-frequency (f_{\max}) is obtained at maximum period (T_{\max}). The maximum frequency in the transformation depends on the sampling frequency f_s . Note in Eq. (5) that in order to improve the resolution in frequency, it is necessary to either decrease the maximum observable frequency in the transformation or increase the number of sample points in time.

The frequency of the emitter can be obtained knowing the resonance frequency of the piezo-electric crystal, which is the natural-vibration frequency. The Fourier Transform (or its fast version, the FFT) of the time signal is used to determine the resonance frequency of the piezo-electric crystal.

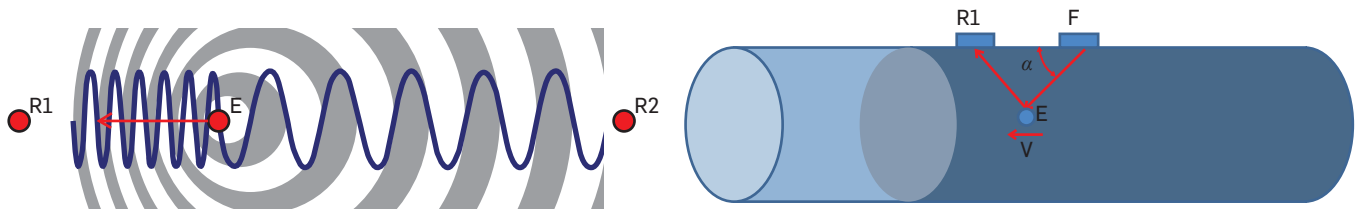


Figure 2. Doppler effect illustration of a particle moving in a pipeline. Left: Example of a particle E moving towards the receiver R1. The frequency observed by the receiver R1 is higher than the one perceived by the receiver R2. Right: Typical propagation method.

ACOUSTIC IMPEDANCE

In addition to the estimation of the frequency change and frequency of the emitter, it is also necessary to know the path of the acoustic ray when it is traveling through a medium. When a pressure wave changes medium, there is change in the path due to the refraction phenomena. This change in the path arises due to the presence of acoustic impedance.

The acoustic impedance Z can be obtained as the product of the speed of the sound c in a given medium and its density, *i.e.*, $Z = cp$. The difference in the acoustic impedance between two mediums affects the signal that is reflected and transmitted. A high reflection coefficient means that most of the signal is reflected rather than refracted. The refraction and reflection phenomena are illustrated in **Figure 3**. The refracted signal has a direction that depends on the angle of the incident wave and the medium characteristics. Snell's law governs this behavior.

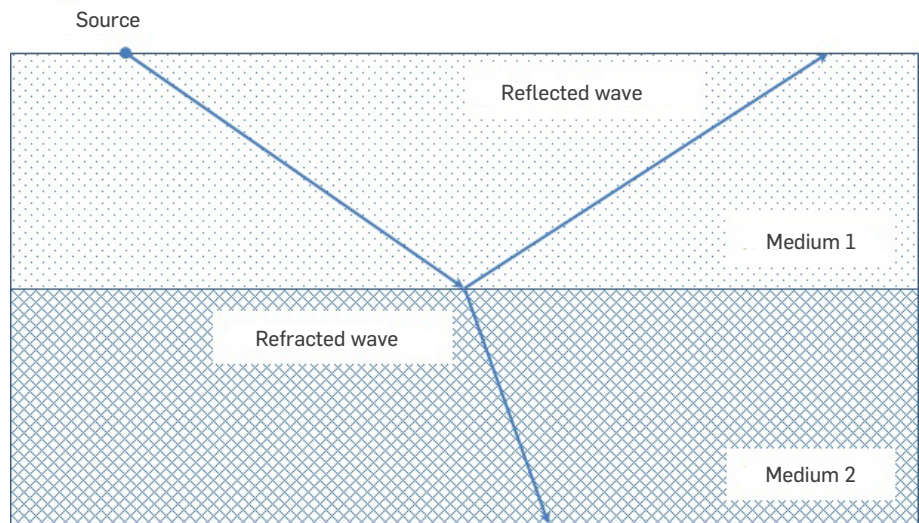


Figure 3. Acoustic wave reflection and refraction. Change in the ray path of the acoustic wave when the signal goes from Medium 1 to Medium 2. The reflected wave remains at Medium 1 and the refracted wave will continue to Medium 2 changing the ray path

3. EXPERIMENTAL DEVELOPMENT

The experiment was designed to resemble the flow line conditions while drilling. Therefore, the cavings size and typical flow values were needed to establish the size and quantity of rock to be used in the experiment. These data were obtained from historic information recorded from wells drilled in Colombia. **Table 1** sets out the amounts and sizes of rock, as well as concentrations in the mud-rock mixture. Furthermore, **Figure 4** shows a picture of both sizes of rock used in the experiment. Additionally, all the experiments required 20 liters of mud with characteristics similar to the drilling mud used in the field, which is a water-based mud consisting of bentonite with a clayseal inhibitor and PAC-R gel.

It was simulated the fluid transport crossing the pipeline by building experimental equipment at laboratory scale. The equipment uses a top tank where the drilling mud is stored, two valves (upper and

Table 1. Rock sizes and concentrations in the mud-rock mixture.

Test	Rock Size (m)	Rock Concentration (%)
1	0.001-0.01	0.1
2	0.001-0.01	0.3
3	0.001-0.01	1
4	0.001-0.01	3
5	0.01-0.02	0.1
6	0.01-0.02	0.3
7	0.01-0.02	1
8	0.01-0.02	3

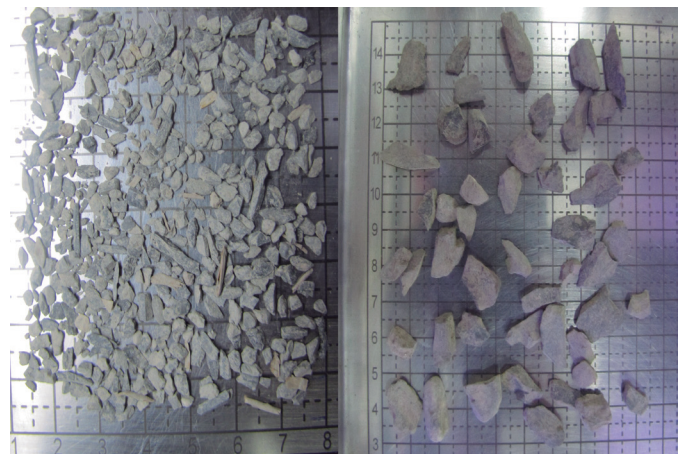


Figure 4. Caving Sizes. Left: the small cavings size from 0.001 to 0.01 m. Right: large cavings size from 0.01 to 0.02 m.

lower) to control the mud flow, a diagonal pipeline and a lower-level tank (See **Figure 5**). The experimental equipment was built in the laboratory and all the experiments were performed using this experiment design.

The transducers were located on the pipe, one acts as an emitter, and the others are receivers. The distance between transducers depends on the pipeline diameter and length. We performed several tests in order to find the best location for the transducers, so that the signal had the best signal to noise ratio.

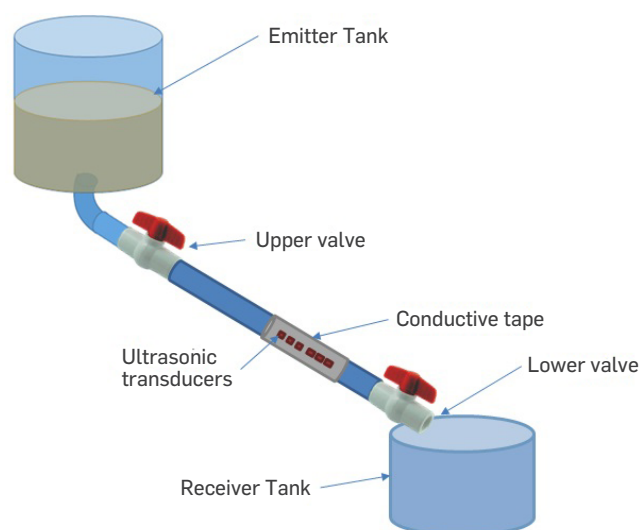


Figure 5. Equipment design used in all experiments. All equipment parts were built in the Geomechanics laboratory at ICP (Colombia), where the tests were conducted.

4. RESULTS

A series of experiments were performed in order to obtain the model for the volumetric flow of rock as a function of the change in frequency detected at the receiver. For all the experiments, the source had a known natural oscillation frequency and the acquisition system recorded acoustical signals automatically. The acquisition system started receiving signals when the flow began. Once the mixture flowed through the pipeline, the system detected a change in the maximum frequency at the receiver and it gave an estimate of the volumetric flow of the rock-mud mixture.

The experiments were performed for the sizes and concentration of rock proposed in **Table 1**. Signals were collected and their frequency was estimated. For each experiment, the amount of cavings (in grams) was also measured along with the travel time through the pipeline. Two different models were obtained: one for a small cavings size and one for a large cavings size. **Figure 6** depicts the data collected, as well as the proposed model for both sizes of cavings. The models relate the estimated frequency with the quantity in grams, and concentration of the rock in the mud-rock mixture. The model for small caving sizes follows an exponential behavior with the fastest change rate. On the other hand, for the larger size of cavings, the exponential model has the slowest change rate.

Once the model was built by running several experiments with different amounts of cavings and cuttings, the model was validated with a set of new experiments. These experiments used different concentration of rocks from both groups of sizes. Before inserting the rock into the drilling mud, the mass of rock was measured with a scale and the concentration of rock in the mixture was calculated. The results from validation tests are recorded in **Table 2**.

As stated before, **Table 2** contains the information from validation data; the first two columns report input data, which correspond to the measured mass obtained with the scale. Columns three and

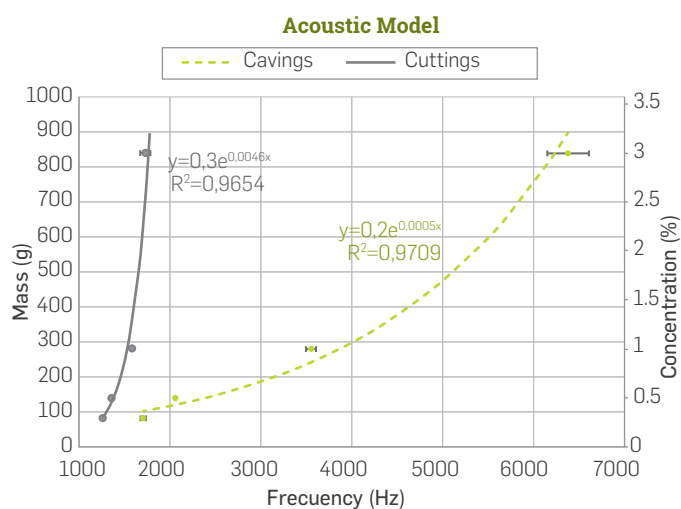


Figure 6. Mathematical model of the volumetric flow as a function of the frequency of the received signals. The solid curve represents the model obtained for small cavings and the dashed curve represents the model for large cavings.

Table 2. Input and experimental data used to validate the model proposed

Input Data		Experimental Data		Relative Error (%)	
Conc. (%)	Mass (g)	Conc. (%)	Mass (g)	Conc. (%)	Mass (g)
0.320	90.000	0.293	82.123	8.437	8.752
0.390	109.000	0.349	99.000	10.512	9.174
0.680	190.000	0.844	236.294	24.117	24.365
0.750	210.000	0.724	202.756	3.466	3.449
1.095	306.000	1.476	413.510	34.794	35.133

four are called "experimental data," corresponding to the modeled results. Finally, in last two columns of **Table 2**, the relative error (as a percentage (%)) is computed as a comparison measure, between measurement by scale and the model.

5. RESULTS ANALYSIS

As shown in the experiment results, there is an exponential relationship between the frequency change of the emitted and received acoustic signals, and the volumetric flow of cavings through the flow line. Thus, the frequency change varies depending on the rock size and concentration of rocks in the drilling mud passing through the flow line pipe.

The frequency change varies from 1100 to 1600 Hz for small rocks or cuttings; and from 1600 to 6800 Hz for cavings. The results obtained during experimentation show that when mud carries small rocks, the acoustic frequency of the received signals experiences rapid decay if only a few grams of rocks were changed. On the other hand, for large samples of cavings, a much slower decay in frequency was observed for the same change in mass, leading to a wider range of frequencies.

Additionally, the empirical model obtained with the experiments shows that there is a range in the frequency change (between 1800 and 2000 Hz) in which mass of rock can be miscalculated, because it indicates either a small concentration of large cavings or a large concentration of small cavings. Since it is important to determine the size of the rock crossing the pipe to detect the instability of the well, then this issue should be corrected by including some additional information on the signals received, such as amplitude.

CONCLUSIONS

The proposed method makes it possible to estimate the concentration of cavings in a mixture of mud-rock using the ultrasound Doppler effect. The method is suitable for real time applications while drilling, since it is non-invasive and the acquisition system is relatively simple.

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