



Journal of Aerospace Technology and
Management

ISSN: 1984-9648

secretary@jatm.com.br

Instituto de Aeronáutica e Espaço
Brasil

Bidinotto, Jorge Henrique; Morgado Belo, Eduardo
Modal Shape Analysis Using Thermal Imaging
Journal of Aerospace Technology and Management, vol. 7, núm. 2, 2015, pp. 1-8
Instituto de Aeronáutica e Espaço
São Paulo, Brasil

Available in: <http://www.redalyc.org/articulo.oa?id=309438481008>

- How to cite
- Complete issue
- More information about this article
- Journal's homepage in redalyc.org

redalyc.org

Scientific Information System
Network of Scientific Journals from Latin America, the Caribbean, Spain and Portugal
Non-profit academic project, developed under the open access initiative

Modal Shape Analysis Using Thermal Imaging

Jorge Henrique Bidinotto¹, Eduardo Morgado Belo²

ABSTRACT: In recent years, advances in aeronautical engineering field include, among others, the development of increasingly lightweight and flexible materials, allowing better performance of systems in applications such as Unmanned Aerial Vehicles, photographic model airplanes, light weight aircraft etc. This progress, however, can cause difficulties in design and various types of tests, such as those performed in modal analysis, since the instrumentation weight and shape can influence the behavior of very light and aerodynamic structures. This paper proposes a new technique to perform modal analysis in simple structures, eliminating the use of accelerometers, which must be numerous in this type of analysis and have significant weight; the whole structure can be analyzed at the same time, and this is an advantage in comparison with other techniques as vibrometer laser, that analyses one point at a time. The technique in question makes use of infrared imaging, detecting, through the heat, the structure deformation, allowing the trace of its modal shape. For this, a theoretical analysis and a thermomechanical modeling of a known structure are performed, with subsequent test to be validated, and finally the conclusions and suggestions for future work are presented.

KEYWORDS: Modal response, Infrared imaging, Thermomechanics.

INTRODUCTION

Recent Engineering advances during the last years have included the development of new materials with the most diverse applications, emphasizing its best performance and improving the functioning of complete systems in the area of mechanical, electrical, aeronautical, and others.

Among the most common applications is the aircraft design, where the best performance depends on more lightweight and flexible materials that allow ease in manufacturing, increased payload and better aerodynamic performance.

The development of these materials, however, brings difficulties in design and implementation of structural tests due the influence of the sensors on the material's tested behavior.

An example is the setting of accelerometers for experimental modal analysis, which can greatly affect the behavior of low-weight structures, such as UAVs or model airplanes for photo applications, since this type of sensor includes in its structure a seismic mass, a piezoelectric crystal and a base, which carry weight to the set. An experimental modal analysis should ideally include multiple accelerometers on the same structure, increasing this problem or the test must be repeated with one accelerometer fixed in different positions, as performed by De Marqui Jr. *et al.* (2007), increasing time and cost for the test.

This paper proposes a kind of modal analysis that provides the shape of each vibration mode based on infrared imaging. This proposal is based on the fact that the structure deformation generates internal stresses, resulting in local temperature increase, detectable by infrared cameras. The temperature variation is very small, requiring a highly accurate experimental apparatus, as described along the text.

For infrared technology research, Hudson Jr. (1969) provides the basic theory of infrared radiation and Holst (2003) explains

¹.Universidade Federal de São Carlos – Centro de Ciências Exatas e de Tecnologia – Departamento de Engenharia Mecânica – São Carlos/SP – Brazil.
².Universidade de São Paulo – Escola de Engenharia de São Carlos – Departamento de Engenharia Aeronáutica – São Carlos/SP – Brazil.

Author for correspondence: Jorge Henrique Bidinotto | UFSCar/CCET/DEMec | Rodovia Washington Luís, km 235 | CEP: 13.565-905 – São Carlos /SP – Brazil
 Email: bidinotto@ufscar.br

Received: 12/23/2014 | **Accepted:** 04/08/2015

its use for imaging and as thermo sensor, while Wyatt (1987) gives design concepts for devices for this purpose.

McShea (2010) shows aeronautical applications for infrared imaging, while Clifton (1996) and Fisher *et al.* (2003) provide applications specifically targeting the flight tests.

Dehne *et al.* (2012), Fujino *et al.* (2003) and FLIR Systems (2011, 2012a) show some applications of infrared imaging in the aircraft industry, mainly aimed at thermal comfort or aerodynamic transition from laminar flow to turbulent.

The same themes are addressed, but in an academic way, in the work of Malerba *et al.* (2008), Banks (2000) and Zuccher *et al.* (2003). FLIR Systems (2012b) and Infrared Training Center (2008) provide information about the use and ideal conditions for application of infrared cameras for various purposes.

To analyze the material's thermomechanic behavior, a study was conducted in three different fronts, given the multidisciplinary character of this phenomenon. The first one was in Materials Science, where Guy (1976) and Van Vlack (1989) had a big importance. The second front of this study was in Mechanics of Materials, obtaining all the necessary information in Beer *et al.* (2006). The third line of research was in Thermodynamics, where Schulz (2003) and Van Wylen and Sonntag (1986) provided the necessary information for the study.

Few articles were found in this area, none of them with similar purpose. Razo *et al.* (1995) make an interesting thermomechanical analysis of a specific material, patented by a private company. Other references, such as Lee *et al.* (1993) and Wedekind *et al.* (2010), mention the study of thermomechanical behavior focused on a mechanical manufacturing approach. Yang and Wang (2013) and Brinson (1993) address the issue from the perspective of intelligent materials such as shape memory alloys.

The paper presents the theoretical fundamentals on which this method is based in the following section. Theoretical Model section shows the structure used in this work and its modeling. Experimental Procedure section presents experiments conducted to validate the model with its respective results and some conclusions are presented on Conclusions section, followed by References.

THEORY

INFRARED TECHNOLOGY

Infrared images are generated by processing electro-optical radiation emitted by any object and captured by proper equipment called infrared cameras.

Infrared radiation means the part of the electromagnetic spectrum radiation (Fig. 1) with a wavelength between 0.8 and 1,000 microns and are divided into 3 categories: short infrared radiation (0.8 to 1.5 μm), medium (1.5 to 5.6 μm) and long (5.6 to 1,000 μm), as described by Holst (2003).

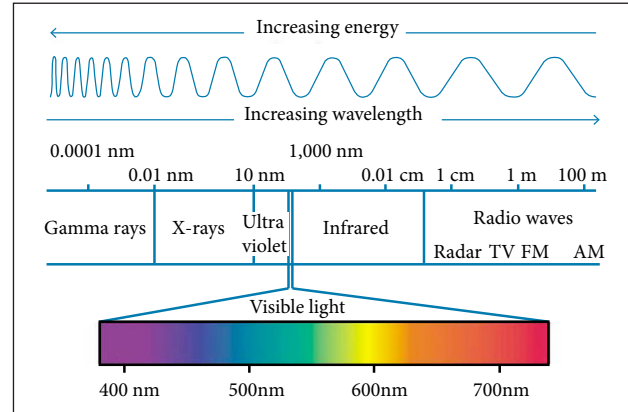


Figure 1. Electromagnetic spectrum (Bidinotto *et al.*, 2013).

Thermal radiation is generally in the region of medium infrared radiation (high temperatures) or long infrared radiation (low temperatures), and this difference in wavelength (and hence in the frequency) captured by the infrared camera is processed to generate the images based on radiation. Some important features of thermal radiation are:

- All objects emit thermal radiation.
- It does not require a material environment to occur, so radiation can cross vacuum.
- It easily crosses most gases.
- Normally, it is not able to cross liquids or solids.

In addition to emission an object reacts to the incident radiation environment, absorbing and reflecting a part of it, or allowing a small amount of radiation to cross (such as through a lens). The law of total radiation (W) is derived from this physical principle and can be determined by the following equation:

$$W = \alpha W + \tau W + \rho W \quad (1)$$

where:

$$\alpha + \tau + \rho = 1 \quad (2)$$

The coefficients α , ρ , and τ describe the absorption of incident energy of the object (α), reflection (ρ) and transmission (τ).

Each coefficient may have a value between 0 and 1, depending on the way the object absorbs, reflects or transmits the incident radiation. For example, if $\rho = 0$, $\tau = 0$ and $\alpha = 1$, then there is no energy reflected or transmitted and 100% of the incident radiation is absorbed. That is called a perfect blackbody (Hudson Jr., 1969).

Holst (2003) describes mathematically the behavior of bodies with respect to heat using the Kirchhoff's law. The properties related to the energy irradiation are denoted by the symbol ε , called emissivity of the body. Kirchhoff's law provides that $\alpha = \varepsilon$, either, as both depend on the wavelength, $\alpha(\lambda) = \varepsilon(\lambda)$. Equation 2 in the case of opaque bodies ($\tau = 0$) can be simplified by:

$$\rho + \varepsilon = 1 \quad (3)$$

In the case of the black body $\rho = 0$ and has therefore $\varepsilon = 1$.

The same reference shows the Planck's law given by Eq. (4), that describes the amount of energy radiated by a black body in thermal equilibrium as function of speed of light (c), Boltzmann constant (k) and temperature (T , in kelvin) and was formulated in 1900 with empirically determined constant. Planck accurately described the blackbody radiation (Fig. 2a), suggesting that electromagnetic radiation was emitted in quanta (Wyatt, 1987). The Sun is an excellent approximation of a black body (Fig. 2b).

$$u(\nu, T) = 4\pi/c \cdot I(\nu, T) = (8\pi h \nu^3 / c^3) \cdot 1/(e^{h\nu/kT} - 1) \quad (4)$$

where:

u : amount of energy radiated; I : spectral radiance; h : Planck constant.

Planck assumed that the energy of these oscillations is limited to integer multiples of the fundamental energy E and proportional to the oscillation frequency ν as in Eq. 5. He assumed that quantization theory five years after Albert Einstein have suggested the existence of photons to explain the phenomenon of photoelectric effect.

$$E = h\nu \quad (5)$$

From Planck's law, the total energy radiated from a blackbody can be calculated. This is expressed by the Stefan-Boltzmann's law:

$$W = \sigma T^4 \quad (6)$$

where:

σ : Stefan-Boltzmann constant ($5.67 \times 10^{-8} \text{ Js}^{-1}\text{m}^{-2}\text{K}^{-4}$).

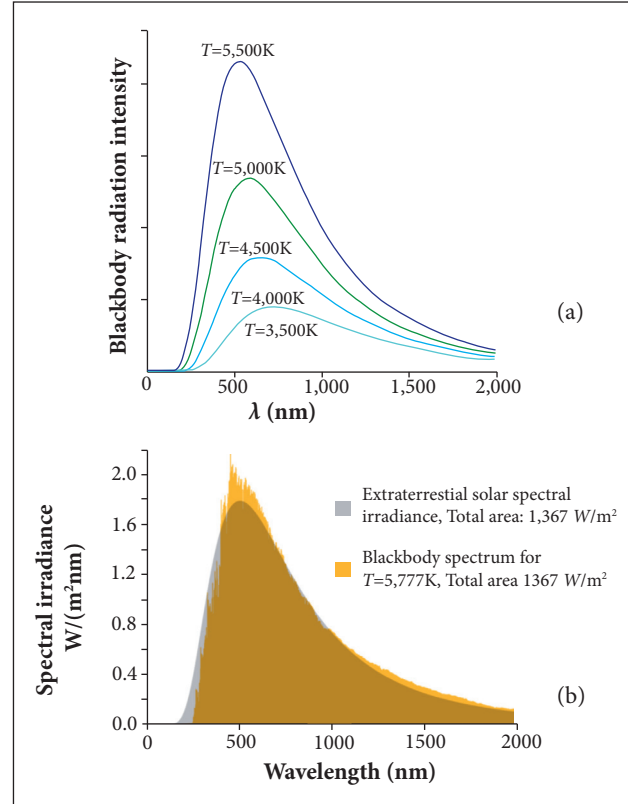


Figure 2. (a) Blackbody radiation and (b) its approximation to the solar irradiance (Bidinotto *et al.*, 2013).

The properties of radioactive objects are generally described in relation to a perfect blackbody. If the energy emitted from a blackbody is denoted as W_{bb} , and the one of an ordinary object at the same temperature, as W_{obj} , the relationship between these two values describes the emissivity (ε) of the object, as in Eq. 7.

$$\varepsilon = W_{obj} / W_{bb} \quad (7)$$

Consequently, the emissivity is a number between 0 and 1. The better the radioactive properties of the object, the higher its emissivity. An object that has the same emissivity for all wavelengths is called a grey body.

The current infrared cameras can transform the radiation emitted by an object to an image. The infrared radiation is emitted by all objects with a temperature above absolute 0 (0 kelvin) and has similar characteristics to the radiation as a visual reflection, refraction and transmission. The higher the temperature of the body, the greater the radiated energy.

For this reason, the principle of operation of an infrared camera is similar to a light visible wavelength camera. It has a lens which focuses the radiation onto the detector and a set of electronic hardware and software that processes and samples the generated signals and images.

Therefore, thermography allows one to make temperature measurements of an object without physical contact. Infrared detectors from modern cameras are composed by a Focal Plane Array (FPA) of various materials sensitive to specific wavelength. The sensor resolution array can vary from about 160×120 pixels to $1,024 \times 1,024$ pixels. Depending on the size and resolution of the detectors array, it can contain more than 60,000 to 1 million of individual detectors.

THERMOMECHANICAL MODELING

Deformation in materials generates energy dispersion as heat (Guy, 1976). Van Vlack (1989) is consistent with this explanation and adds that when a stress is applied to a material deforming elastically, and then removed, the energy involved in this deformation is dispersed mostly in the form of heat, generating a local temperature increase, which soon is transferred to environment.

In order to quantify this temperature increase, a study was performed to create a numerical model and predict the rise in temperature in each section of the structure when a load is applied.

In the present paper, the structure analyzed is modeled as a cantilever beam subject to a bending force, a momentum and torque, as shown in Fig. 3, following the energy method described by Beer *et al.* (2006).

For simplification, the bending load effect (P and M) represented by Fig. 4 is studied separately from the torsion (M_x) showed by Fig. 6.

Following this method, the energy obtained in deformation is a sum of two parts: the strain energy of normal stress (U_σ) and the energy of shear stress (U_τ), which will be equated using the shear and momentum diagrams shown in Fig. 6.

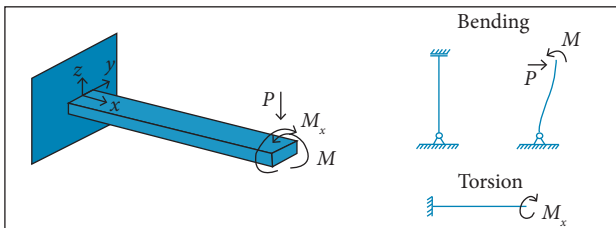


Figure 3. Simplified model for the studied structure.

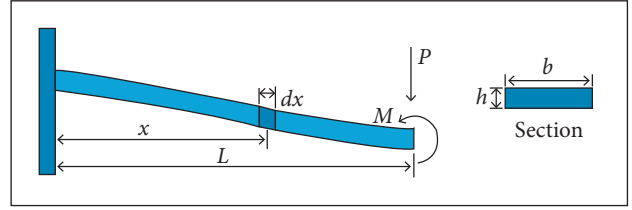


Figure 4. Bending beam model.

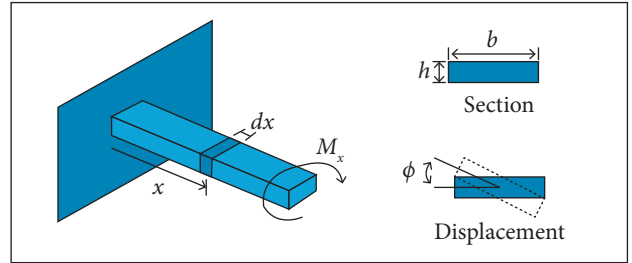


Figure 5. Torsion beam model.

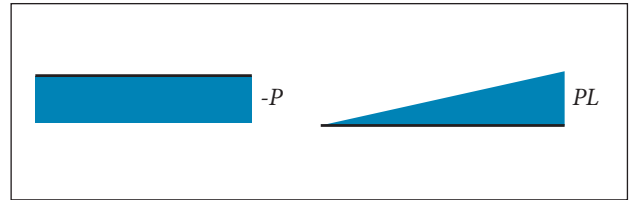


Figure 6. Shear force (a) and momentum (b) diagrams from the structure.

Normal stress has the strain energy given by (Beer *et al.*, 2006):

$$U_\sigma = \frac{1}{2EI} \int_0^L (Px)^2 dx \quad (8)$$

For shear stress,

$$U_\tau = \frac{1}{2G} \left(\frac{3}{2} \frac{P}{bh} \right) \int_0^L \int_{-h/2}^{h/2} \left(1 - \frac{z^2}{c^2} \right) b dx dz \quad (9)$$

where:

G: modulus of transversal elasticity.

Solving the integrals and converting the forces to stress using the equations described by Beer *et al.* (2006), the sum of both parts, considering stress as a scalar number, is:

$$U_h = U_\sigma + U_\tau = \sigma^2 \frac{bh^3}{12} \left[\frac{bhL^3}{18x^2 EI} + \frac{1}{5GL} \right] \quad (10)$$

Using the same method, it was made the beam equationing subjected to torsion stress, schematized in Fig. 6 and modeled by Eq. 11.

$$U_\theta = \int_0^L M_x d\phi \quad (11)$$

Analyzing dx element, one can evaluate the presence of a shear stress τ as shown in Fig. 7.

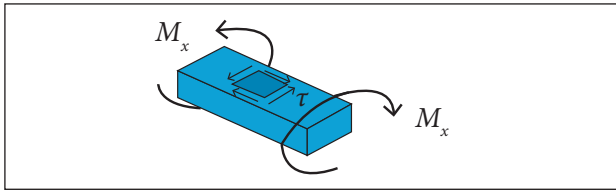


Figure 7. Shear stress applied to element dx .

And, for this case, the shear stress can be represented by:

$$\tau = \frac{M_x}{c_1 b h^2} \quad (12)$$

Substituting Eq. 12 in Eq. 11 and integrating it, one reaches:

$$U_\theta = \frac{c_1^2 b h}{c_2 G} \int_0^L \tau^2 dx = \frac{c_1^2 b h L}{c_2 G} \tau^2 \quad (13)$$

For a closed system, it can be used the First Law of Thermodynamics, which states that the cyclic integral of heat is equal to the cyclic integral of work (Van Wylen and Sonntag, 1986), reaching:

$$\oint \delta Q = \oint \delta W \quad (14)$$

Considering that thermal energy results in temperature increasing and, as stated by the Law of Conservation of Energy (Schulz, 2003), all the energy involved in bending and torsional stress (U) are converted to work (W), Eq. 15 can be written:

$$\oint \delta W = U = \int \rho(hbdx)c\delta T \quad (15)$$

Substituting Eqs. 10 and 13 in Eq. 15, one has for bending:

$$\sigma^2 \frac{bh^3}{12} \left[\frac{bhL^3}{18x^2 EI} + \frac{1}{5GL} \right] = \int \rho(hbdx)c\delta T \quad (16)$$

and for torsion:

$$\tau^2 \frac{c_1^2 b h L}{c_2 G} = \int \rho(hbdx)c\delta T \quad (17)$$

THEORETICAL MODEL

For this study, a set composed by a rigid wing fixed to a flexible support was used, which will be used in a complementary future work. The structure is shown in Fig. 8 and its details are described in Table 1.

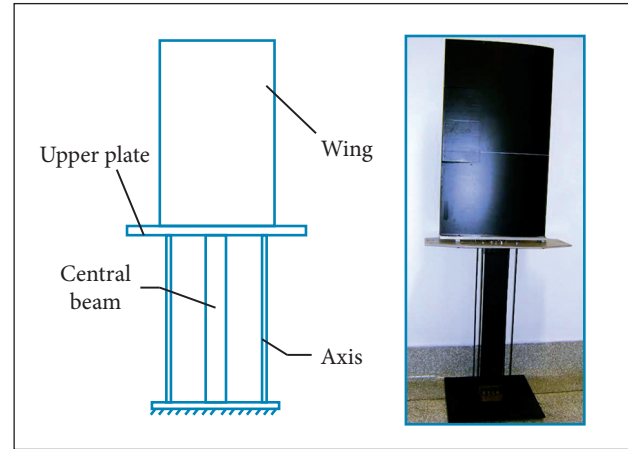


Figure 8. Images presenting the set used in this study.

Table 1. Structure's properties.

Element	Material	Dimensions [mm]	
		Length	Width
Central beam	Steel Alloy 1020	700	100
		Thickness	2
		Diameter	5.5
Upper plate	Aluminum Alloy 2024T	Thickness	5.8
		Width	300
		Length	600
Wing NACA 0012	Aluminum Alloy 2024T	Span	800
		Chord	450

Applying the structure properties in Eqs. 16 and 17, equations to predict the expected increase of temperature (in degrees Celsius) when a given load is applied can be obtained. The equations found are as follows:

For bending:

$$\Delta T_h = \sigma^2 [3.563 \times 10^{-17} x^{-2} + 3.242 \times 10^{-21}] \quad (18)$$

For torsion:

$$\Delta T_{\theta} = 1.129 \times 10^{-15} \tau^2 \quad (19)$$

For analysis, a Finite Element Model was raised using the MSC Patran 2010 software and the first two vibration modes were obtained solving the modal analysis in MSC Nastran 2010 software. The results are presented in Fig. 9.

Knowing the shape and frequency of the first two vibration modes, a new simulation by the Finite Element Method was carried out, statically loading the structure in order to deform it in bending and in torsion, similar to the deformation applied in the experiment explained in the next section, considering that the only part of interest in the structure is the support central beam. This simulation is intended to take a spectrum that gives the stress at each point of the structure, in order to complete the thermomechanical modeling. Figure 10 shows the position of the applied deformation in each case: 35 mm in bending case, 15 mm in torsion case, both in static conditions.

Figure 11 shows the simulation results for stress using the Von Mises criteria. The numerical results are presented in Pascal.

Combining the result of simulation with Eqs. 18 and 19 obtained in thermomechanical modeling, it is possible to create the spectrum of temperature rise at each point of the structure shown in Fig. 12. The numerical results are presented in degrees Celsius.

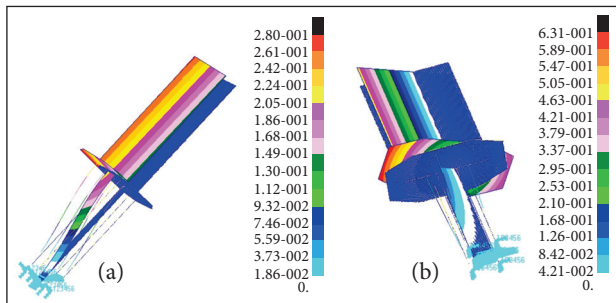


Figure 9. First (a) and second (b) vibration modes.

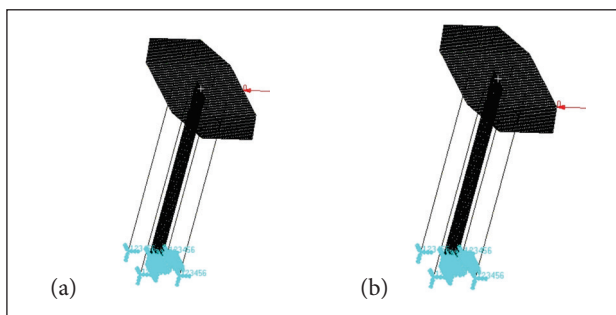


Figure 10. Load position in simulation for bending (a) and torsion (b).

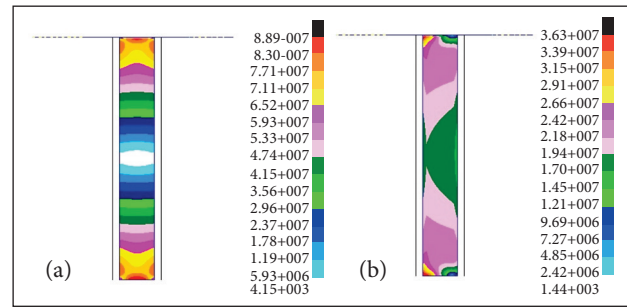


Figure 11. Simulation results for bending (a) and torsion (b).

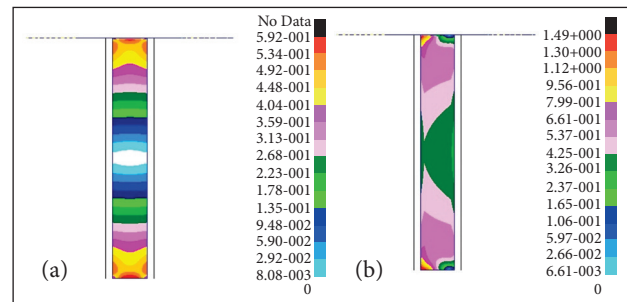


Figure 12. Temperature raise spectrum for bending (a) and torsion (b).

EXPERIMENTAL PROCEDURE

For validation of thermomechanical model, a test for obtaining the first and second vibration mode shapes was performed with the aid of infrared imaging, in order to compare them with those obtained by the model.

In this case, the structure was excited at natural frequencies, for better characterization and the mode shapes be captured by the infrared camera. For this reason, it was chosen the excitation by shaker at the same points and displacements used in the model (Fig. 10) obtaining its frequencies by an accelerometer fixed in the end of the driver, in order to accurate the sinusoidal excitation method. Thus, the structure suffered deformations per cycle of vibration and the infrared camera could capture small changes in temperature along the central beam at each movement occurred.

The test was performed with the experimental configuration shown in Fig. 13.

For the test, environment was conditioned at 18°C, the structure was painted matt black, and it was positioned, behind the structure, one plate at a considerably higher temperature than the structure in order to improve the contrast in images.

Figure 14 shows images of the experimental apparatus used. Test results are shown in Fig. 15, which presents the structure on its maximum deflection during bending (a) and torsion (b).

For image analysis, a software feature was used, which provides a Microsoft® Excel table, where each pixel from the image generates a table cell, with the value of the temperature on that pixel. With this tool, pixels corresponding to the central bar structure were isolated and, using a routine in MATLAB, the data were filtered and plotted on a color chart for better characterization of the bar regions according to their temperature.

For a better visualization of the results predicted by the model, the gross experimental results and the experimental results after processing of data, Fig. 16 was generated, which shows the three plots side by side for direct comparison in

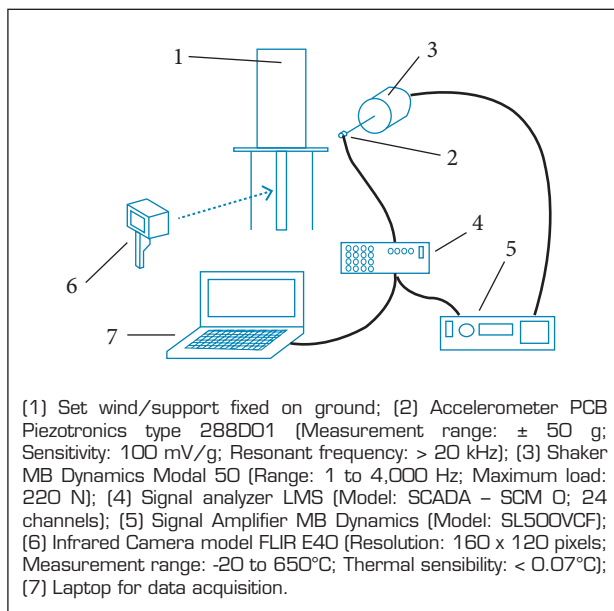


Figure 13. Experimental apparatus used in the test.

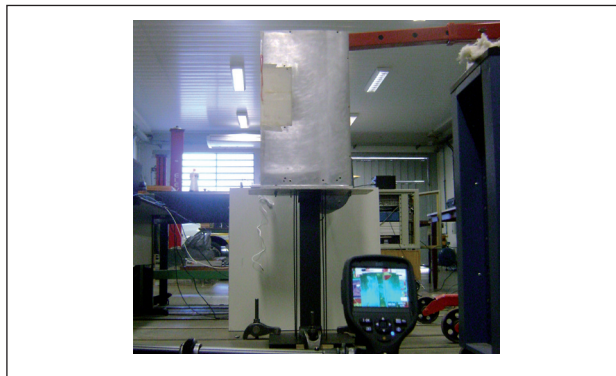


Figure 14. Test performance.

bending. All numerical results are presented in degrees Celsius for Figs. 16 and 17. Similarly, results in torsion are shown in Fig. 17.

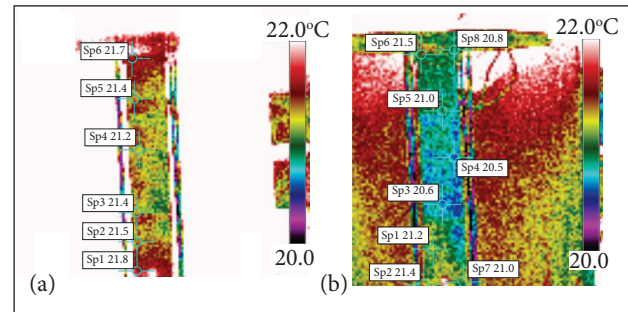


Figure 15. Infrared images from the structure loaded in bending (a) and torsion (b) at its maximum deflection point.

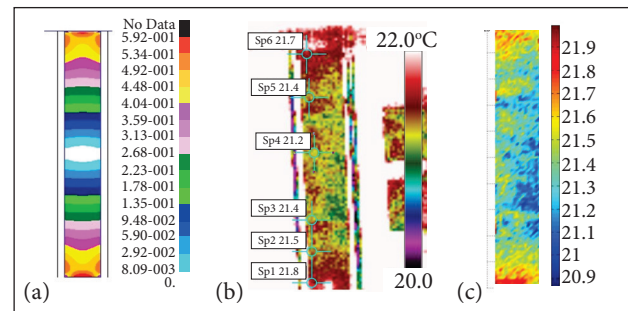


Figure 16. Comparative results obtained in bending case from model (a), gross data (b) and processed experimental data (c).

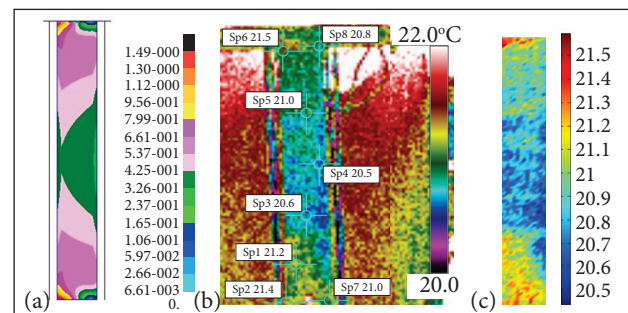


Figure 17. Comparative results obtained in torsion case from model (a), gross data (b) and processed experimental data (c).

CONCLUSIONS

Experiments performed with infrared imaging showed satisfactory results which allow doing a preliminary validation of this testing methodology. In these trials, it was possible to identify a similar trend to that provided in the model, but with a lower temperature contrast than predicted. This may be due to instant heat exchange between the bar and the atmosphere,

since the ambient temperature during test was considerably lower than that of the frame (18°C), which may have caused a loss of heat from the bar, decreasing its temperature more markedly in its warmer regions.

These tests also showed some limitations in using this infrared camera model: low resolution and low speed in frames capture. Such problems can be solved using a camera with higher resolution and higher frequency. In future trials, one should consider obtaining such equipment.

For future work, some innovations are already planned:

- The acquisition of a new camera, with more precision and better resolution, in order to give better images.
- Improving the test precision and studying its limitations, such as the complexity of the studied structure and its excitation frequency.
- Development of a subroutine in MATLAB to provide a figure plotted in real time, providing best results instantly.

With the results obtained, it can be concluded that, with some improvements in data acquisition, a new modal shape measurement method can be developed, being cheaper, simpler and faster.

REFERENCES

- Banks, D.W., 2000, "Visualization of In-Flight Flow Phenomena Using Infrared Thermography", NASA TM-2000-209027.
- Beer, F.P., Johnston Jr., E.R. and DeWolf, J.T., 2006, "Mechanics of Materials", 4th edition, McGraw-Hill, New York, USA.
- Bidinotto, J.H., Kleinubing, M., Catalano, F.M. and Belo, E.M., 2013, "Thermography Applied on Boundary Layer Transition Visualization", Proceedings of the International Congress of Mechanical Engineering, COBEM, Ribeirão Preto, Brazil.
- Brinson, L.C., 1993, "One-Dimensional Constitutive Behavior of Shape Memory Alloys: Thermomechanical Derivations with Non-Constant Material Functions and Redefined Martensite Internal Variable", Journal of Intelligent Material Systems and Structures, Vol. 4, No. 2, pp. 229-242. doi: 10.1177/1045389X9300400213
- Clifton, J.M., 1996, "Introduction to Avionics Flight Test", Vol. 15, AGARDograph, London, UK.
- De Marqui Jr., C., Rebolho, D., Belo, E.M., Marques, F.D. and Tsunaki, R.H., 2007, "Design of an Experimental Flutter Mount System", Journal of the Brazilian Society of Mechanical Sciences and Engineering, Vol. 29, No. 3, pp. 246-252. doi: 10.1590/S1678-58782007000300003
- Dehne, T., Bosbach, J. and Heider, A., 2012, "Dynamics of Aircraft Cabin Ventilation by In-flight Infrared Thermography", Proceedings of the 11th International Conference on Quantitative InfraRed Thermography, QIRT, Naples, Italy.
- Fisher, D., Horstmann, K.H. and Riedel, H., 2003, "Flight Test Measurement Techniques for Laminar Flow", Vol. 23, AGARDograph, London, UK.
- FLIR Systems, 2011, "Application Story – DLR Dornier 228", Catalogue, FLIR Systems Co. Ltd., Hong Kong, China.
- FLIR Systems, 2012a, "Application Story – Dassault Falcon 7X", FLIR Advanced Thermal Solutions, France.
- FLIR Systems, 2012b, "The Ultimate Infrared Handbook for R&D Professionals", FLIR Systems AB, Sweden.
- Fujino, M., Yoshizaki, Y. and Kawamura, Y., 2003, "Natural-Laminar-Flow Airfoil Development for a Lightweight Business Jet", Journal of Aircraft, Vol. 40, No. 4, pp. 609-615. doi: 10.2514/2.3145
- Guy, A.G., 1976, "Essentials of Materials Science", McGraw-Hill, New York, USA.
- Holst, G.C., 2003, "Electro-optical Imaging System Performance", 3rd edition, JCD Publishing, Oviedo, USA.
- Hudson Jr., R.D., 1969, "Infrared System Engineering", John Wiley & Sons, New York, USA.
- Infrared Training Center, 2008, "Termografia Nivel 1 – Training course material", ITC, Sorocaba, Brazil.
- Lee, H.T., Chen, J.C. and Wang, J.M., 1993, "Thermomechanical Behaviour of Metals in Cycling Loading", Journal of Materials Science, Vol. 28, No. 20, pp. 5500-5507. doi: 10.1007/BF00367821
- Malerba, M., Argento, M., Salviuolo, A. and Rossi, G.L., 2008, "A Boundary Layer Inspection on a Wing Profile Through High Resolution Thermography and Numerical Methods", WSEAS Transactions on Fluid Mechanics, Vol. 3, No. 1, pp. 18-28.
- McShea, R.E., 2010, "Test and Evaluation of Aircraft Avionics and Weapon Systems", SciTech Publishing, Inc., Raleigh, USA.
- Razo, L.M., Solis, S., Asomoza, M. and Hernandez, A., 1995, "Establishment of Thermodynamic Properties of Pure Solid Substances by Thermomechanical Analysis", Journal of Thermal Analysis, Vol. 45, No. 6, pp. 1323-1330. doi: 10.1007/BF02547426
- Schulz, H.E., 2003, "O Essencial em Fenômenos de Transporte" (in Portuguese), EESC-USP, São Carlos, Brazil.
- Van Vlack, L.H., 1989, "Elements of Material Science and Engineering", 6th edition, Prentice-Hall, New Jersey, USA.
- Van Wylen, G.J. and Sonntag, R.E., 1986, "Fundamentals of Classical Thermodynamics", 3rd edition, John Wiley & Sons, New York, USA.
- Wedekind, M., Both, J. and Baier, H., 2010, "Thermo Mechanical Behaviour of Metal Matrix Composite Structure", International Journal of Material Forming, Vol. 3, No. 1, pp. 857-860.
- Wyatt, C.L., 1987, "Radiometric System Design", Macmillan Publishing Co., New York, USA.
- Yang, H. and Wang, L.Y., 2013, "Thermomechanical Analysis of Shape-Memory Composite Tape Spring", Applied Composite Materials, Vol. 20, No. 3, pp. 287-301. doi: 10.1007/s10443-012-9271-x
- Zuccher, S., Saric, W.S., Reed, H.L. and McNeil, L.R., 2003, "The Role of Infrared Thermography in the Study of Crossflow Instability at M=2.4", Proceedings of the 7th International Symposium on Fluid Control, Measurement and Visualization, FLUCOME, Sorrento, Italy.