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Cálculo de parámetros cinéticos en reacciones foto-catalíticas usando un modelo efectivo de campo de radiación

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Resumen

En este estudio se evaluó el efecto de la geometría y la concentración de sustrato en la determinación de rendimientos cuánticos globales del proceso. Los rendimientos cuánticos se obtuvieron bajo un enfoque de parámetros globales constantes, fundamentados en las propiedades isotrópicas del campo radiante y de distribución perfecta de partículas en la fase fluida. Se usó un modelo idealizado para la cuantificación del campo de radiación y las expresiones matemáticas para la velocidad de reacción y la energía global efectiva absorbida del proceso (OVRPA) por medio de una solución aproximada de la ecuación de transferencia radiativa (RTE). Los resultados obtenidos para los rendimientos cuánticos permitieron mostrar la naturaleza no intrínseca de los parámetros cinéticos por la fuerte influencia de la geometría asociada a la dependencia con la energía radiante global absorbida por el sistema, evaluando estos parámetros foto-cinéticos a concentración inicial de ácido dicloroacético (DCA) constante. El error relativo global es menor al 2.5% y los coeficientes de correlación son mayores a 0.97 entre los datos de simulación y los datos experimentales utilizados.

Palabras Clave: Acido dicloroacético, Rendimientos cuánticos no intrínsecos, Campo de radiación efectiva, Velocidad volumétrica global de absorción de fotones.

Calculation of kinetics parameter on photo-catalytic reactions using an effective radiation field model

Abstract

This study assessed the effect of the geometry and concentration of substrate in the determination of overall quantum yields. The quantum yields were obtained under an approach of constant global parameters based on the properties of isotropic radiant field and perfect distribution of particles in the fluid phase. An idealized model for quantifying the radiation field was used for reaction rate and overall volumetric rate of photon absorption (OVRPA) were obtained by means of an approximate solution of the radiative transfer equation (RTE). The results for quantum yields allowed to show the non-intrinsic nature of the kinetics parameters because of the strong influence of geometry associated to the dependence on the radiant energy absorbed by the system, evaluating these photo-kinetic parameters at constant initial concentration of dichloroacetic acid (DCA). The overall relative error between the simulation and experimental data is less than 2.5% and the correlation coefficients are greater than 0.97.

Keywords: Dichloroacetic acid, Non-intrinsic quantum yields, Effective radiation yield, Overall volumetric absorption photon rate.

1. Introduction

The heterogeneous photocatalytic processes are strongly influenced by four key components: system reactive (substrate), catalyst (semiconductor), geometry reactor (reactor type) and radiation field (luminous flux). The geometry and radiation field introduce a no-intrinsic nature to this type processes (reflected in kinetic of reaction rate), these characteristics are the major differences with the conventional chemical processes (Alfano & Cassano, 2009; Braham & Harris, 2009; Liu & Zhao, 2010; Herrmann, 2010).

The performance of photocatalytic process depends critically on the amount of incident radiation that can be used to activate the catalyst particles and therefore it requires a correct quantification of the volumetric rate of energy absorption (VREA). This in turn will allow an adequate description of the kinetic parameters such as quantum yields (Sagawe et al., 2010; Machuca et al., 2008; Kuhn et al., 2004).

This parameter has been used in various studies of photocatalytic reaction. For the evaluation of different materials, in monitoring the photocatalytic reactions of pure compounds and mixtures, follow up the production of OH radicals, in modeling and evaluation of photoreactors, scaling of processes and reactors (Egerton and Mattinson, 2010; Liu and Zhao, 2010; Li Puma et al., 2010; Serrano et al., 2009; Siamak & Fariborz, 2010; Zhang and Anderson, 2010).

Several substances have been proposed for the calculation of quantum efficiency, there are found from pure substances to complex mixtures; e.g., pesticides, endocrine disrupting chemicals and microorganisms. Among the more pure substances used are phenol and its derivatives, ethanol, inorganic and organic substances and the dichloroacetic acid (Ballari et al., 2010; Egerton and Mattinson, 2010; Sagawe et al., 2010; Trujillo et al., 2010).

In particular, the DCA has been implemented as a key component of heterogeneous actinometry and/or model substance for kinetic studies of heterogeneous photocatalytic systems, due to the

simplicity of the stoichiometric equation and simple experimental tracking, as well as its physical and chemical properties that allow it to be considered a valid chemical actinometer for heterogeneous photodegradation reactions (Zalazar et al., 2005; Machuca et al., (2008); Ballari et al., 2010).

The importance of assessing the quantum yields as comparison parameters is established by the nature of the induction processes of electron hole (e⁻)/(h⁺) pairs at the semiconductor/solution interface, where the reaction rate in the primary stage of the catalyst excitation is considered as the quantum yield of the process, Rothenberger (1985), Serpone (1997).

Nevertheless, the conventional definition of quantum yield used in heterogeneous photocatalysis (which relates the number of moles processed per unit of absorbed energy by the photochemical semiconductor), Serpone (1997), is strongly associated to reference states that are obtained by homogeneous actinometry leading to apparent quantum yield parameters in order to extrapolate results from simple systems to complex reaction mixtures, while retaining the same geometry reaction, Zalazar et al. (2005), Brandi et al. (2003), Trujillo et al. (2010).

The quantum yields obtained by this route are usually calculated by adjusting experimental data from simple actinometric reactions, coupled to a solution of the radiative transfer equation, Duderstadt (1979), resulting in values that are not necessarily unique to the reaction system, i.e. non-intrinsic quantum yields, due to the heavy dependence of the radiant field for constant flow of photons, in relation to the geometry of the system. So, the evaluation of the global quantum yield and the overall volumetric rate of photonic adsorption can be made by fitting results of heterogeneous actinometrical experiments or using an appropriate phase field model coupled with the RTE. (Machuca et al., 2008, Mueses et al. 2008).

Among the least studied variables in heterogeneous photocatalytic reaction in determining the quantum yield is the type of reactor and the effect of substrate concentration.

This keys components, into all heterogeneous photocatalytic processes, have been evaluated in previous investigations, Blanco et al. (2001), Brandi (2003), Dijkstra et al. (2003), Bandala et al. (2004), Mueses (2008), where overall photodegradation conversion have been assessed in irradiated reactors with direct and diffuse solar or artificial polychromatic radiation at low concentrations of substrate in different reaction systems but no related with the quantum and photonic parameters.

However, few studies have been reported with comparative theoretical and experimental evidence that differentiate the significance of these two effects (concentration and geometry) and that assess the parameters of photo-kinetic reactions, as quantum yields and rate of photon absorption, by means of the evaluation of a single reaction system in different geometrical configurations, Bandala et al. (2004), Brucato et al. (2007), Alfano & Cassano (2009).

This paper aims to show the effect of geometric configuration and the initial concentration of substrate for three reaction systems (compound parabolic collector - CPC, tubular, and axial) on quantum yields using a new model of radiation field and the data from actinometrical heterogenous reaction.

2. Mathematical model

Machuca et al. (2008) have proposed a model for calculating photo-kinetic parameter based on a methodology of isotropic global parameters, quantum yield (Φ_g) and overall volumetric rate of photon absorption OVRPA (E_g^a). This model was validated from the DCA photocatalytic degradation data in a differential perfect-mixture reactor. The effective radiation field model (ERFM) used in this study is based on the modification of the RTE equation assuming an isotropic field, the conceptual basis of the model without the mathematical rigor was published partially by Mueses and Machuca (2010b).

The formulation of the constituent equations of the system supports the following general considerations without breaking the basic principles of photocatalysis, Herrmann (2010):

Isothermal and isobaric system, heterogeneous system with isotropic distribution of perfect mix, fluid + particles, effective radiation field with constant energy, monochromatic radiation, constant optics and isotropic absorption properties, No radiation absorption in the fluid phase, heterogeneous photocatalytic reaction controlled by the primary stage of the semiconductor excitation and light scattering effects with function of isotropic phase.

The global structure of systems include the reaction rate model for DCA, mass balance for the reactors, radiative energy balance from the absorption model, effective radiation model from emission model, and the OVRPA. In forthcoming publications an extension and validation of mathematical development will be made.

2.1 Reaction rate model

For this study, it uses the DCA photocatalytic degradation as model reaction. Zalazar et al. (2005) proposed a mechanism and an expression of reaction rate for the DCA photodegradation based on the direct attack by the holes (h^+) generated during the activation of the catalyst, towards the dichloroacetate ion ($CHCl_2COO^-$). In a previous work, Machuca et al. (2008), the expression of reaction rate was modified in terms of overall quantum yield (Φ_g) and the overall volumetric rate of photon absorption (E_g^a). The resulting expression is shown in equation (1):

$$R_{DCA} = \frac{2\Phi_g E_g^a}{1 + \left[1 + \frac{\beta}{C_{DCA}}\right]^{\frac{1}{2}}} \quad (1)$$

$$\beta(K_{Obs}, \Phi_g) = \beta = 2 \frac{K_{Obs}}{C_{Cat}^2 C_{O_2}} \Phi_g E_g^a \quad (2)$$

Where (K_{cat}, Φ_g) is a function of photocatalytic kinetic parameters, K_{cat} is an adjustment kinetic parameter, C_{DCA} is the concentration of DCA, C_{O_2} is the oxygen concentration, and C_{cat} the catalysts concentration.

2.2 Mass balance: the generating equation

The material balance is independent of the geometry of the evaluated reactors. The resulting expression for batch systems is an integer-differential function as shown in equation (3):

$$\left. \frac{dC_{DCA}}{dt} \right|_n = -2 \left(\frac{1}{v_r} \right) \int_0^{v_R} \frac{\Phi_g E_b^a}{1 + \left[1 + \frac{\beta}{C_{DCA}} \right]^{\frac{1}{2}}} dv \quad (3)$$

Where T_R refers to the volume of the absorber, v_r is the system total volume, and v_R is the reaction volume.

The isotropic nature of the kinetic parameters, the concentration of reagents and catalyst particle distribution, implies that equation (3) does not depend on the volume of the reactor, and becomes a non-linear ordinary differential equation depending on the concentrations of reactive species and time. The functional form of the solution is given by (4):

$$C_{DCA} + \sqrt{C_{DCA}(C_{DCA} + \beta)} + \frac{\beta}{2} \ln \left\{ (C_{DCA} + \beta) + \sqrt{C_{DCA}(C_{DCA} + \beta)} \right\} - f(C_{DCA,0}) = -2 \left(\frac{v_R}{v_r} \right) \Phi_g E_b^a t \quad (4)$$

Where $f(C_{DCA,0})$ is the solution evaluated at the initial condition ($t=0$). Equation (4) is the generating equation, which links the concentration of DCA depending exclusively on time and has only two adjustable parameters from experimental data: the overall quantum yield and the K_{cat} constant.

2.3 Radiative energy balance

The radiation field properties can be defined under the foundations of Cassano et al. (1995) and through the use of the one-dimensional equation of radiative transfer, modified to an isotropic effective radiation field with constant energy I_N . Mathematical procedure in detail was developed by Mueses (2008), Mueses and Machuca (2010b).

The independent RTE equation of the geometry of the reactor is:

$$\frac{dI_N}{ds} + [\kappa_v + \sigma_v] I_N - \frac{\sigma_v}{4\pi} I_N \int_{\Omega=4\pi} \rho(\vec{\Omega} \rightarrow \vec{\Omega}') d\Omega' \quad (5)$$

Where I_N is the net incident radiation energy on the semiconductor particles, κ_v , σ_v are the volumetric absorption and scattering coefficients, Cassano et al. (1995): The integral term is a function of elastic scattering and s is the geometry reference coordinate: r for tubular reactor radio and z for axial configuration, Alfano et al. (1995)

2.3.1 Effective radiation field

The energy radiation field can be calculated by applying the following assumptions: (i) it is possible to redistribute the total energy Φ_g of an incident photon flux on an energy absorber in a constant energy field (energy pit), $\Phi_{g,T}$ which surrounds isotropically the element of absorption, regardless of the direction and spreading frequency and (ii) the radiant field inside the reactor remains isotropic nature and is spread evenly throughout the system volume. Similar concepts were used by Ballari et al. (2010) in the study of the mass transfer limitations in slurry photocatalytic reactors, and Sagawe et al. (2010) in the analysis of photoreactors by observed photonic efficiency.

In particular, the total effective radiant energy in a cylindrical absorber with absorption surface area $S_A = S_H^i + S_L^i$ with S_H^i and S_L^i as the directly illuminated surface by a radiating source and the not illuminated surface respectively can be estimated using the following equation:

$$\int_{S_H} \zeta_F(\mathbf{x}, \Omega) d(S_H^I) = \int_{S_A} I_N d(S_A) = I_N \int_{S_A} d(S_A) \quad (6)$$

Now, considering the emission source and following the tenets for modeling lamp emission proposed by Cassano et al. (1995), the net radiation energy field entering the absorber is expressed as follows:

$$I_{N,0} = \zeta_{F,T} = \frac{A^{eff}}{\pi^2 D_L L_L (\lambda - \lambda_0)} \int_{\lambda} \eta_L P_{\lambda} Y_R d\lambda \quad (7)$$

Where A^{eff} is proposed as the quotient between the illuminated area S_H^I and the total absorption area S_A ; D_L , L_L and L correspond to the diameter, length and total number of radiation lamps respectively; $(\lambda - \lambda_0)$ is the lamp wavelength operating range, P_{λ} is the photochemical power of the lamps and Y_R is the transmittance coefficient of the wall of the absorber.

Therefore, this approach can be applied without homogeneous actinometry requirements for estimating overall quantum yields, coupled with the concept of heterogeneous actinometry and models for the radiation field.

2.3.2 OVRPA calculation and net absorbed energy

In mathematical terms, the overall volumetric rate of photon absorption can be defined as the integration throughout the volume of reaction of the product between the semiconductor volumetric absorption coefficient and the net incident energy (by analogy with the volumetric local rate of photon absorption, LVRPA), as shown by equation (8):

$$E_g^a = \frac{1}{V_R} \int_V \kappa_v I_N(\nu) dV \quad (8)$$

The net effective energy absorbed by particles of catalyst can be estimated from the solution of the RTE equation (equation 5) with a function of isotropic phase with elastic scattering and

considering also an adimensional function of fraction of absorbed radiation, defined by equation 9:

$$\phi_N^{eff} = \frac{E_g^a}{E_{g,0}^a} = \frac{1}{V_R} \int_V I_N^{eff}(\nu) dV \quad (9)$$

With:

$$I_N^{eff}(\nu) = \frac{I_N}{I_{N,0}} \quad (10)$$

Where I_N^{eff} is the net energy absorbed by the semiconductor particles in the volume of reaction, $I_{N,0}$ is the total net isotropic energy at the entrance of the reactor and $E_{g,0}^a$ is the overall volumetric rate photon absorption on the wall of the reactor.

The equations of the model can be transformed by consideration of an adimensional variable χ of effective length. For tubular reactors with radial configuration is defined by equation (11) and axial by equation (12):

$$\chi = 1 - \frac{r}{\xi} \quad (11)$$

$$\chi = \frac{z}{\xi} \quad (12)$$

With ξ is the total radio R of the absorber for radial tubular, and length L for axial configurations.

The solution of the RTE equation and the implementation of equations (9) to (12) generate the following expressions for evaluating the overall absorbed fraction in all three geometric configurations:

For radial-tubular reactors:

$$\phi_N^{eff}(\chi) = 1 + 2 \sum_{n=1}^{\infty} \frac{(-1)^n}{(\kappa, \xi)^n} \left[1 - (1 - \chi)^{\frac{n+1}{2}} \exp(-\kappa, \xi \chi) \right] \quad (13)$$

For cylindrical-axial:

$$\phi_N^{eff}(\chi) = 1 + \frac{1}{(\kappa_v \xi)} \exp(-\kappa_v \xi \chi) \quad (14)$$

Both expressions are governed by the general boundary condition:

$$\chi = 0 \rightarrow \phi_N^{eff} = 1 \quad (15)$$

2.4 Generalized scheme solution

The generating function (equation 4) has two adjustable parameters that can be obtained through experimental photodegradation data, Mueses (2008). A generalized method of non-linear least squares was used to obtain the values of overall quantum yield Φ_g and the adjustment constant K_{obs} . The method uses a Broyden type modification of the generalized Newton-Raphson method coupled to a new concept of "non-negativity of the quantum yield", this new concept restricts the method to positive values but lower than unity in the overall quantum yield, Broyden (1965), Mueses & Machuca (2010a).

The value of the initialization parameters was determined from a modified method of initial velocity, Wold (1993), in conjunction with the reaction rate equation (equation 1). The expressions obtained are shown in equations 16 and 17:

$$\Phi_g^{(0)} = \frac{1}{E_g^a} \lim_{t \rightarrow 0} [\langle R_{DCA} \rangle_R] \quad (16)$$

$$K_{obs}^{(0)} = \lim_{t \rightarrow 0} [\tau = \langle R_{DCA} \rangle_R - R(K_{obs})] \quad (17)$$

Where $\langle R_{DCA} \rangle_R$ is the average reaction rate in the reactor and τ is a function of the discrepancy between the initial average reaction rate and the evaluation of the expression of reaction rate $R(K_{obs})$.

3. Results and discussion

To study the geometry effect and initial concentration in the DCA photodegradation, experimental data reported previously were considered, Mueses et al. (2008). This paper shows in detail, obtaining experimental data for three lab-scale reactors with UV radiation and using P-25 Degussa TiO_2 . Summarizing the previous work, a CPC reactor, a tubular and a cylindrical-axial reactor were evaluated. The CPC and tubular reactors were of equal size and radial configuration of radiation entrance (except for collectors); the axial reactor was smaller and was named that way because the incident radiation comes lengthwise through the axial axe of the container. The optical properties of the semiconductor (titanium dioxide), volumetric absorption coefficient and volumetric scattering coefficient, were taken from Cabrera et al. (1996) and the transmittance coefficient of the material of the reactor was taken from Alfano et al. (1995).

The implementation of the scheme solution allows obtaining overall quantum yields and the adjustment constant, for any substance under heterogeneous photocatalytic reaction. For the DCA, the photodegradation in all three reactors was evaluated at different initial concentration of substrate, those results are presented in Table 1.

The obtained quantum yields are positive and less than unity, consistent with the physical restraint of the conventional definition (Serpone, 1997) and the concept of non-negativity of quantum yield (Mueses & Machuca, 2010a), without breaking the fundamental principles of catalysis (Herrmann, 2010). But its order of magnitude is low and possibly attributed to the type of radiation and its photochemical power.

The results can be explained as follows: the behavior of quantum yield may be due to the electron flow goes from the DCA to TiO_2 . Then, assuming that the reaction started after reaching adsorption equilibrium, increasing the initial concentration of DCA increases the amount of molecules adsorbed on the surface, so that more holes are stabilized by electrons from the DCA, so it oxidized and increases increasing performance

Table 1. Quantum yields and adjustment constants for different reactors and initial concentration

Reactors	[DCA] ₀ ppm	$\Phi_g \times 10^3$ (mol·Eins ⁻¹)	$K_{Obs} \times 10^{10}$ (mol·min ⁻¹ ·s ² ·cm ⁻³)
CPC	120	3.48679	5.4181
	60	3.26716	5.0906
	30	1.54054	9.9063
Tubular	120	2.45819	3.6354
	60	1.97430	4.5075
	30	1.34513	4.3931
Axial	120	0.39367	20.275
	60	0.39517	10.124
	30	0.24126	21.305

degradation and therefore the quantum yields. Additionally, it is likely that the free electrons in the conduction band of TiO₂ leading to the formation of superoxide radical (O₂^{-•}) and these could increase the oxidation of DCA.

The emission system of the reactors has high photochemical power but low-energy incident photons. The wavelength of radiation of the lamps is 365 nm (near the upper limit of UV). The energy of the incident photons is close to the optical absorption barrier of the semiconductor (P-25 Degussa TiO₂), significantly below 385 nm (Wold, 1993; Siamak and Fariborz, 2010), but near the band gap of the semiconductor.

The forbidden band-gap energy E_{gap}^+ should be lower than the radiated energy on the catalyst particle $h\nu$ so the photocatalytic process can be physically possible, thus ensuring a high efficiency in generating electron-hole pairs (Serpone, 1997; Brucato and Rizzuti, 1997). The semiconductor has a bandwidth $E_{gap}^+ = 3.2$ eV (5.126710×10^{-19} J) and the energy value at 365 nm is $5.4423210 \times 10^{-19}$ J, therefore $h\nu_{365nm} > E_{gap}^+$. This indicates that the semiconductor activation is promoted at 365 nm, and its low energy due to the closeness of $h\nu_{365nm}$ and E_{gap}^+ . Because of the proximity of these

two energies, fluctuations in the luminous flux can be despised, Zhang and Anderson (2010), being only the geometry and initial concentration of DCA the explicit purpose.

3.1 Geometry effect

The results reveal the "non-intrinsic" nature of the quantum yield relative to the geometric configuration of the system and the initial concentration of DCA.

For the system at initial constant concentration, the quantum yield values for the CPC reactor are higher than the tubular and axial ones. Furthermore, for the same geometric configuration, the quantum yield is greater at high concentrations.

The first result is related to the total amount of absorbed energy by the system OVRPA to induce the generating process of electron-hole pairs. The Figure 1 shows the quantum yield tendencies depending on the overall net distributed energy by assessing each geometry at initial constant concentration of DCA. The experimental data are shown with symbols. The lines only show the trend of the results when changing from one reactor to another. The results are consistent with

It can be concluded that the luminous flux and geometry of the reactor play a fundamental role in carrying out photodegradation. A suitable geometric configuration for the provision of the radiation field space implies greater absorbed energy (Blanco et al., 2001) and therefore, greater photodegradation efficiencies reflected in the overall quantum yields and high reaction rates for constant light flows, (Brucato and Rizzuti, 1997a, 1997b; Brucato et al., 2007; Davydov et al., 1999; Moreira et al., 2010).

3.2 Effect of initial concentration of DCA

The quantum yield results indicate that for any geometry, this photo-kinetic parameter is higher when working at higher initial concentration of DCA, showing high reaction rates. The quantum yield is lower, and the reaction rate decreases for low initial concentration of DCA. This behavior is consistent with others substances as the phenol, 4-chlorophenol, methanol, and organic compounds (Thomas Jr. et al., 1995; Wang et al., 2002; Sagawe et al., 2003; Cernigoj et al., 2009). In addition, the numerical magnitudes are turning away from each other, as the initial concentration increases (see Figure 1).

The low quantum yields (at low concentration) are attributed to the recombination rate due to electron deficit, presenting a reduction in the transformation of molecules with the same amount of absorbed energy (Monllor-Satoca et al., 2007).

In general, the radiant field of the system provides a constant induction of reactive pairs and an electric potential field inducing constant charges that promote the migration of the holes towards semiconductor-solution interface and of the electrons into the bulk of the semiconductor, restricting the process to an exclusive function of the solution concentration (Monllor-Satoca et al., 2007).

A higher concentration of dissolved DCA ions at the beginning of the process ($5 \geq \text{pH} \geq 3.2$), provides greater absorption on the surface (Zalazar et al., 2005) and therefore, the neutralization of surface potential, inducing migration of reducer electrons towards it. This will

increase the effect of transformed molecules by indiscriminate oxidizing agents. This behavior is attributed to the reactions between different species such as highly oxidizing holes and radicals. This increases the efficiency in the processing of molecules, and comprehensively decreasing the probability of the recombination of electron-hole pairs (Marugan et al., 2006; Monllor-Satoca et al., 2007; Li et al., 2010; Serrano et al., 2009).

By contrast, lower concentrations of DCA will show higher recombination rates, and although the free holes tend to attack the molecules with the same effectiveness, the number of present molecules in the surface reaction will be smaller (Candal et al., 2001), showing a lower net molecule transformation for the same absorbed OVRPA.

3.3 Prediction of experimental data of DCA photodegradation

The implementation of the scheme solution presented in section 2.4 allowed predicting DCA photodegradation rates. The Figure 2 shows an example of the prediction of DCA photodegradation, in particular for CPC reactor (data not shown for tubular and axial reactors), using the estimated values of non-intrinsic overall quantum yield and the approach of effective radiation model versus the experimental data for all reactors. It was found that the three reactors had a similar behavior. The results show a clear effectiveness of the used numeric scheme solution, plus a satisfactory stoichiometric representation of the DCA photodegradation reaction.

The overall average relative errors associated to the prediction of the experimental data in each reactor are less than 2.5% (see Table 2). There are minimal discrepancies of the model regarding to the experimental data, as well as predictive effectiveness, the validity of the model approach in this study, and the stability of the proposed numerical algorithm. Similar results were reported using parameter estimating and modeling of reactors (Marugan et al., 2008, 2009; Alfano & Cassano, 2009).



Figure 1. Quantum yields depending on the OVRPA. $\circ C_{DCA}=120$ ppm; $\Delta C_{DCA}=60$ ppm; $\diamond C_{DCA}=30$ ppm.

those reported in the literature for different systems (Minero and Vione, 2006; Liu and Zhao, 2010).

The Figure 1 shows that for low OVRPA (axial reactor case) the quantum yield declines, and on the other hand, at high absorbed energy (CPC) the quantum yield is high. This is attributable to the diffuse component and to the radiation energy distribution as a result of the CPC collectors (Colina-Marquez et al., 2010).

It further notes that for the same high initial concentration (120 and 60 ppm), the quantum yield tends to rise with the increase of absorbed energy. However, for lower concentrations, the quantum yield presents an asymptotic tendency towards $0.0015 \text{ (mol}\cdot\text{Einstein}^{-1})$, with a steep change of slope. This may represent a rapid decline (for this concentration) of the generation of electron-hole pairs, in addition to the increase of the recombination rate of the induced pairs (Candal et al., 2001). These results agree with those reported in the literature, (Trujillo et al. 2010, Sagawe et al. 2010, Ballari et al., 2010).

The above observations are related to the band-gap of titanium dioxide. For the three evaluated geometric configurations, the incident luminous

flux is the same; and therefore, its photochemical power. The low energy of the radiant field implies that the excitation of the semiconductor is also low due to its value close to the band gap energy and hence the numerical value of quantum yields (Serpone, 1997; Emilene et al., 2008; Trujillo et al., 2010).

However, the geometry effect plays a fundamental role on the system, because it affects the radiant energy distribution within the absorber and how it arrives at each dispersed particle, thus affecting the induction of reactive pairs and kinetics reaction. The results are in agreement with literature, Carp et al. (2004) shows a complete review about the photoinduced reactivity of titanium dioxide. It is clear that reaction regimes depend on the flux of energy and this affects the electronhole pairs generation and reaction rate.

At high OVRPA, high superficial excitement is generated, more electron hole pairs attack on the reactive species, and hence greater efficiency of redox reactions. This is reflected in higher quantum yields. In contrast, low OVRPA induces less redox reactions, minor transformation of molecules and therefore, lower quantum yields (Serpone et al., 1996; Serpone, 1997; Serpone and Salinaro, 1999; Salinaro et al., 1999; Arancibia-Bulnes et al., 2009; Li Puma et al., 2010).



Figure 2. Experimental data simulation for the DCA photodegradation as a function of time for the CPC reactor. $\circ C_{DCA0}=120 \text{ ppm}$; $\Delta C_{DCA0}=60 \text{ ppm}$; $\diamond C_{DCA0}=30 \text{ ppm}$, Model (—).

Table 2. Overall errors and maximums local errors for the established model.

Reactors	% Overall Average Error	% Maximum Local Error
CPC	0.53	1.27
Tubular	1.33	3.79
Axial	2.36	4.62



Figure 3. Experimental (all reactors) and simulated data comparison for initial DCA concentration of 120 ppm.

The Figure 3 shows a typical behaviour of the difference between the model discrepancy and the all experimental data. The total experimental data were compared to the model prediction for each constant initial concentration of DCA. The correlation coefficients for the three linear functions were 0.973, 0.986 and 0.980, for initial concentrations of 120, 60 and 30 ppm, respectively. This ratified the predictive ability of model used.

4. Conclusions

The evaluation of the overall quantum yields, coupled to an approach model of effective radiation field, demonstrated the strong influence of the geometry of the system reaction on the photo-kinetic parameters when working at a constant initial concentration of substrate. This suggests that the quantum yields calculated with the model has "non-intrinsic" nature, dependent on the absorbed radiant energy by the system and the initial concentration of the substrate.

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Nomenclature

C	Concentration, [$\text{mole} \cdot \text{cm}^{-3}$] or [$\text{g} \cdot \text{cm}^{-3}$]
E^a	Global volumetric rate of photon absorption, [$\text{einstein} \cdot \text{cm}^{-3} \cdot \text{min}^{-1}$]
e^-	Semiconductor conduction band electron
h	Plank constant, [J·s]
h^+	Semiconductor valence band hole
I	Incident energy, [$\text{einstein} \cdot \text{cm}^{-2}$]
K	Fitting parameter of kinetic model, [$\text{mol} \cdot \text{g}^{-2} \cdot \text{min} \cdot \text{cm}^{-9}$]
R	Reaction rate, [$\text{mol} \cdot \text{cm}^{-3} \cdot \text{min}^{-1}$]
S	Superficial area, [cm^2]
S	Cartesian coordinate, [cm]

T Time, [min]
 V Volume, [cm³]

Greek letters

β Kinetic photo-kinetic parameter, [mole·cm⁻³]
 Z Relative to radiation field
 Ξ Geometry parameter
 γ Frequency, [s⁻¹]
 χ Effective longitude, [dimensionless]
 λ Wavelength, [nm]
 P Phase function
 η_L Geometry parameter or lamp numbers, [dimensionless]
 κ_v Volumetric absorption of semiconductor coefficient [cm⁻¹]
 σ_v Volumetric scattering coefficient [cm⁻¹]
 Y Transmittance coefficient, [dimensionless]
 T Discrepancy function
 Ψ Fraction of incident radiation, [dimensionless]
 Φ Quantum yield, [mol·einstein⁻¹·cm⁻³]

Subscripts

A Absorption
 Cat Catalyst
 DCA DCA
 F Field
 G Global
 Gap Band gap
 H High
 L Longitude or low
 M Step in summity
 N Net
 O_2 Oxygen
 θ Initial condition
 Obs Observed
 R Reactor
 T Total

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