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Parra Mena, Juan Carlos; Gallardo Vizuite, Erling Ricardo; Torres Peñaloza, Erick Damian
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Effect of the filling percentage on tensile strength in 3D desktop printing for different printing patterns, using a randomized design of experiments

(Efecto del porcentaje de relleno en la resistencia a la tracción en la impresión de escritorio 3D para diferentes patrones de impresión, utilizando un diseño aleatorio de experimentos)

Juan Carlos Parra Mena¹, Erling Ricardo Gallardo Vizúete¹, Erick Damian Torres Peñaloza¹

Abstract

The evaluation of the tensile strength of printed parts by means of fused deposition modeling (FDM) or fused filament fabrication (FFF) is essential, since parts whose resistance does not differ significantly depending on the percentage of filling used can be obtained, optimizing the use of the material. The present work details the analysis of polylactic acid (PLA) specimens manufactured according to ASTM D 638 with different percentages for the most commonly used filling patterns (Honeycomb, Octagram, Stars, Archimedean, Hilbert and Triangles). With the help of an analysis of variance and a design of experiments with a single factor, the appropriate percentages for printing parts according to the desired filling pattern are obtained.

Keywords

3D printing, Filling percentage, Filling pattern, PLA, Stress.

Resumen

La evaluación de la resistencia a la tracción de las piezas impresas mediante el modelado por deposición fundida (FDM) o la fabricación de filamentos fundidos (FFF) es esencial, ya que se pueden obtener piezas cuya resistencia no difiere significativamente dependiendo del porcentaje de relleno utilizado, optimizando el uso del material. El presente trabajo detalla el análisis de muestras de ácido poliláctico (PLA) fabricadas de acuerdo con ASTM D 638 con diferentes porcentajes para los patrones de relleno más comúnmente utilizados (Panal, Octagrama, Estrellas, Arquimedean, Hilbert y Triángulos). Con la ayuda de un análisis de varianza y un diseño de experimentos con un solo factor se obtienen los porcentajes apropiados para imprimir piezas de acuerdo con el patrón de llenado deseado.

Palabras clave

Impresión 3D, porcentaje de relleno, patrón de relleno, PLA, estrés.

1. Introduction

The 3D printing started in the 70's with the technological revolution started by Steve Jobs with the Apple brand and, at the same time, when Charles W. Hull invented a method of stereolithography (SLA) that was used for the production of mockups; this method is the prologue for the creation of 3D printers.

Currently, applications in this research area have increased, obtaining prototypes for the simulation of surgical interventions, production rehabilitation prosthesis, among others. (Ordoñez-Alemán, 2017). Funding modeling allows consumers to become creators, especially in the case of professionals. For example, an electronic engineer can create his own housings for the electronic equipment that he develops; an architect can create his models; a traumatologist can create and develop prosthesis; a mechatronic can create his robot prototypes, machines,

parts, mechanisms, converting 3D printers in tools that make real any object your creativity designs (Díaz Abad, 2016).

3D printers have the ability to make parts with different fill patterns, depending on the model and brand of the printer. However, these characteristics are rarely used properly since they are usually only limited to printing parts in the shortest time and with the least use of raw material (PLA) with 0 % filler, regardless of tensile strength of the final piece. In other cases, its used to print parts with 100 % fill printing, overriding the fill pattern setting. To determine the appropriate filling percentage, specimens are manufactured under ASTM D638 to be tested in order to obtain their maximum breaking strength, a variance analysis and a completely randomized block design with five treatments and three repetitions; this method doesn't considers the existence of a factor almost always unknown and hardly controllable, as the weather conditions during the test. With Basic Manual of the IBM SPSS Statistics software (González, 2009), the dedicated mathematical models for the type of analysis implemented are processed and the variability factor is compared with that obtained from Fisher's F table (Polished, 2012) in 95 % desired reliability function.

The work was based on research of Haid (2014), which considered rectilinear patterns, in both ABS and PLA, and the study by Álvarez, Lagos & Aizpun (2016), which studied hexagonal patterns in ABS, establishing the appropriate filling percentages based on Tensile strength Globally; the growth that 3D printing has experienced projects a growth of 184 % by 2021. In Ecuador this phenomenon is in full development due to the accessibility of this technology, but at the time of manufacturing parts there are uncertainties related to the configuration of the print parameters and the possibility to obtain a good tensile strength in the manufactured parts.

The results obtained in previous investigations are taken as starting parameters, but articulated to the prevailing atmospheric conditions in the city of Quito-Ecuador for six different filling patterns with PLA, with the purpose of contributing with 3D printing configuration parameters in our environment, which allow a good tensile strength compared to a solid piece, optimizing the use of material and printing time.

2. Materials and methods

This research takes into account that the unknown factor will directly influence the process. It will not be possible to have a complete control over the environment in which the specimens are printed, nor the weather conditions during the test. Within the design of completely randomized experiments (Montgomery, 2004) a null hypothesis is proposed: "The percentages and fill patterns have no relation to their tensile strength"; and an alternative hypothesis: "The fill percentages and patterns are directly related to the tensile strength of the specimens" to reach the best number of the filling percentage depending on the printing pattern used. The reliability for this study is 95 % and two study groups were considered: Group 1, with the patterns Hilbert, Triangular and Archimedean; Group 2, with the Stars, Honeycomb and Octagram patterns, with fill percentages shown in Table 1.

Table 1. Distribution of specimens according to the filling pattern

Pattern	Number of specimens manufactured and tested	Fill Percentages (Treatments)
Hilbert	15	25,40,60,80, 90
Triangular	15	25,40,60,80, 90
Archimedean	15	25,40,60,80, 90
Stars	15	30,40,60,80,90
Honeycomb	15	30,40,60,80,90
Octagram	15	30,40,60,80,90
TOTAL	90	

The chosen treatments for each group are based on the work carried out by Haid (2014) and Álvarez, Lagos & Aizpun (2016) who studied rectilinear and hexagonal patterns.

2.1 Characterization of PLA test specimens

The 3D printing of the specimens was done on the Prusa i3 MK2S printer, that has the technical features listed in table 2.

Table 2. Technical features of Prusa i3 MK2S

Print Area	(250 x 210 x 200) mm
Nozzle size	0.4 mm for 1.75 mm filament
Layer height	since 0,05 mm
Compatible materials	PLA, ABS, PET, HIPS, Flex
PLA extrusion temperature (min)	180°C

The most used material in 3D printing is the polylactic acid (PLA), which has similar properties to PET (Polyethylene Terephthalate), which is also used for beverage packaging. According to its properties, this material is used in many different industries such as food, chemical, plastic, textile, among others. The mechanical and physical properties of the PLA filament used as raw material are listed in Table 3. It must be considered that, at the time of PLA specimens manufacturing, the properties of the material may vary according to the color in which the tests are carried out (Wittbrodt & Pearce, 2015); for this study, a green color was used with the patterns corresponding to the group 1; the red color was used for the patterns corresponding to group 2.

Table 3. Physical and mechanical properties of PLA filament (ESUN)

Tensile strength	65 MPa
Viscosity	0.61 - 8.2 dL/g
Tension Module	3 - 4 GPa
Density	1.241 g/cm ³

According to Castillo, Llor, Muñoz, Naranjo, Padrón & Peralta (2016), the traction machine to be used complies with the ASTM D3039 design standard and has the technical features presented in the table 4; this machine allows to obtain the mechanical resistance to the traction of the PLA filament specimens, using the stress-strain graph according to Escobar & Escobar (2018).

Table 4. Technical specifications of tensile machine.

Supply source	120/220 VAC
Power	360 W
Range Temperature	(5 - 40) °C
Maximum Humidity	Up to 85 % (non condensing)
Load cell	100 Kg (980 N)

It is important to consider the conditions in which the specimens were printed and the tensile test is performed, as presented in Table 5. Three specimens of each percentage and fill pattern are printed following the research of Cazañas, San Miguel & Parra (2017), which indicates the appropriate sample size to perform such an analysis.

Table 5. Environmental conditions during the test

Altitude	2978 a.s.l.
Pressure	717.39 mbar
Environmental Temperature	13 °C - 24 °C
Humidity	30 % - 45 %

With the data obtained from the environment conditions and the technical specifications to be used, the specimens are sized to perform the stress tests. According to Navas, Reyes & Galván (2015), for any analysis involving the production of material an attempt should be made to prevent the environmental impact through recycling or technological improvements; in this case, all the material tested can be recycled.

2.2 Sizing and sketching of PLA specimens

The specimens of plastic materials fit to ASTM D638 (2008) type IV, for specimens with thicknesses less than or equal 4 mm, where the measures are established to be tested.

The specimen is sized in the Solidworks 2018 CAD software that, according to Juiña, Cabrera & Reina (2017), has a higher rating respect to others (see Figure 1). Once the drawing in 3D it's saved in *.STL format to be processed in the software Slic3r PE of the manufacturer of the 3D printer, the configuration of the type and percentage of filling begins.

Figure 1. General dimensions of the 3D specimens printed in PLA (thickness: 2 mm) CAD model (b) 3D print

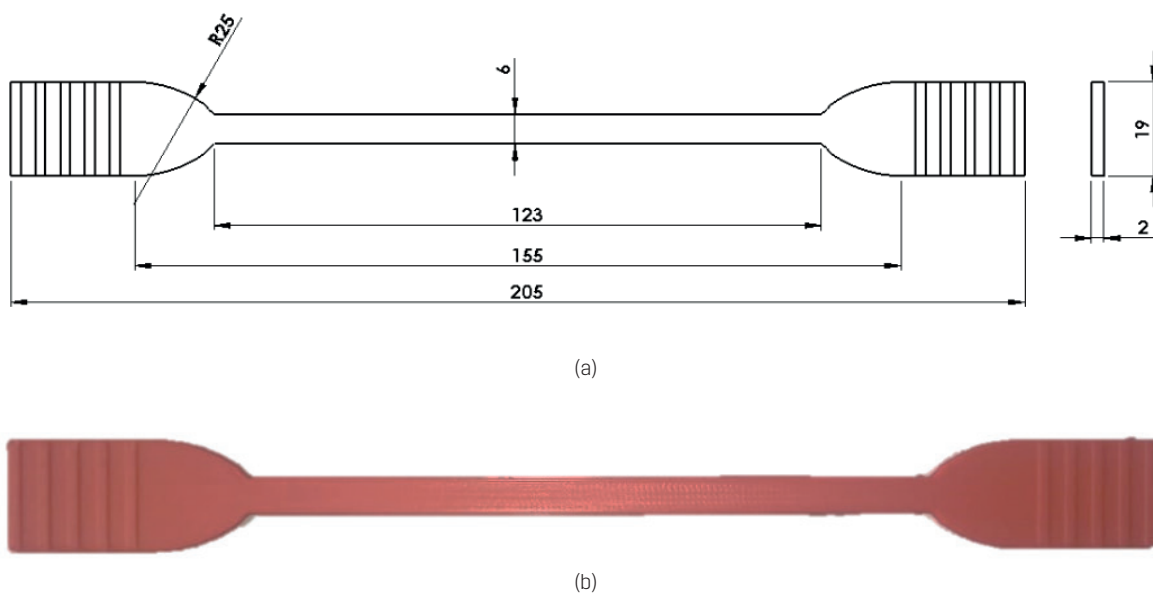
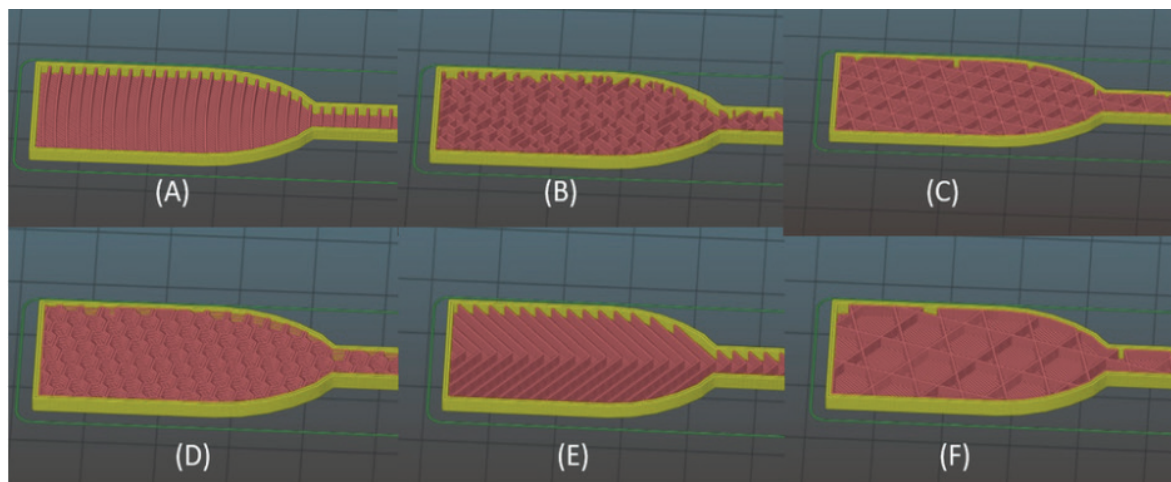


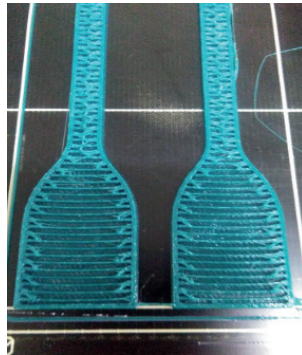
Figure 2 shows the different types of infill patterns used in the present investigation: Archimedean (A), Hilbert Curve (B), Triangular (C), Honeycomb (D), Octagram (E) and Stars (F).

Figure 2. 3D printing of different pattern types (Allevi, 2014)



A small part of the printing of specimens with the Archimedean, triangular, Honeycomb and Octagram patterns is presented on figure 3.

Figure 3. Printed specimens (a) Archimedean with 60 % infill (b) Triangular with 40 % infill (c) Honeycomb with 80 % infill (d) Octagram with 70 % infill



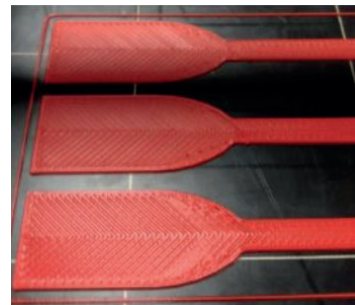
(a)



(b)



(c)



(d)

3. Results

To identify values that differ or aren't significantly from each other, the analysis of variance of a completely randomized block design is carried out by means of Table 6 (Montgomery, 2004), using the data obtained by the tensile test; subsequently, with the SPSS Statistics software, validation tests of the statistical data are carried out to verify the information obtained and find the Fisher value calculated F_0 .

Table 6. Variance for a completely randomized block design

Source of variation	Sum of squares	Freedom Degrees	Middle square(M)	F_0
Treatments	SS_{Tr}	$I - 1$	$(SS_{Tr}) / (I - 1)$	MSS_{Tr} / MSS_E
Error	SS_E	$(I - 1)(J - 1)$	$(SS_E) / (I - 1)(J - 1)$	-
Total	SS_{TT}	$N - 1$	-	-

Treatment equations for the sum squares (1), total (2) and error (3) are presented based on the mechanical strength data of the three repetitions in all the analyzed treatments (patterns, fill percentages and number of repetitions), located as shown in Table 7.

Table 7. Fully randomized block design (Pérez, 2014)

Treatments	Blocks					
	1	2	...	<i>j</i>	...	<i>J</i>
1	y_{11}	y_{12}	...	y_{1j}	...	y_{1J}
2	y_{21}	y_{22}	...	y_{2j}	...	y_{2J}
\vdots	\vdots	\vdots	\vdots	\vdots	\vdots	\vdots
<i>i</i>	y_{i1}	y_{i2}	...	y_{ij}	...	y_{iJ}
\vdots	\vdots	\vdots	\vdots	\vdots	\vdots	\vdots
<i>I</i>	y_{I1}	y_{I2}	...	y_{IJ}	...	y_{IJ}

$$SS_{Tr} = \frac{1}{j} * \sum_{i=1}^I y_i - \frac{Y_{..}^2}{N} \quad (1)$$

Where

SS_{Tr} : Sum of treatment squares

j : Column position

i : Row position

I : Total rows

y_i : Value according to row

$Y_{..}$: Sum of all the values obtained in the tests

N : Multiplication of total columns by total rows

$$SS_{TT} = \sum_{i=1}^I \sum_{j=1}^J y_{i,j}^2 - \frac{Y_{..}^2}{N} \quad (2)$$

Where

SS_{TT} : Sum of the squares of the total

I : Total rows

J : Total columns

i : Row position

j : Column position

$y_{i,j}$: value according to row and column

$Y_{..}$: Sum of all the values obtained in the tests

N : Multiplication of total columns by total rows

$$SS_E = SS_{TT} - SS_{Tr} \quad (3)$$

Where

SS_E : Sum of error squares

SS_{TT} : Sum of squares of the total

SS_{Tr} : Sum of treatment squares

The tensile test of the specimens with patterns and percentages of filling is carried out; the data obtained by the test is presented in Tables 8, 9, 10, 11, 12 and 13, while in Figures 4, 5, 6, 7, 8 and 9 the data is displayed graphically. It is taken into account that the test specimens can be used for additional studies within the same analysis, considerably reducing the cost of the study (Tamayo, Pazmiño, Valencia, Galván & Batista, 2015).

Table 8 shows the tensile strength values of the specimens with an Archimedean pattern.

Table 8. Tensile strength (Mpa) of specimens with an Archimedean pattern

Treatments	Specimen 1	Specimen 2	Specimen 3
25 %	20,505	19,985	20,072
40 %	28,519	28,148	28,460
60 %	29,465	30,572	29,307
80 %	24,366	24,957	24,475
90 %	27,018	27,957	24,475

Figure 4 shows the values of table 8 in graphical form; it is evident that the highest tensile strength occurs with a 60 % fill.

Figure 4. Graphical representation of the data in table 8

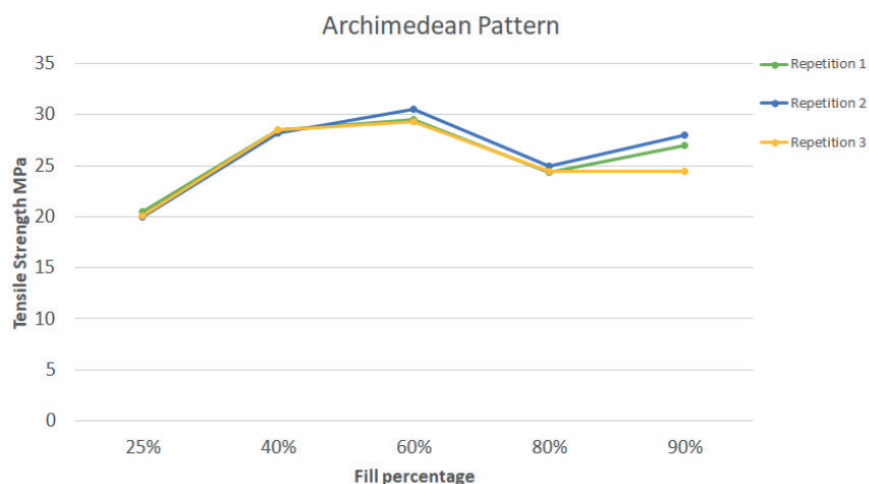


Table 9 shows the tensile strength values of the specimens with a Hilbert curve pattern.

Table 9. Tensile strength (Mpa) of specimens with Hilbert curve pattern

Treatments	Specimen 1	Specimen 2	Specimen 3
25 %	22,433	23,001	23,101
40 %	27,837	27,812	27,494
60 %	33,772	33,412	33,800
80 %	33,578	31,055	36,938
90 %	26,576	26,621	26,601

Figure 5 shows the values of table 9 in graphical form;; it is evident that the highest tensile strength occurs with an 80 % fill.

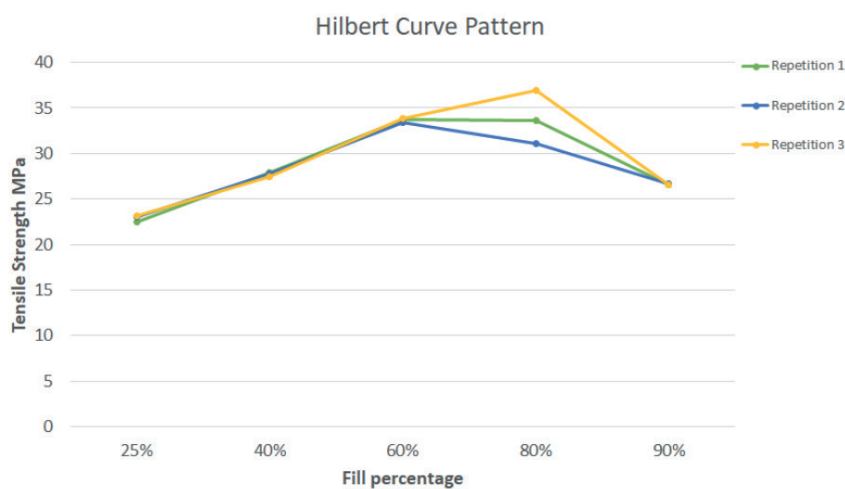
Figure 5. Graphical representation of the data in table 9

Table 10 shows the tensile strength values of the specimens with a Triangular pattern.

Table 10. Tensile strength (Mpa) of specimens with Triangular pattern

Treatments	Specimen 1	Specimen 2	Specimen 3
25 %	31,274	31,249	31,575
40 %	25,618	25,905	25,551
60 %	45,065	43,840	45,724
80 %	39,279	43,185	39,823
90 %	31,196	31,223	31,271

Figure 6 shows the values of table 10 in graphical form;; it is evident that the highest tensile strength occurs with a 60 % fill.

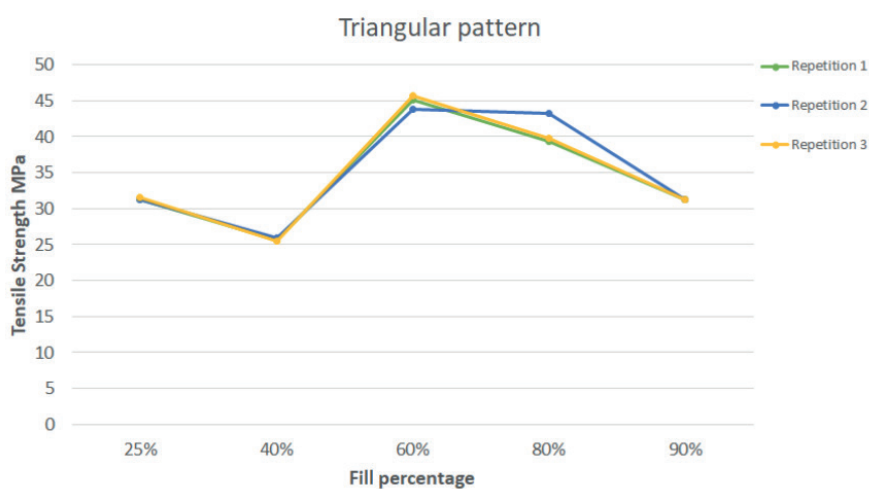
Figure 6. Graphical representation of the data in table 10

Table 11 shows the tensile strength values of the specimens with a Honeycomb pattern.

Table 11. Tensile strength (MPa) of specimens with Honeycomb pattern

Treatments	Specimen 1	Specimen 2	Specimen 3
30 %	25,650	19,206	15,852
40 %	43,348	52,780	65,667
60 %	52,639	40,350	50,258
80 %	29,990	27,561	31,368
90 %	30,358	32,220	32,416

Figure 7 shows the values of table 11 in graphical form; it is evident that the highest tensile strength occurs with a 40 % fill.

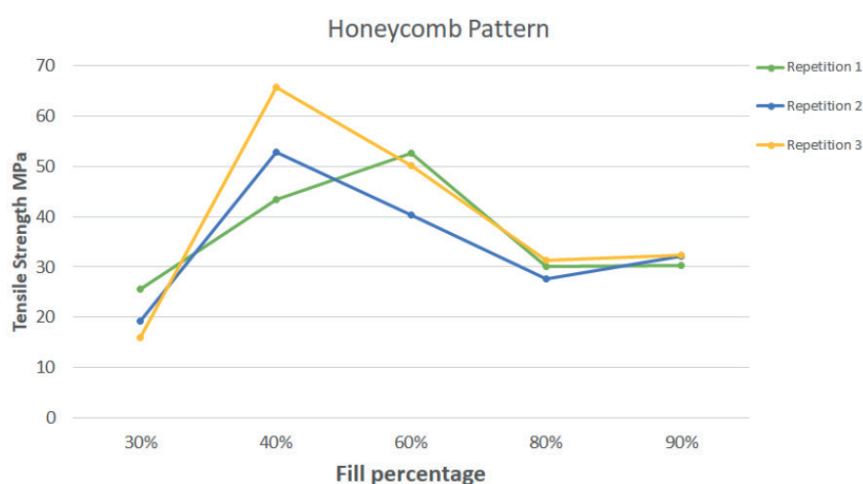
Figure 7. Graphical representation of the data in table 11

Table 12 shows the tensile strength values of the specimens with an Octagram pattern.

Table 12. Tensile strength (Mpa) of specimens with Octagram pattern

Treatments	Specimen 1	Specimen 2	Specimen 3
30 %	32,223	27,314	21,159
40 %	13,583	20,437	16,548
60 %	14,233	16,406	18,739
80 %	24,598	29,770	26,013
90 %	30,208	25,360	27,254

Figure 8 shows the values of table 12 in graphical form; it is evident that the highest tensile strength occurs with a 30 % fill.

Figure 8. Graphical representation of the data in Table 12

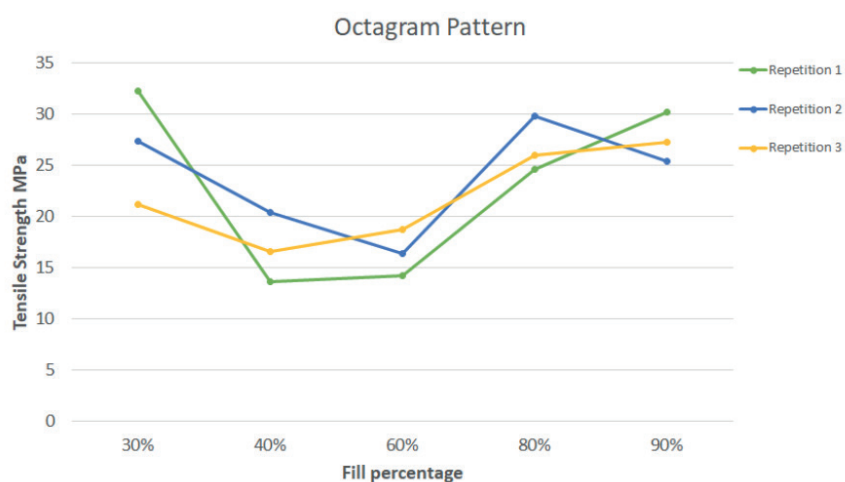


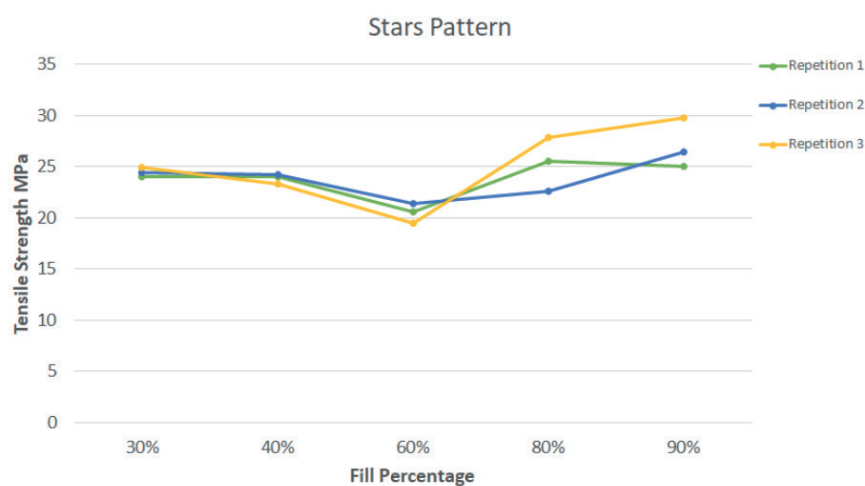
Table 13 shows the tensile strength values of the specimens with a Stars pattern.

Table 13. Tensile strength (Mpa) of specimens with Stars pattern

Treatments	Specimen 1	Specimen 2	Specimen 3
30 %	24,050	24,452	24,965
40 %	24,014	24,201	23,322
60 %	20,618	21,360	19,517
80 %	25,493	22,647	27,835
90 %	24,997	26,406	29,815

Figure 9 shows the values of table 13 in graphical form; it is evident that the highest tensile strength occurs with a 90 % fill.

Figure 9. Graphical representation of the data in table 13



The variance analysis for triangular pattern is performed in the IBM statistics SPSS software, and the results are presented in the table 14; the work with the other patterns proposed in the present study are developed in a similar way. Chart 15 shows the results of the triangular pattern obtained on SPSS Statistics software.

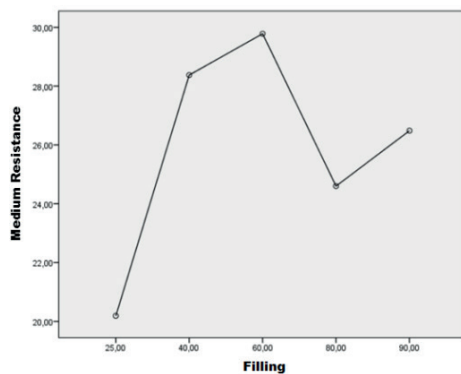
Table 14. ANOVA result using the SPSS Statistics software for the triangular pattern

	Sum of squares	Degrees of freedom	Middle square (M)	F	Sig.
Between groups	733,785	4	183,489	167,992	.000
Within groups	10,920	10	1,092	-	-
Total	744,677	14	-	-	-

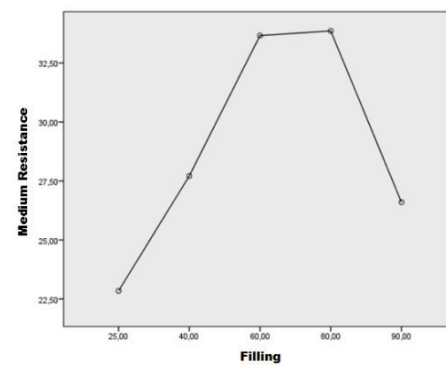
Finally, a statistical summary is presented using means graphs of each type filled; these graphs are presented in figures 10, 11 and 12.

Figure 10 shows the statistical means obtained for the Archimedean patterns and Hilbert curves.

Figure 10. Statistical summary patterns: (a) Archimedean and (b) Hilbert



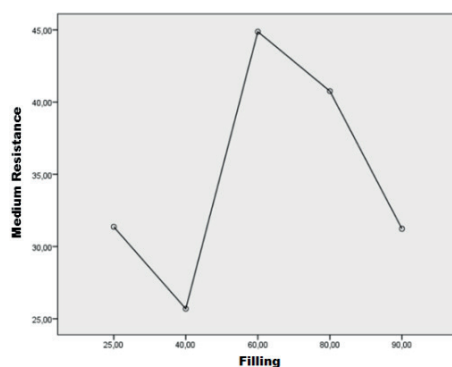
a)



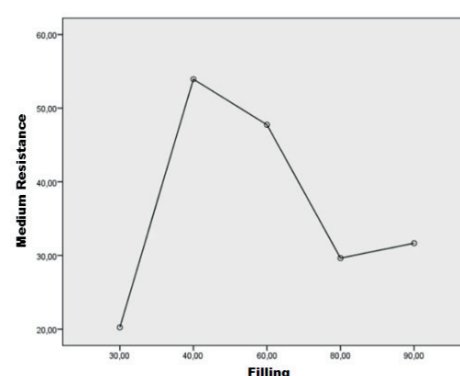
b)

Figure 11 shows the statistical means obtained for the Triangular and honeycomb patterns.

Figure 11. Statistical summary patterns: (a) Triangular and (b) Honeycomb



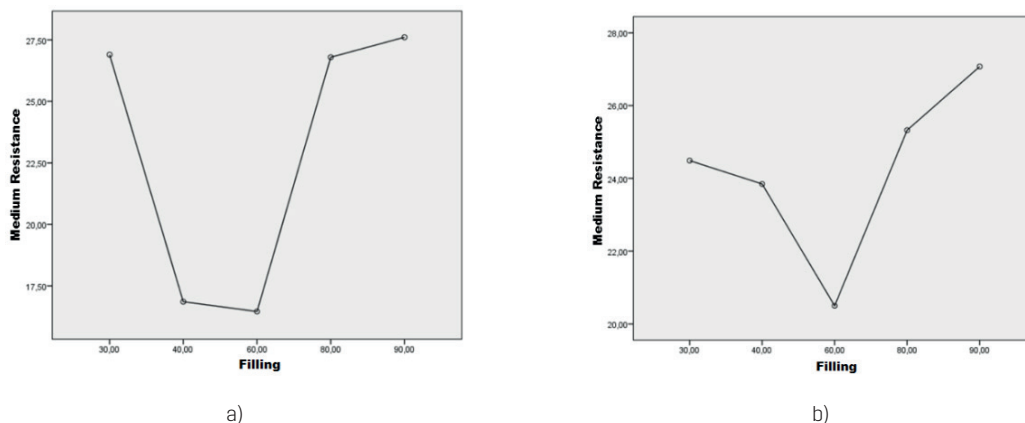
a)



b)

Figure 12 shows the statistical means obtained for the Octagram and Stars patterns.

Figura 12. Statistical summary patterns: (a) Octagram and (b) Stars



In the ANOVA results showed in Table 14, it was determined that the null hypothesis raised is rejected and the alternative hypothesis, "the percentages and filling patterns are directly related to the tensile strength of the specimens", is accepted, with in a 95 % confidence. In addition, using the Tukey statistical test, it was determined that filling percentages do not differ significantly, choosing the lowest for each filling pattern as the most appropriate to guarantee good tensile strength with the least use of material, as presented in Table 15.

Table 15. Recommended percentages of filling according to the pattern used for an acceptable mechanical tensile strength with 95 % confidence

Pattern	Percentage
Archimedean	40 %
Hilbert	40 %
Triangular	25 %
Octagram	30 %
Honeycomb	40 %
Stars	30 %

4. Discussion

The experimental tensile tests on PLA specimens reflect a similar behavior in terms of percentage of filling and type of pattern. According to Haid (2014), a graph of means between the two mentioned considerations, approximately in a range between 20 to 30 %, of a rectilinear filling pattern, does not have a significant difference respect to a 100 % test that, according to Fernández, Calle, Ferrandiz & Conejero (2016), has a similar value. It should be noted that in this research 6 different types of filling are compared. Choosing an optimal percentage for each one of them relates to their tensile strength.

According to Álvarez, Lagos & Aizpun (2016), comparisons are made between tensile strength, fill percentage and printing time, where the information is related to the average tensile strength and various fill percentages of the hexagonal pattern; by visual inspection it is determined that there is no significant difference between approximately 25 and 40 %. It also ensures that the printing time is shorter if the fill percentage decreases.

According to Molina, Pender, Moro & Piovan (2018), when setting the temperature conditions when it is printing, it is possible to obtain the maximum creep resistance. By means of thermofluence tests they conclude that when stresses greater than 20 MPa are applied, significant decreases are evidenced of mechanical resistance; however, the atmospheric conditions must be considered, so that the mechanical properties obtained are met.

The percentages obtained for each filling pattern studied in the city of Quito are in ranges from 25 % to 40 % for specimens made with PLA, depending on the pattern used. The alternative hypothesis is confirmed: "the tensile strength if it depends on the percentage of filling" and the value of the tensile strength corresponding to the identified percentage does not differ significantly with the high value of tensile obtained in the respective tests.

5. Conclusions and Recommendations

With this research it is possible to compare results between several types of 3D printing patterns, as well as different fill percentages. And by means of a variance analysis, the appropriate fill percentages have been determined for the conditions stipulated in the study and for each analyzed pattern.

The data obtained from ultimate tensile strength may differ from other tests due to the type of 3D printer, the printing parameters, as well as the weather conditions and even the brand of the filament used, both for printing of the specimens and for the test of these; however, the statistical procedure performed will allow to determine the appropriate percentages based on the tensile strength obtained.

The use of Octagram, Triangular and Star patterns within the conditions presented in the investigation (Table 15) to reduce the use of material in prints without damaging their tensile strength it is recommended.

6. Collaborations

The following people supported and contributed during the stress tests carried out in this work: Juan Ullauri, Lenin Pasaca, Stefano Buitrón, Eduardo Urresta, Ángel Enriquez, David Racines, Mauricio González, Martín Flor and Estefanía Suasti.

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