



Ingeniería

ISSN: 0121-750X

Universidad Distrital Francisco José de Caldas

Mejía-Gallón, Valentina; Naranjo-Cardona, María Camila; Atehortua Carmona, Juan;
Vallejo Pareja, Samuel; Santa-Marín, Juan Felipe; M. Posada, Viviana; Ramírez, Juan

SSOP Three-Dimensional Reconstruction of Tibia and
Fibula for Applications in Biomechanical Fracture Models

Ingeniería, vol. 26, no. 3, 2021, September-December, pp. 450-464

Universidad Distrital Francisco José de Caldas

DOI: <https://doi.org/10.14483/23448393.18471>

Available in: <https://www.redalyc.org/articulo.oa?id=498870156009>

- How to cite
- Complete issue
- More information about this article
- Journal's webpage in redalyc.org

redalyc.org

Scientific Information System Redalyc

Network of Scientific Journals from Latin America and the Caribbean, Spain and
Portugal

Project academic non-profit, developed under the open access initiative

SSOP Three-Dimensional Reconstruction of Tibia and Fibula for Applications in Biomechanical Fracture Models

SSOP Reconstrucción tridimensional de la tibia y el peroné para su aplicación en modelos biomecánicos de fracturas

Valentina Mejía-Gallón* ¹, **María Camila Naranjo-Cardona** ¹, **Juan Atehortua Carmona** ¹, **Samuel Vallejo Pareja** ¹, **Juan Felipe Santa-Marín** ¹, **Viviana M. Posada** ¹, **Juan Ramírez** ¹

¹Departamento de ingeniería mecánica, Universidad Nacional de Colombia, Medellín, Colombia.

*Correspondance email: vamejiag@unal.edu.co

Recibido: 15/08/2021. Modificado: 27/08/2021. Aceptado: 15/09/2021.

Open access



Cite this paper as: V. Mejía-Gallón *et al.*, "SSOP Three-Dimensional Reconstruction of Tibia and Fibula for Applications in Biomechanical Fracture Models," INGENIERÍA, Vol. 26, Num. 3, 2021. 450-464.

© The authors; reproduction right holder Universidad Distrital Francisco José de Caldas.

<https://doi.org/10.14483/23448393.18471>

Abstract

Context: Non-fatal injuries represent a public health issue. Among them, lower limb fractures have a large impact on the costs related to orthopedic treatments. In this work, a three-dimensional reconstruction of the tibia and fibula was performed for biomechanical applications with the purpose of defining the 3D reconstruction parameters that allow reducing patients' radiation exposure and computational costs.

Method: For the 3D reconstruction, a computerized tomography taken from a volunteer was used, as well as two software applications specialized in DICOM image reconstruction (Mimics Research and 3DSlicer). The number of images included in the volume was modified, and the results were compared. The quality of the reconstructed volumes was verified by comparing the reference volume reconstructed with the total number of images/slices vs. the modified volumes. The MeshLab software was used for this purpose. The analyzed parameters were the distance differences between the reference and the alternative models, as well as the qualitative curvature analysis.

Results: The ANOVA results for the Max (maximum distance between meshes) response shows that software and slices are significant factors. However, the software-slices interaction did not have a significant influence. As for the RMS (root mean square) distance response, software, slices, and the software-slices interaction are not significant. For the Mean distance response, slices and the software-slices interaction are not significant. Nevertheless, software significantly influences the response. These results suggest a potential way to reduce the computational cost and the patient's radiation exposure in future biomechanical and preoperative analyses, since the same quality can be obtained by including fewer 2D images in the reconstruction.

Conclusions: The reconstructed surfaces are smoother when Mimics is used, even though the same smoothness factor was employed in both software applications during the reconstruction. When 16 slices are used (retained every 16 images from the complete original model), the distance differences increased for both bones (tibia and fibula). For the RMS, reducing the number of slices and using either one of the two applications analyzed would not show any significant differences in the reconstruction, thus allowing the potential reduction of radiation exposure of the patient.

Keywords: biomechanical models, fibula, 3D reconstruction, tibia

Acknowledgements: The authors are grateful to Universidad Nacional de Colombia for funding the project "Estado de esfuerzos en un elemento de osteosíntesis en la consolidación de una fractura de miembro inferior".

Language: English

Resumen

Contexto: Las lesiones no fatales representan un problema de salud pública. Entre ellas, las fracturas de las extremidades inferiores tienen un gran impacto en los costos relacionados con los tratamientos ortopédicos. En este trabajo se realizó una reconstrucción tridimensional de la tibia y el peroné para aplicaciones biomecánicas con el fin de definir los parámetros de reconstrucción 3D que permitan reducir la exposición a la radiación de los pacientes y el costo computacional.

Método: Para la reconstrucción 3D se empleó una tomografía computarizada tomada a un voluntario. Se utilizaron dos programas de software especializados en la reconstrucción de imágenes DICOM (Mimics Research y 3DSlicer). Se modificó el número de imágenes 2D incluidas en el volumen y se compararon los resultados. La calidad de los volúmenes reconstruidos se verificó comparando el volumen de referencia reconstruido con el número total de imágenes/cortes frente a los volúmenes modificados. Para ello se utilizó el software MeshLab. Los parámetros analizados fueron las diferencias de distancia entre el modelo de referencia y el alternativo, y el análisis cualitativo de la curvatura.

Resultados: Los resultados del ANOVA para la respuesta Max (distancia máxima entre mallas) muestran que el software y los cortes son factores significativos. Sin embargo, la interacción software-cortes no tuvo una influencia significativa. Para la respuesta RMS (Root Mean Square) el software, los cortes y la interacción software*cortes no son significativos. Para la respuesta media, los cortes y la interacción software-cortes no son significativos. Sin embargo, el software influye significativamente en los resultados. Estos resultados suponen una reducción del coste computacional y de la exposición de los pacientes a radiación en futuros análisis biomecánicos y preoperatorios, ya que se puede obtener la misma calidad incluyendo menos imágenes 2D en la reconstrucción.

Conclusiones: Las superficies reconstruidas son más suaves cuando se utiliza Mimics a pesar de que se utilizó el mismo factor de suavidad en ambos programas durante la reconstrucción. Cuando se utilizan 16 cortes (retenidas cada 16 imágenes del modelo original completo), las diferencias de distancia aumentan para ambos huesos (tibia y peroné). Para el RMS, reducir el número de cortes y utilizar cualquiera de los dos programas analizados no presentaría diferencias significativas en la reconstrucción planteándose como una forma potencial para la reducción de la exposición a la radiación del paciente.

Palabras clave: modelos biomecánicos, peroné, reconstrucción 3D, tibia

Agradecimientos: Los autores agradecen a la Universidad Nacional de Colombia la financiación del proyecto “Estado de esfuerzos en un elemento de osteosíntesis en la consolidación de una fractura de miembro inferior”.

Idioma: Inglés.

1. Introduction

The World Health Organization (WHO) defines non-fatal injuries as a public health problem [1]. Within these traumas, tibia injuries have been demonstrated to be one of the most common. Epidemiological studies worldwide report that this type of injury represents the largest number of fractures, which can be attributed to traffic accidents affecting the lower limbs [2], [3]. Moreover, the National Institute of Forensic Medicine reported tibia fractures as the third most prevalent pediatric injury. According to the data reported by the WHO, on an annual basis, between 20 and 50 million people in the world suffer non-fatal injuries due to traffic accidents, highlighting lower limb fractures as a public health problem. Hence, repairing lower limb fractures greatly impacts the costs related to orthopedic treatments around the world. [4], [5] indicate that the leading causes of tibial fractures in developed countries like Sweden between 2011 and 2015 were simple falls (44 %) and traffic accidents (22 %). Tibial fractures can be classified according to their location and type of

injury. The Orthopedic Trauma Association and the AO Foundation classified these fractures by location and morphology, and they provided additional classifications related to open, pediatric, and periprosthetic fractures [6]. Tibial plateau fractures are prevalent, and they have been divided into several groups: lateral and medial tibial plateau fractures, posterior tibial plateau fractures, coronal splits, bicondylar fractures, and under subcondylar fractures [7]. The type of treatment is selected based on the surgeon's experience, and, in some cases, the result can be subjective. Another option to select and evaluate the fixation geometry is the use biomechanical models, which are developed based on a 3D reconstruction of fractured bones.

Biomechanical models allow evaluating and predicting the behavior of potential fixation configurations in different types of fractures using computer simulation and laboratory tests [8]. Computational models also aid in making several therapeutic decisions, such as patient positioning for radiotherapy treatments [9], kidney stones surgery [10], and preoperative orthopedic planning processes [11], [12]. The construction of biomechanical models starts with the acquisition of a stack of 2D cross-sectional medical images (*i.e.*, computerized tomography, CT), which are then volumetrically represented and used in numerical computational analyses. Therefore, improving the image acquisition protocols would provide safer and more cost-effective processes. Experimental analysis of the influence of scan resolution, thresholding, and reconstruction algorithm on CT-based kinematic measurements [13] showed no significant influence on the accuracy of the calculated bone kinematics. Therefore, a lower resolution scan was recommended, which is one of the physical parameters to optimize the quality of the image for it to be good enough to perform a clinical diagnostic or a 3D reconstruction while keeping the patient's radiation exposure as low as possible [14]. This is especially important since low-dose radiation exposure due to the increasingly common use of CT has been associated with a potential increased risk of cancer in patients, especially in children [15].

As mentioned above, the first step to developing a biomechanical model is reconstruction using a 2D stack of tomographic images in a medical image analysis software (such as Mimics or 3DSlicer). Previous reports [16] have found minimum differences when the reconstruction is carried out using different free software applications, which obtained bone models of good quality. The authors postulated that freeware is suitable for 3D bone model reconstruction. In this work, a commercial (Mimics Research 19.0, research license) and free software (Slicer, version 4.11) were included in the analysis to study the offer of computational tools and their compliance with quality standards. This paper aims to evaluate the configurations used for 3D reconstructions in the tibia and fibula for applications in biomechanical fracture models. This evaluation includes the advantages and disadvantages of two software applications, as well as the number of slices required for quality reconstruction, aiming to reduce the potential exposure dose to radiation.

2. Experimentation

2.1. Acquisition of 2D cross-sectional medical images for 3D reconstruction

Tomography images were taken from an individual male, who was 25 years old and 1,82 m tall, with a weight of 80 kg and no reported pathologies. Before the image acquisition, the volunteer

filled out an informed consent. He was chosen to be used in future studies since his results could be compared to previously collected data available in Opensim databases. The tomographic images were taken using the parameters shown in Table I, based on the CT scan protocol provided by Materialise [17].

Table I. Parameters obtained for the CT scan

Parameter	Value	Parameter	Value
Scanning technique	CT	kVp	120
Planes	(Axial, sagittal, coronal) A, S, C	mAs	150
Target tissue	Bone	Pitch	0,9
Field of view -FOV	Width \leq 50 cm. Details: Complete pelvis between the iliac crests. From astragalus to proximal ilium.	Matrix	512 x 512
Slice thickness	0,5 mm	Bones	Tibia and fibula (left and right)
Slice Increment	1,25 mm	Contrast	None
Tilt	None	Image type file	DICOM
Scan type	Helical mode	Overlap	40 % (0,5mm/ 1,25mm)

2.2. Selection of reconstruction software

Two software applications with similar capabilities were selected because they were readily available for the study. The selected software was Mimics Research 19.0 (research license) and 3DSlicer (Slicer version 4.11.20210226, open source). The capabilities of the both applications are shown in Table II.

2.3. Modeling the tibia

The total number of 2D cross-sectional images (slices) acquired during the CT scan was 2.118. After obtaining the data, the reference model was reconstructed. Alternative models were also reconstructed, creating gaps between the 2D slice files. Table III shows the different number of slices (retained slices from the reference model) used to reconstruct the alternative models. The model's total number of images/slices considered the helicoidal scanning mode, and the same number was used for both software applications.

The general operation principle was similar in both applications, including importing the DICOM files. The threshold values with a minimum of 124 HU and a maximum of 3.071 HU were used. Image segmentation was performed using various tools that met the same objectives in both Mi-

Table II. Capabilities of two software used in this study

Software	Operating system	Input Data	Output Data	Features
3DSlicer (Slicer version 4.11.2021022)	Windows MacOS Linux	DICOM, NRRD MetaImage, VTK Analyze, NifTI, BMP BioRad, Brains2, GIPL, JPEG, LSM, PNG Stimulate, TIFF, MGH-NMR, MRC, Electron Density	JPEG, PNG, TIFF, VTK Image, STL, OBJ, volume rendering, NRRD, image segmentation, VTK.	No linear transformations 2D and 3D visualization and interactive segmentation of image and data Support for modules of command-line interface (CLI) Multiple compatible extensions
Mimics Research 19.0	Windows Linux	CT, μ CT or MRI, DICOM	STL, OBJ, and PLY formats, volume rendering, and manual or semiautomatic image segmentation.	Thresholding tool and active contour thresholding. STL creation. Mesh for FEM Commercial software

Table III. Parameters using different software

Number of slices	Expected gap (mm)	Total number of images
Alternative. model 1: Every 4 images	2	424
Alternative. model 2: Every 6 images	3	303
Alternative. model 3: Every 8 images	4	236
Alternative. model 4: Every 16 images	8	128
Reference model: Full set	0,5	2.118

mics and 3D Slicer. A smooth factor of 0,4 was performed in two iterations, as well as minimal intervention of manual segmentation of the mask. A schematic representation of the steps used to obtain the model is shown in Fig. 1.

2.4. Analysis of reconstructed tibias and fibulas

A factorial design was used to analyze the effect of two factors: software and the number of slices in the RMS (root mean square), Max (maximum distance between meshes), and Mean distance

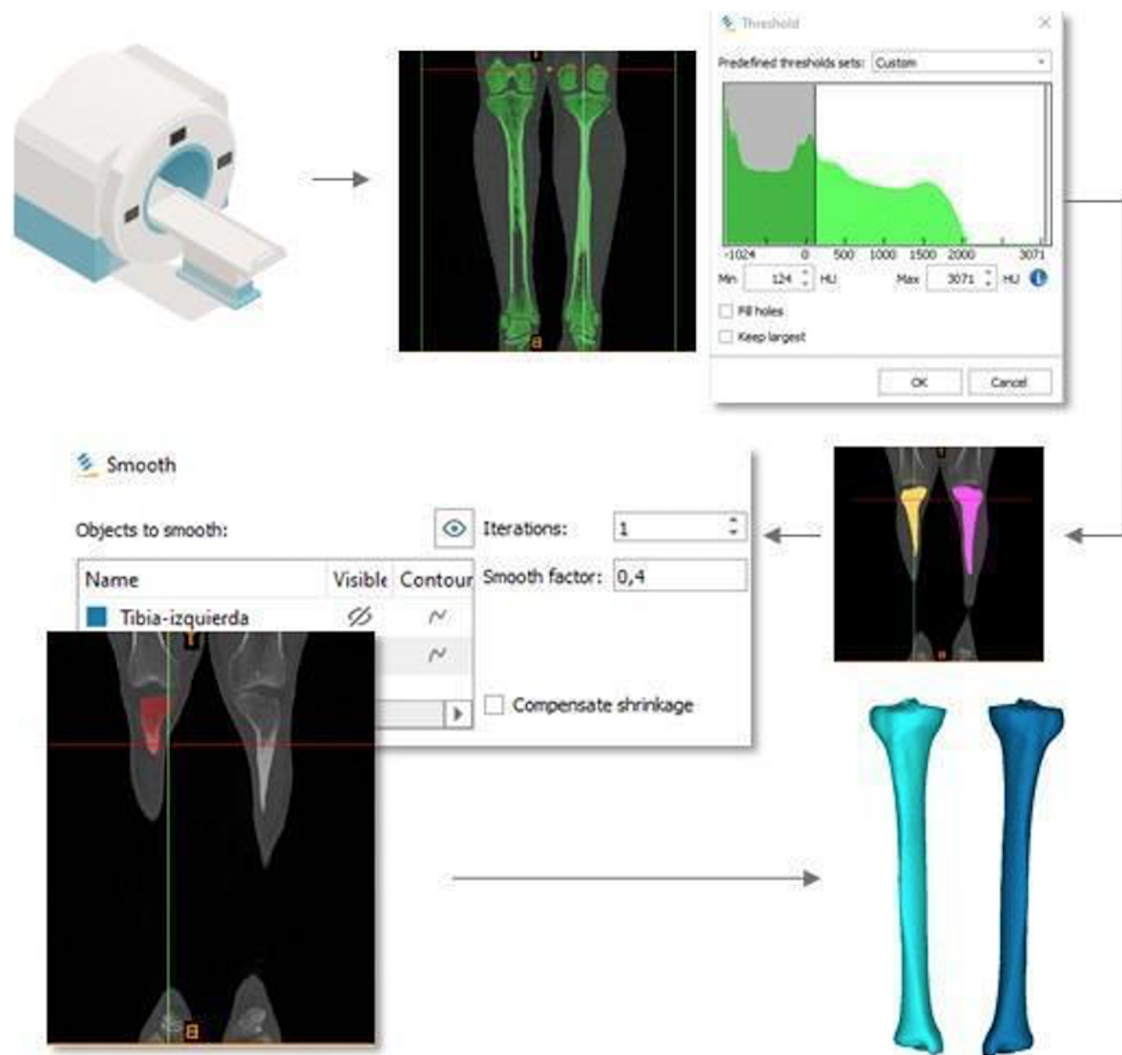


Figure 1. Schematic representations of the steps used to obtain the volumetric model

responses. The responses were obtained via the Euclidean distance of the model with a reduced number of slices vs. the control (the model with the complete number of slices). The MeshLab software was used to calculate the Hausdorff distance, which refers to the maximum distance between two subsets of points, where one belongs to an x-mesh, and the other belongs to a y-mesh. MeshLab samples each point belonging to the x-mesh and takes the closest point of the y-mesh. Therefore, it is very important to perform a previous alignment process between the meshes as accurately as possible. It is also essential to take as many points as possible when applying the filter, which can be ensured by sampling the vertices, edges, and faces [18]. The software factor had two levels: Mimics and 3D Slicer. The number of slices factor had four levels: 4, 6, 8, and 16. The alternative reconstructed models were compared with the reference model, and the right tibia and left tibia were considered as replications. The experimental setup is shown in Table IV. Residual plots were used to test the normality, independence, and constant variance assumptions (data not shown). Outliers identified via scatter plots were extracted from the analysis. The incidence of the effects and two-level interactions was evaluated via ANOVA ($p < 0,05$).

Table IV. Experimental setup for the factorials design

Run Order	Blocks	Software	Slices	y1 RMS	y2 Max	y3 Mean
16	Left tibia	Mimics	4	0,0903	0,8401	0,0633
15		Mimics	6	0,1311	0,7851	0,106
12		Mimics	8	0,1981	1,3788	0,1448
10		Mimics	16	0,289	1,3786	0,2542
9		3D Slicer	4	0,1453	0,7742	0,0473
14		3D Slicer	6	0,147	0,8535	0,0654
13		3D Slicer	8	0,1829	0,9685	0,1131
11		3D Slicer	16	0,2266	1,0433	0,1355
2	Right tibia	Mimics	4	0,2627	0,6525	0,2548
4		Mimics	6	0,298	1,097	0,2815
6		Mimics	8	0,3327	1,4137	0,2946
1		Mimics	16	0,268	1,9779	0,1555
3		3D Slicer	4	0,0832	0,9433	0,1094
7		3D Slicer	6	0,1093	0,9073	0,1096
8		3D Slicer	8	0,1566	1,0809	0,1466
5		3D Slicer	16	0,2185	1,0426	0,1724

3. Results and discussion

From the p-values, software ($p = 0,02$) and slices ($p = 0,007$) are significant for the response. The software affects the Max of the calculated distances because the line is not horizontal. Moreover, the Mimics software has a higher Max value than 3D Slicer. The number of slices also affects the Max, and, as observed in Figs. 2c and 2d, the highest number was obtained when extracting 16 slices. The overall mean is marked in the dotted reference line. As seen in Fig. 2d, 3DSlicer reports lower Max values in most cases related to slices. However, the p-value (0,060) reveals that this interaction is not significant. The ANOVA results for Max RMS and Mean can be seen in appendix Tables SI, SII, and SIII, respectively.

Figs. 2a and 2b show the Mean effects and interaction plots, respectively. As observed, 3DSlicer has lower RMS values than Mimics, and the higher RMS was noticed with the 16 slices. However, from the p-values, software ($p = 0,07$), slices ($p = 0,24$), and the interaction between software and slices ($p = 0,97$) are not significant for the RMS response. On the other hand, the highest mean value was observed for the model with 8 slices (Figs. 2e and 2f). However, slices ($p = 0,56$) and the software-slices interaction ($p = 0,95$) are not significant for the response. Nevertheless, software ($p = 0,046$) significantly influences the response, and 3DSlicer had a lower Mean value than Mimics.

Visible differences are spotted in the 3D images when using both reconstruction software applications. Fig. 3 shows the reference model for Mimics and its corresponding 3DSlicer reconstructions. The first interesting change is related to the visual smoothness of the surface. Generally speaking, the surfaces are smoother when using Mimics, even though the same smooth factor was used in 3DSlicer. There are indeed differences in the smoothing algorithms. The wrapping tool in Mimics deletes rough areas and gaps in the model, which is especially useful in numerical analyses [19]. Since the 2D cross-sectional images were acquired using the helical mode, the removal of images

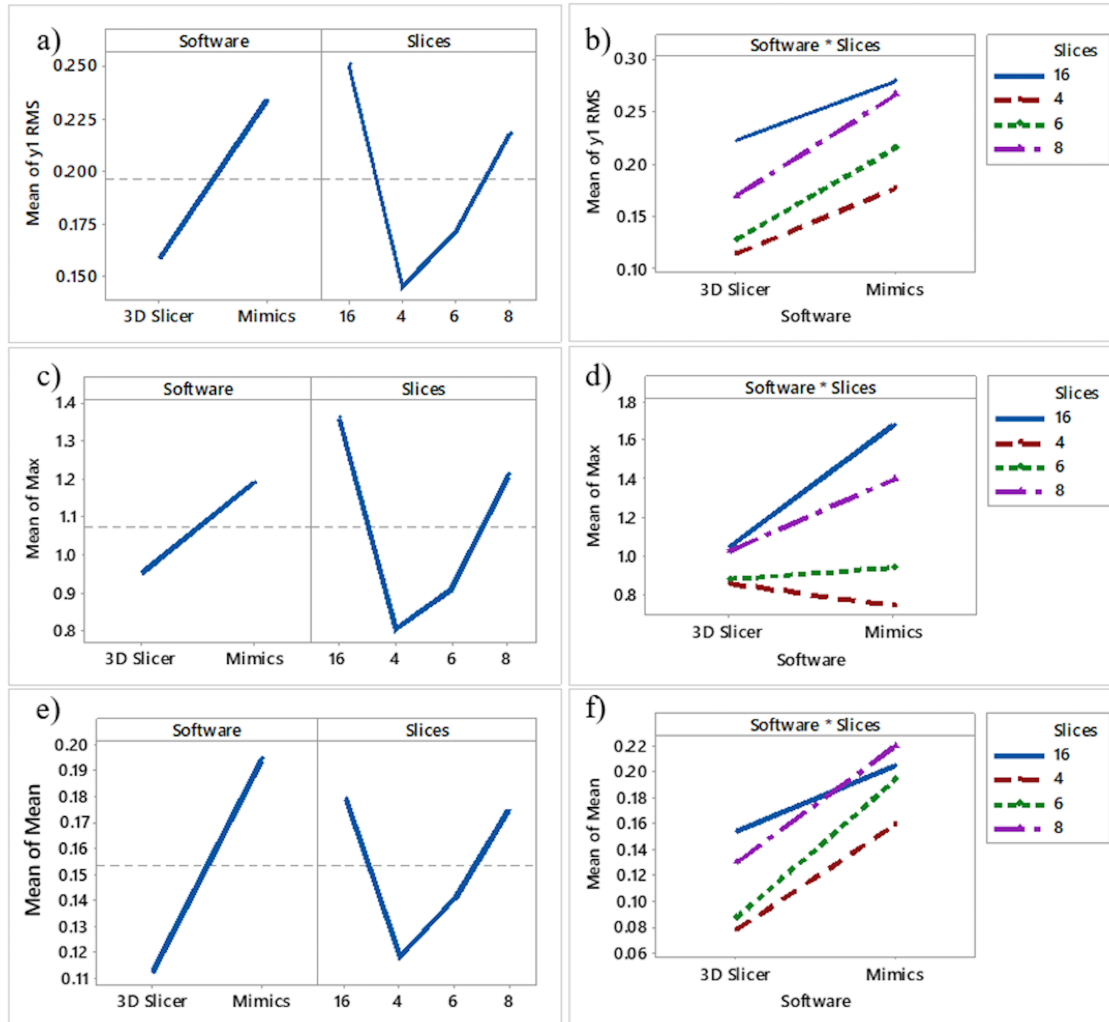


Figure 2. Main effects and interaction plots for RMS, Max, and Mean

considered potential helicoidal artifacts. On the other hand, the smoothing process in 3DSlicer consists of the remotion of small extrusions and the filling of small gaps without changing the smooth contours [20]. Additionally, Boolean operations were used in 3DSlicer to simulate the wrapping tool in Mimics.

Fig. 4 shows the distance differences from the reference model for both bones using Mimics for the most representative alternative models. In addition, the distance difference between the reference models and the alternative models obtained using each software is shown. When the distance between the two models is larger, the color tends towards red, and when the vertex is close, the color tends to be blue. The chromatic scale defines the intermediate values. The results suggest that the distances between the reference model and the alternative model are neglectable when using 4 slices in the reconstruction. However, with 16 slices, the differences increased, as shown in the changes in the color scale (from blue to red) around the tibia and fibula. The greatest differences (red) in all cases are located at the proximal tibia, given that the complexity of the geometry increases in that area (the tibial plateau). When the two applications are compared, the visual differences are concentrated at the image's top-left area (proximal zone) for the tibia and at the top-right for the

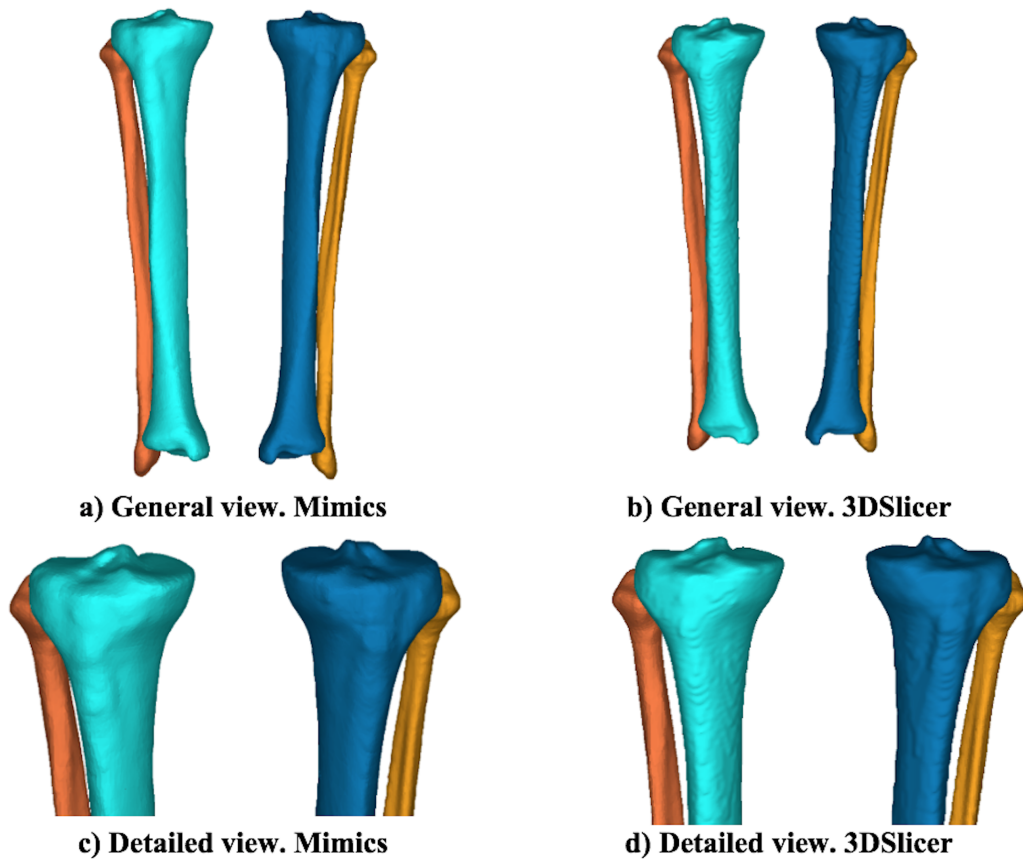


Figure 3. Reference model after reconstructions: a) and c) Mimics; b) and d) 3DSlicer

fibula. However, along the length of the bone, the model turns blue, meaning that the reconstruction of each software is very similar. Moreover, the reference model has been colored for comparison purposes. The zones at the Figure that do not have a chromatic scale indicate that, locally, the reconstructed model is larger than the reference model.

Figure 5 shows the curvature analysis for the left tibia and right fibula alternative models, as well as the reference models using both Mimics and 3DSlicer. The greatest curvature value displayed is 1, and the smallest one is 0,0010. As the radius of curvature decreases, color changes from black (0,0010) to blue, green, and red (1,0000). As the radius of curvature increases, the curvature value decreases. A planar surface has a curvature value of zero because the radii of flat faces are infinite. The results showed that there are no noticeable differences between the reference model and the model reconstructed using 4 slices (not shown). However, when 16 slices are used to reconstruct the alternative model, the curvature (and the continuity) of the surfaces is affected.

Another important difference between the reference and alternative models (16 slices) are compared is the mesh size (element size) in the STL file. When 16 slices are used, the software (Mimics) cannot provide continuity for the surfaces, and some empty elements can be identified (see the empty element in black in Fig 5b at the top-right). When the number of slices is 16, the wrapping tool should be modified as slices are removed. However, in this work, the same wrapping tool was used

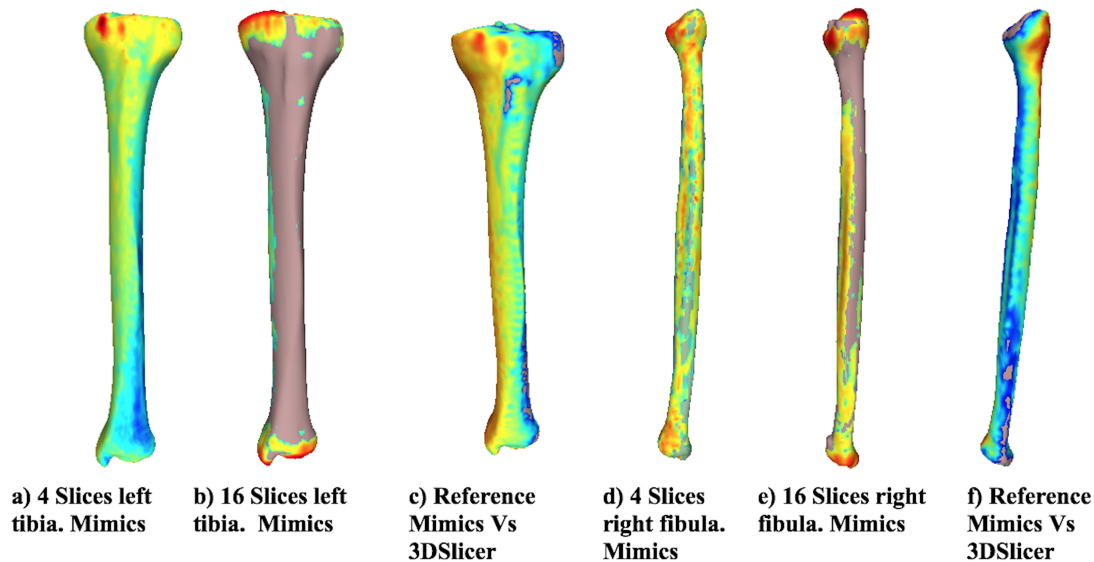


Figure 4. Distance from the reference model

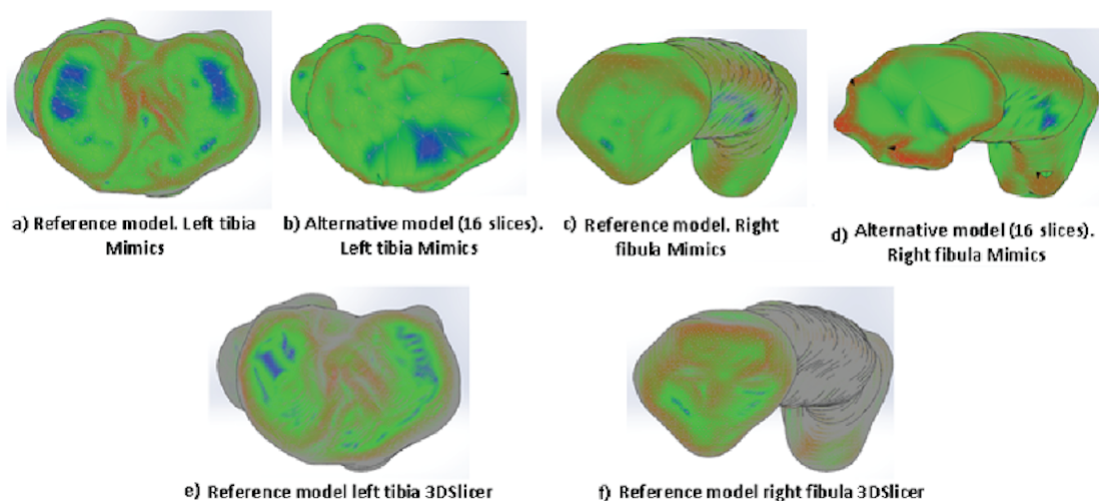


Figure 5. Curvature analysis for different numbers of slices (tibia and fibula)

for comparison purposes. The same behavior was identified for the tibia and fibula, where several empty elements can be observed in Fig. 5d.

The alternative model (16 slices) for the fibula shows that the mesh size is extremely large, and it does not properly describe the curvature in the proximal zone of the fibula. On the contrary, the curvature along the shaft of the fibula is very similar since the geometry is less complex than the fibular head. Figs. 5e and 5f show the reference model reconstructed using 3DSlicer. The first interesting result is related to the size of the elements. The mesh created using the same procedure in Mimics provides a reference model with more details in the proximal zone of both bones. The curvature is similar for the model reconstructed using Mimics for the proximal zone. However, the surfaces are smoother when reconstructed using Mimics.

To summarize, in this work, the differences between the two software applications were investigated to create STL bone models. The manual intervention by the operator was limited as much as possible by using the same processing parameters, even though the segmentation algorithms of this software are not known. Another important detail related to the processing performed in order to obtain an STL file is that, when the model is exported using the ASCII file, the imported model is less prone to show errors in MeshLab. The same behavior has been reported by other authors [16]. In this work, the mesh parameters, such as the number and density of the triangles in the mesh, were only qualitatively specified. Future work could focus on quantifying the parameters of the mesh after the final file is generated. This result suggests that the individual physical size of the triangles depends on the analyzed bone (tibia or fibula).

4. Conclusions

This work revealed that the software-slices interaction did not significantly influence any of the analyses. The main effects and interaction plot showed that the highest differences were observed in the 16-slice model for the tibia with the RMS and Max analysis. Furthermore, the reconstructed surfaces were smoother when Mimics was used, even though the same smooth factor was used in both software applications during the reconstruction. Nevertheless, Mimics reported continuity issues, and it had the highest RMS and Max.

As for the RMS distance, reducing the number of slices and using either of the applications analyzed, without nature of proof, would not present a significant difference in the reconstruction allowing for the reduction in radiation exposure and computational cost. However, for the Max distance, the reduced mesh would present a significant difference compared with the original reconstruction. For the Mean distance, the mesh would only be affected by the software used and not by the reduced number of slices.

5. Acknowledgments

The authors are grateful to Universidad Nacional de Colombia for funding the project *Estado de esfuerzos en un elemento de osteosíntesis en la consolidación de una fractura de miembro inferior* (Stress state in an osteosynthesis element in the consolidation of a lower limb fracture, code H:50195).

References

- [1] OMS, “Accidentes de tránsito,” 2018. <https://www.who.int/es/news-room/fact-sheets/detail/road-traffic-injuries> (accessed Jul. 13, 2021). ↑452
- [2] K. Gichuhi, “Injury Pattern Among Non-fatal Road Traffic Crash Victims,” *East Afr. Orthop. J.*, vol. 1, no. 1, pp. 23-25, 2010. <https://doi.org/10.4314/eaoj.v1i1.49454> ↑452
- [3] R.-H. Pan *et al.*, “Epidemiology of Orthopedic Fractures and Other Injuries among Inpatients Admitted due to Traffic Accidents: A 10-Year Nationwide Survey in Taiwan,” *Sci. World J.*, vol. 2014, ID. 637872, Feb. 2014. <https://doi.org/10.1155/2014/637872> ↑452

- [4] J. D. Heckman and J. Sarasohn-Kahn, "The economics of treating tibia fractures. The cost of delayed unions," *Bull. Hosp. Jt. Dis.*, vol. 56, No. 1, pp. 63-72, 1997. <https://pubmed.ncbi.nlm.nih.gov/9063607/> ↑ 452
- [5] D. Wennergren, C. Bergdahl, J. Ekelund, H. Juto, M. Sundfeldt, and M. Möller, "Epidemiology and incidence of tibia fractures in the Swedish Fracture Register" *Injury*, vol. 49, no. 11, pp. 2068-2074, Nov. 2018. <https://doi.org/10.1016/j.injury.2018.09.008> ↑ 452
- [6] E. Meinberg, J. Agel, C. Roberts, M. D. Karam, and J. F. Kellam, "Fracture and Dislocation Classification Compendium-2018," *J. Orthop. Trauma*, vol. 32, no. 1, Jan. 2018. <https://doi.org/10.1097/bot.0000000000001063> ↑ 453
- [7] S. H. Khan, A. J. Ahmad, and M. Umar, "Tibial Plateau Fractures: A New Classification Scheme," *Clin. Orthop. Rel. Res.*, vol. 375, pp. 231-242, Jun. 2000. <https://pubmed.ncbi.nlm.nih.gov/10853174/> ↑ 453
- [8] H. Sun, Q. F. He, B. Bin Zhang, Y. Zhu, W. Zhang, and Y. M. Chai, "A biomechanical evaluation of different fixation strategies for posterolateral fragments in tibial plateau fractures and introduction of the 'magic screw'," *Knee*, vol. 25, no. 3, pp. 417-426, Apr. 2018. <https://doi.org/10.1016/j.knee.2018.03.015> ↑ 453
- [9] Nelson, V., Deshpande, S., Gray, A. *et al.* "Comparison of digitally reconstructed radiographs generated from axial and helical CT scanning modes: a phantom study," *Australas. Phys. Eng. Sci. Med.*, vol. 37, pp. 285-290, Mar. 2014. <https://doi.org/10.1007/s13246-014-0257-x> ↑ 453
- [10] A. Tsaturyan *et al.* "Technical aspects to maximize the hyperaccuracy three-dimensional (HA3D™) computed tomography reconstruction for kidney stones surgery: a pilot study," *Urolithiasis*, vol. 49, pp. 559-566, Apr. 2021. <https://doi.org/10.1007/s00240-021-01262-6> ↑ 453
- [11] J. Huo *et al.*, "Value of 3D preoperative planning for primary total hip arthroplasty based on artificial intelligence technology," *J. Orthop. Surg. Res.*, vol. 16, art. no. 156, Feb. 2021. <https://doi.org/10.1186/s13018-021-02294-9> ↑ 453
- [12] G. Marongiu, R. Prost, and A. Capone, "Use of 3D modelling and 3D printing for the diagnostic process, decision making and preoperative planning of periprosthetic acetabular", *BMJ Case Rep.*, 13, no. 1, art no. e233117., Jan. 2020. <https://doi.org/10.1136/bcr-2019-233117> ↑ 453
- [13] C. J. Tan, W. C. H. Parr, W. R. Walsh, M. Makara, and K. A. Johnson, "Influence of Scan Resolution, Thresholding, and Reconstruction Algorithm on Computed Tomography-Based Kinematic Measurements", *J. Biomech. Eng.*, vol. 139, no. 10, art. no. 28787471, Oct. 2017. <https://doi.org/10.1115/1.4037558> ↑ 453
- [14] J. Aldrich *et al.*, *Dose Reduction in CT while Maintaining Diagnostic Confidence: A Feasibility/Demonstration Study*, Vienna, Austria: International Atomic Energy Agency, 2009. https://www-pub.iaea.org/MTCD/Publications/PDF/te_1621_web.pdf ↑ 453
- [15] D. J. Brenner, "Computed Tomography — An Increasing Source of Radiation Exposure", *N. Eng. J. Med.*, vol. 357, no. 22, pp. 2277- 2284, Nov. 2007. <https://dx.doi.org/10.1056/NEJMr072149> ↑ 453
- [16] K. Matsiushevich, C. Belvedere, A. Leardini, and S. Durante, "Quantitative comparison of freeware software for bone mesh from DICOM files," *J. Biomech.*, vol. 84, pp. 247-251, Feb. 2019. <https://doi.org/10.1016/j.jbiomech.2018.12.031> ↑ 453, 461
- [17] Materialise, "CT scan protocol leg 3 regions", 2017. <https://www.materialise.com/en/resources/all/scan-protocols> (accessed Jul. 13, 2021). ↑ 454
- [18] Aloopingicon, "Stuff: Measuring the difference between two meshes", 2010. <http://meshlabstuff.blogspot.com/2010/01/measuring-difference-between-two-meshes.html> (accessed Jul. 13, 2021). ↑ 456
- [19] Mimics, "Mimics Student Edition Course Book", 2021. <https://www.materialise.com/en/medical/mimics-innovation-suite/academic-research-education> (accessed Jul. 13, 2021). ↑ 457
- [20] 3DSlicer, "Documentation/4.10", 2021. <https://www.slicer.org/wiki/Documentation/4.10>, (accessed Jul. 13, 2021). ↑ 458

Juan Ramírez

Mechanical engineer and PhD in Engineering from Universidad Nacional de Colombia. I have been an Associate Professor at the same university since 2003. In addition, between 2018 and 2020, I was the Vice-dean of Research at the Department of Mines - Universidad Nacional de Colombia. Nowadays, I am acting as the director of GIBIR

(Biomechanics and Rehabilitation Research Group), where 4 PhD and more than 10 MSc have been formed.
Email: jframirp@unal.edu.co.

Juan Atehortúa-Carmona

Mechanical engineer, Master's degree student in Mechanical Engineering from Universidad Nacional de Colombia. I am currently a project design manager engineer and a researcher of GIBIR (Biomechanics and Rehabilitation Research Group).
Email: jfatehortuac@unal.edu.co.

Juan Felipe Santa-Marin

BSc in Mechanical Eng. (2005), M. Eng. in Materials and Process Engineering (2008) and PhD. in Engineering with emphasis in Materials Science and Technology (2013) from the same university. He is currently a researcher for the Advanced Materials and Energy (MATyER) Research Group at Instituto Tecnológico Metropolitano. His interests include materials in general with emphasis on wear, processing, and physicalchemical and mechanical characterization of materials.
Email: jfsanta@gmail.com.

Maria Camila-Naranjo

Mechanical Engineering student from Universidad Nacional de Colombia and a researcher of GIBIR (Biomechanics and Rehabilitation Research Group).
Email: mcnaranjoc@unal.edu.co.

Valentina Mejía-Gallón

Mechanical Engineering student from Universidad Nacional de Colombia and a researcher of GIBIR (Biomechanics and Rehabilitation Research Group).
Email: vamejiag@unal.edu.co.

Samuel Vallejo Pareja

Mechanical engineer (2019) from Universidad Nacional de Colombia, Medellín, Colombia, and researcher of GIBIR (Biomechanics and Rehabilitation Research Group) since 2016. Project design manager engineer at Universidad Nacional de Colombia (2019-2020). Since 2020, researcher of BIOMATIC (Biomechanics, materials, ICTs, design and quality for the leather, plastics and rubber sector and its production chains Research Group) at Sistema Nacional de Aprendizaje (SENA), Itagüí, Antioquia, Colombia. Currently a Master's degree student in Mechanical Engineering at Universidad Nacional de Colombia, Medellín, Colombia. My research interests include mechanical design, computational mechanics, and biomechanics.
Email: savallejopa@unal.edu.co.

Viviana M. Posada

BSc. in Biomedical Engineering (2012), M. Eng. in Mechanical Engineering (2016) and PhD in Mechanical and Mechatronics Engineering (2021) from Universidad Nacional de Colombia. She currently works as assistant researcher of GIBIR (Biomechanics and Rehabilitation Research Group) at Universidad Nacional de Colombia, Medellín, Colombia.
Email: vmposadap@unal.edu.co.

Appendix

Table S. I. Analysis of Variance for Max

Source	DF	Adj SS	Adj MS	F-Value	P-Value
Blocks	1	0,07468	0,07468	2,70	0,145
Software	1	0,22803	0,22803	8,24	0,024
Slices	3	0,80435	0,26812	9,68	0,007
2-Way Interactions	3	0,32995	0,10998	3,97	0,060
Software*Slices	3	0,32995	0,10998	3,97	0,060
Error	7	0,19381	0,02769		
Total	15	1,63082			

Table S. II. Analysis of Variance (y1 RMS)

Source	DF	Adj SS	Adj MS	F-Value	P-Value
Blocks	1	0,006348	0,006348	1,28	0,295
Software	1	0,022538	0,022538	4,54	0,071
Slices	3	0,026435	0,008812	1,78	0,239
2-Way Interactions	3	0,001082	0,000361	0,07	0,973
Software*Slices	3	0,001082	0,000361	0,07	0,973
Error	7	0,034737	0,004962		
Total	15	0,091140			

Table S. III. Analysis of Variance (Mean)

Source	DF	Adj SS	Adj MS	F-Value	P-Value
Blocks	1	0,022112	0,022112	4,86	0,063
Linear	4	0,036848	0,009212	2,02	0,195
Software	1	0,026847	0,026847	5,90	0,046
Slices	3	0,010001	0,003334	0,73	0,565
2-Way Interactions	3	0,001619	0,000540	0,12	0,946
Software*Slices	3	0,001619	0,000540	0,12	0,946
Error	7	0,031862	0,004552		
Total	15	0,092440			