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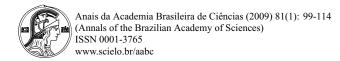
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# High spatial resolution analysis of Pb and U isotopes for geochronology by laser ablation multi-collector inductively coupled plasma mass spectrometry (LA-MC-ICP-MS)

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#### ABSTRACT

Age determinations using the  $^{235}$ U and  $^{238}$ U radioactive decay series to the daughter isotopes  $^{207}$ Pb and  $^{206}$ I respectively, using the mineral zircon (ZrSiO<sub>4</sub>), are widely used to decipher geological processes. A new meth developed in the last couple of years, the *laser* ablation multi-collector inductively coupled plasma mass spectromet (LA-MC-ICP-MS), overcomes previous laborious sample preparation, and yields isotopic ratios and age data with high spatial resolution of ten of microns. The present study describes the analytical set-up and data reduction process as presently applied at the Laboratory for Geochronology of the University of Brasília. It explores the precision a accuracy of the method by cross-analysing three international zircon standards. We arrive at a precision of 1.9 to 3.7 ( $^{2}\sigma$  SD) and an accuracy of 0.6 to 3.8% ( $^{2}\sigma$  SD) for and U isotopic ratios of the standards. We also apply the meth to two natural zircon samples, which have previously been dated by other analytical methods. A comparison of the results shows a good conformity of the age data, being within the error limits. The data demonstrate the great analytic potential of the method for rapid, precise and accurate U-Pb isotopic analyses on the micron scale.

**Key words:** geochronology, U-Pb isotopes, LA-MC-ICP-MS, zircon, age dating.

#### INTRODUCTION

Absolute age determinations in the geosciences serve for a variety of applications including geotectonic studies, sedimentation ages and sediment provenance, as well as dating of igneous and metamorphic rocks. They use the decay of a radioactive isotope in a natural mineral with a half-life favourable for the expected age of the material or process investigated. Many of these applications are conducted in materials of considerable age (millions to billions of years), which suggests the use of the radioactive uranium isotopes  $^{235}$ U and  $^{238}$ U with half-lifes of  $7.04 \times 10^8$  and  $4.47 \times 10^9$  years, and the radiogenic daughter isotopes  $^{207}$ Pb and  $^{206}$ Pb,

respectively. Analysis of the parent and daugh topes allows the determination of the crystallizat of the mineral. The mineral analysed should she tain physicochemically favourable characteristic as high resistance to chemical exchange and relization, and reasonably high U and radiogenic letents for analysis, amongst others. These are the abundantly occurring mineral zircon (ZrSiO4 is, therefore, the most traditional and widely use eral for age determinations of various geologica cations (e.g. Garbe-Schönberg and Arpe 1997, K al. 2002).

Apart from the improvement in precision, ac

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troduction of the sample in aqueous solution, a laser microprobe for sampling of solid material on the micron scale is connected to an ionization cell, which ionizes the sampled material in an inductively coupled plasma (ICP) and supplies single-charged ions to a magnetic sector or quadrupole mass spectrometer. The technique is referred to as "laser ablation inductively coupled mass spectrometry" (LA-ICP-MS). It avoids the laborious sample cleaning, dissolution and element separation in an ultraclean laboratory environment required by the traditional isotope dilution thermal ionization mass spectrometry (ID-TIMS). Since the pioneering work by Feng et al. (1993) and Hirata and Nesbitt (1995), significant analytical progress of the LA-ICP-MS method was achieved (see Vanhaecke and Moens 1999, Günther et al. 2000, Horn et al. 2000, Stirling et al. 2000, Simonetti et al. 2006, Paquette and Tiepolo 2007, Simon et al. 2007).

In this study, advances of this particular dating method, the multi-collector inductively coupled plasma mass spectrometry (MC-ICP-MS) coupled to a *laser* microprobe, which has recently been set up at the Geochronology Laboratory of the University of Brasilia, are reported. We present results of three international zircon standards cross-calibrated one against the other, and two natural zircon samples which have previously been analysed by other analytical methods. The data demonstrate the capacity of the method in terms of rapid, precise and accurate U and Pb isotope analyses with high spatial resolution.

#### RATIONALE

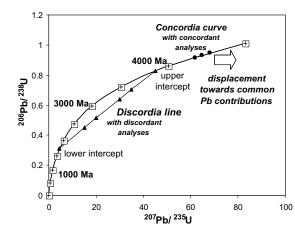
For the case of two radioactive isotopes of a single element, as for the decay systems of <sup>238</sup>U and <sup>235</sup>U, the ratios between the stable decay products and the radioactive parent isotopes (<sup>206</sup>Pb/<sup>238</sup>U and <sup>207</sup>Pb/<sup>235</sup>U) are interrelated. Given closed-system conditions, they plot on a curve which extends from today towards the formation of the Earth and the solar system at approximately 4.53 Ga ago (Fig. 1). The ratios have to concord one to the other following the relationship:

$$\frac{206 \text{Pb}}{1} - \left(\frac{207 \text{Pb}}{1} + 1\right)^{\lambda 238 \text{U}/\lambda 235 \text{U}} - 1$$
 (1)

age information can be obtained by the <sup>207</sup>Pb/<sup>206</sup>Pb age, based on the relationship:

$$\frac{^{207}\text{Pb}}{^{206}\text{Pb}} = \frac{^{235}\text{U}}{^{238}\text{U}} \times \frac{(e^{\lambda 235\text{U} \times \text{t}} - 1)}{(e^{\lambda 238\text{U} \times \text{t}} - 1)}$$
(2)

With the constant present-day <sup>238</sup>U/<sup>235</sup>U ratio of 137.88, this age information considers only the daughter isotopes. Hence, the more accurate and valid age information is obtained from the <sup>206</sup>Pb/<sup>238</sup>U and <sup>207</sup>Pb/<sup>235</sup>U isotope ratios.



There are two fundamental problems with this method. Firstly, the material analysed may contain initial common Pb of non-radiogenic origin. The non-radiogenic Pb fraction displaces the isotope analyses towards values below the Concordia curve (Fig. 1). The problem of this "common Pb" content can be resolved by correction procedures using crustal <sup>206</sup>Pb/<sup>204</sup>Pb and <sup>207</sup>Pb/<sup>204</sup>Pb compositions. These Pb isotope ratios, however, change with time in terrestrial materials, due to the radiogenic growth of <sup>206</sup>Pb and <sup>207</sup>Pb from the decay of <sup>238</sup>U and <sup>235</sup>U, respectively. The respective, time-dependant isotope ratio used for correction may be calculated from the average crustal Pb isotopic composi-



In order to avoid these corrections, it is always more effective to analyse minerals which, due to their crystal lattice characteristics, contain sufficient U to analyse the parent and the daughter isotope but, on the other hand, do not accommodate common Pb in the structure, because of the mismatch between ionic charge and effective ionic radius (Shannon 1976). These are, for example, zircon (ZrSiO<sub>4</sub>) or monazite (Ce,La,Nd,Th)PO<sub>4</sub>, which generally contain sufficient U to be analysed, ranging from 1 to > 10000 ppm for zircon and 282 to > 50000 ppm for monazite (Heaman and Parish 1991). The common Pb content of the two minerals is generally (but not always) very low.

Secondly, the system must have been closed to the gain or loss of the parent and daughter isotopes. In most cases, we deal with a loss of radiogenic lead which can be easily mobilized by geological processes because, as in the case of zircon, radiogenic Pb<sup>2+</sup> does not fit the Zr<sup>4+</sup> ion characteristics (Mezger and Krogstad 1997). The result is that the isotopic analyses plot on a "Discordia line" which intersects the Concordia curve twice (Fig. 1): the upper intercept generally represents the time of crystallization of the mineral; the lower intercept may, in cases, be interpreted as the geological event when the crystal lost part of his radiogenic lead. Mineral standards for isotopic analyses by LA-ICP-MS or ion microprobe should meet these two requirements, i.e. they should be concordant, and void of common lead.

### METHOLOGICAL PROGRESS OF Pb-U ISOTOPIC ANALYSIS

Conventional Pb-U analyses for absolute age determination of geological materials commonly use the technique of ID-TIMS (Isotope Dilution Thermal Ionization Mass Spectrometry). Sample preparation is laborious (e.g. Nebel-Jacobsen et al. 2005, Amelin and Davis 2006). The minerals have to be separated from the rock matrix, cleaned and sometimes abraded if the outer margins show alteration features (Mattinson 2005). The minerals are dissolved, and the Pb and U isotopes separated by resin columns in an ultra-clean laboratory to allow sub-panogram Pb isotopic analysis. The solutions

This techniques has been successfully apprehensives and is still commonly used for U-Pb agraminations and other isotopic geochemical applications and other isotopic geochemical application worldwide. Low-blank laboratories normally according to the precision of the age determinations (and Noble 2003, Krymsky et al. 2007). However, comings of the technique are the need to separate of the analyses, and the laborious wet chemical perion under ultra-clean laboratory conditions. On the hand, the quality of the analyses is excellent, reprecisions down to  $\leq 0.1\%$  for the Pb/U isotopic (e.g., Mattinson 2005).

Another method which overcomes the need chemical preparation is the Sensitive High Res Ion Micro Probe (SHRIMP). It focuses a high ion beam (usually  $O_2^-$ ) onto an area of usually of in situ isotopic analysis of minerals such as The method reaches a precision and accuracy of 1.0% (e.g., Cocherie et al. 2005). The SIMS (Secondary Ion Mass Spectrometry), on the other employs a primary ion beam and analyses the secondary ions. It focuses an  $O^-$  ion beam of ty >  $10\mu$ m in diameter on a solid sample surface, primarily applied to quantify major and trace of contents (for example, Pettke et al. 2004).

Many recent analytical methods, instead, "Inductively coupled plasma" ionization method of the sample, generating a fine aerosol which is in an Ar plasma (Horn et al. 2000). With Ar h high first ionization potential of 15.759 V, the ionizes all other elements to single-charged ions for He, F and Ne. The method was developed early 1980s for introduction of dissolved sa Likewise, the ICP array may be connected to system which ablates a solid sample whose vamaterial is then transported by a He gas flow i ICP unit. This method overcomes the need of ultr laboratory conditions and allows the selective sa of solid material on the micrometer scale. On tector side, the recent technology came up with collector (MC) arrangements which allow the s



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equipped with additional multichannel ion counters (MICs) for high-sensitivity isotope analyses. The equipment with additional MICs is only a spatial problem within the Faraday cup arrangement and, generally, 6–8 MICs may easily be accommodated, allowing the simultaneous analysis of about 15 isotopes.

The shortcomings of the laser ablation multi-collector inductively coupled plasma mass spectrometry (LA-MC-ICP-MS) relative to SHRIMP or conventional TIMS analyses have been its lower precision. The laser ablation process is not as stable as the SHRIMP method, or as the introduction of the sample in solution as in the case of TIMS. Firstly, this is due to the fragmentation and vaporization process of the solid material ablated. The *laser* beam may ablate parts of the mineral which are slightly fractured, altered or otherwise physically weakened or inhomogenized by previous geological processes, including the destruction of the mineral lattice by the proper radioactive radiation. The result is that the ablation and vaporization process of the material may vary in efficiency and completeness and, thus, the material transport to the plasma may not be continuous. Secondly, the carrier gas flux, normally ultrapure He, has an appreciable effect on the stability of the gas flow. Hence, the *laser* settings, such as *laser* intensity, laser frequency and beam diameter, together with the gas flow parameters, are fundamental for a reasonably stable signal reaching the detectors.

With the more recent developments, however, the analytical uncertainties are getting closer to those of SHRIMP (see Willigers et al. 2002). Bruguier et al. (2001) arrived at 6%, Horn et al. (2000) at 2%, Chang et al. (2006) at 4%, and Gerdes and Zeh (2006) at 3–4% precision or accuracy for U-Pb isotope ratios of natural materials. These values depend very much on the nature of the material analysed, such as its composition, presence of fractures, inclusions and heterogeneities. The LA-ICP-MS analyses may be even more precise for synthetic glass standards which are chemically and isotopically homogeneous (Bernal et al. 2005). Often, the largest uncertainty is given by the analysis of the standards (Chang et al. 2006) which are gener-

ysed, and with the relatively easy preparation of the samples, the *laser* ablation MC-ICP mass spectrometry certainly is the method of choice for the coming years for isotopic analysis of solid materials in the geo- and environmental sciences (Willigers et al. 2002, Košler and Sylvester 2003).

## SET-UP OF THE LASER ABLATION MC-ICP-MS U-Pb METHOD

The analytical equipment used in this study was installed at the "Laboratório de estudos geocronológicos, geodinâmicos e ambientais" of the Geosciences Institute of the University of Brasília, Brasília, Brazil, by initiative of Petróleo Brasileiro S/A – PETROBRAS and the "Ministério de Minas e Energia". The laboratory is part of the "Rede de Estudos Geodinâmicos e Ambientais – GEOCHRONOS". It was inaugurated in December 2006 and consists, apart from other installations and instrumentation, of a Thermo Finnigan *Neptune* multicollector inductively coupled plasma mass spectrometer. Attached to this is a New Wave  $213\mu m$  Nd-YAG solid state *laser* which provides the ablated material to the mass spectrometer.

#### SAMPLE PREPARATION

Sample preparation is straightforward. The minerals of interest, in this case zircon, are separated from the rock matrix by crushing the rock, concentrating the heavy mineral fraction by panning, separating the zircon grains by a Frantz magnetic separator, and final hand-picking of individual zircon grains. *In situ* analysis directly on a rock slab or thin section is also possible. However, it was found that the procedure of pre-concentration largely facilitates the measurements and localization of the zircons, so that it is worthwhile to be done.

The zircon grains are then located under the binocular one by one on a glass wafer covered with a double-sided tape in order to secure the grains. A 9 mm diameter plastic ring is placed on the tape around the zircons, and filled with two-compound epoxy. After 1-2 days of drying, the mounts are removed from the tape. Polishing of the mounts is done with 3 µm followed by 1 µm diamond



The mounts are then taken to an ultrasonic bath with 3% HNO<sub>3</sub>, and then cleaned with distilled water. A Nylon sample holder which takes three mounts was especially constructed. The three sites may be occupied with one standard and two samples, or with two standards and one sample.

#### THE LASER SET-UP

The sample chamber is flushed with He gas of analytical quality, which samples the ablated and vaporized material to be transported via Tygon tubes into the ICP. Before entering the *laser* sample chamber, the He passes through a glass tube filled with gold-coated quartz crystals (gold trap) to remove the largest part of mercury (Hg) whose isotope <sup>204</sup>Hg interferes with the <sup>204</sup>Pb isotope analysed to apply the common Pb correction. The He gas flux is commonly 0.35–0.45 L/min.

The laser is run at a frequency of 7-10 Hz and an energy of 30–36%, resulting in a *laser* energy of ca. 0.5 to 1.2 J/cm<sup>2</sup>. A small *laser* spot size of say  $30\mu m$ applied to a single spot with these laser conditions would not produce enough material for a reasonable signal, but at least  $40-50\mu m$  would be required, with the signal intensity deteriorating along duration of the analysis because of the deepening of the *laser* pit. This suggested the use of a raster scheme of the laser which samples only the surface of the zircon. The raster is composed of two parallel and a connecting line with a  $20\mu$ m spacing. With a  $30\mu$ m beam diameter applied here, the sampled area of the zircon is a square of about  $70\mu m$  on each side. With a speed of  $1\mu$ m/sec, the propagating laser spot takes about 1 min to pass the raster, which is enough time to collect the signal. This setting also avoids the prominent down-hole fractionation of isotopes which would require an additional correction, and a significantly higher laser energy to drill the zircon. Before signal collection, a pre-ablation run along the raster is applied to clean the mineral surface. The running conditions of this cleaning run are:  $40\mu m$  spot size, frequency 10 Hz and 25% laser energy.

THE ICP-MS AND MULTI-COLLECTOR SET-UP

tector arrangement consists of a central Faraday of 4 Faraday cups each on the high side and low sid centre cup (Fig. 2). For high-sensitivity analyse Pb and U isotopes, the mass spectrometer is ed with 6 ion counters (ICs, or multichannel ion c MICs). Four of them are fixed on the outermost H cup of the low side (cup L4), one on the third cup low side (cup L3), and one on the outermost Farac on the high side (cup H4). The latter is used of the analysis of <sup>238</sup>U in materials with extremely content. For the present application, we analyse on the Faraday cup H4. The other isotopes are co on the low side. The four ICs on the cup L4 at at defined distances referring to: one mass unit b L4 and IC5, one mass unit between IC5 and IC mass units between IC4 and IC3, and two mass between IC3 and IC2. The signals collected on t ICs are: <sup>207</sup>Pb on IC5, <sup>206</sup>Pb on IC4, <sup>204</sup>Hg/<sup>20</sup> IC3, and <sup>202</sup>Hg on IC2. Because of the always contamination of the He gas with Hg, a correct the isobaric interference between <sup>204</sup>Hg and <sup>204</sup> to be applied, using the signal of <sup>202</sup>Hg collected

#### DATA COLLECTION

With this collector set-up, five isotopes are analymultaneously. Before analysis, the Faraday of calibrated for baseline and gain, and the ICs for yield. To ensure the optimal operating voltage same sensitivity for the ICs, a signal of about 3 counts per second (cps) is successively directed at ICs using different analysing lines. We use a sof 206 Pb for this cross-calibration. Based on the response for each IC, the operating voltage of a sadjusted in order to ensure measuring condition the same sensitivity for all ICs used.

For standard and sample analysis, the sign collected in a single block with 40 cycles of 1.0 each. The *laser* is started and, when the si the detectors has reached its maximum, the 40 are taken. A typical analysis therefore takes a min and is illustrated in Figure 3. The isotopes  $^{204}(Ph+Hg)$   $^{206}Ph$  and  $^{207}Ph$  are read in counts to



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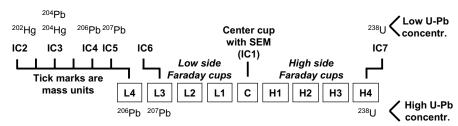


Fig. 2 – Set-up of the cup configurations (Faraday cups and ICs) for low U-Pb and high U-Pb concentrations in zircon with the Thermo Finnigan *Neptune* MC-ICP-MS.

a blank, a standard, and three samples, blank, standard, and so on. The method accounts for the drift of the instrument, and eliminates the need to correct for the mass bias of individual isotopes.

#### DATA REDUCTION

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The isotope data of the 40 analysed cycles are transferred into an in-house Excel spreadsheet for data reduction. The isotope ratios of the 40 cycles are evaluated on a  $2\sigma$  standard error rejection basis. The routine then calculates the error correlation value  $\rho$  (rho) for the <sup>206</sup>Pb/<sup>238</sup>U and <sup>207</sup>Pb/<sup>235</sup>U data. The isobaric contribution of <sup>204</sup>Hg is subtracted from the joint <sup>204</sup>Pb/<sup>204</sup>Hg peak by considering the analyzed <sup>202</sup>Hg/<sup>204</sup>Hg ratio. The spreadsheet allows to chose between three ways to determine the <sup>202</sup>Hg/<sup>204</sup>Hg value which is applied for correction: (i) from the mean of the two bracketing blanks, (ii) from the mean of the two bracketing (common Pb-free) standards, or (iii) from the mean of the four. Normally, the difference between the three determinations is minor. We consider this more favourable than applying the natural <sup>202</sup>Hg/<sup>204</sup>Hg ratio of 4.346, which would require an absolutely precise cross-calibration of IC2 and IC3. Because <sup>235</sup>U cannot be analysed with this type of cup configuration, the natural ratio <sup>238</sup>U/<sup>235</sup>U of 137.88 is used to calculate the <sup>235</sup>U intensity.

The correction for instrumental drift and mass bias is done by considering the two standards analysed before and after the samples, and the two blank analyses run before and after the samples, respectively, after applying a blank correction for all isotopes analysed. The normalization of the isotopic ratios of the samples

for which R<sub>std</sub> is the true isotopic ratio of the standard  $(^{207}\text{Pb}/^{206}\text{Pb} \text{ or } ^{206}\text{Pb}/^{238}\text{U ratios, respectively)}, r_{\text{spl}} \text{ is}$ the analysed isotopic ratio of the sample, and r<sub>std1</sub> and  $r_{\text{std2}}$  are the analysed isotopic ratios of the two standards before and after the samples along the sequence. The variable  $\theta$  (theta) is a time factor (Albarède et al. 2004) or, in other words, gives respective weight to the two standard measurements. It depends on the location of the samples within the analysing sequence, and takes values between 0 and 1. For example, three successive analyses run between two standards and two blanks suggest  $\theta = 0.25$ , 0.50 and 0.75 for samples 1, 2 and 3, respectively. The term  $(r_{std1}^{1-\theta} \times r_{std2}^{\theta})$  is a linear interpolation of the logarithms of the isotopic ratios, which accounts for the generally exponential instrumental drift. The same algorithm is applied to correct for the drift in the blank analyses. An alternative would be to inject a diluted thallium (Tl) solution to determine the mass bias of the Pb isotopes (e.g., Horn et al. 2000) which, however, does not allow the correction of U mass bias. The standard-sample bracketing approach applied here, therefore, certainly bears the least error for that analytical method, as it does not require intensive mass bias corrections.

The corrected <sup>206</sup>Pb/<sup>238</sup>U and <sup>207</sup>Pb/<sup>206</sup>Pb ratios so obtained are transferred into absolute age information using the software of Ludwig (2003). The software was also used to plot the Concordia diagrams. The errors of the <sup>206</sup>Pb/<sup>238</sup>U and <sup>207</sup>Pb/<sup>206</sup>Pb ratios were propagated by quadratic addition of the external reproducibility and the within-run precision, following equation (4):

$$/^{206} Pb$$
  $^{207} Pb$ 



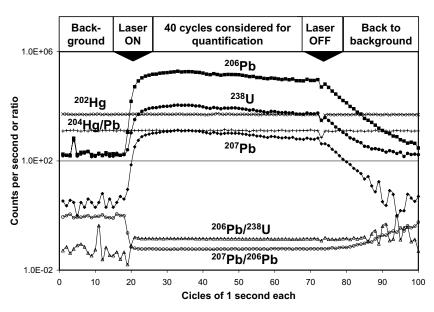


Fig. 3 – Typical signal sequence of a *laser* ablation experiment. Note that the absolute count rates of the isotopes may vary during the ablation process while the isotope ratios remain constant. The signals of <sup>202</sup>Hg and <sup>204</sup>Hg/Pb, in the case of no common <sup>204</sup>Pb present in the ablated sample, come solely from the Hg contents in the Ar gas, and are therefore not influenced by the ablation process.

with SD being the sample standard deviation  $\sigma$ :

$$\sigma = \sqrt{\frac{1}{N} \sum_{i=1}^{N} (x_i - x_m)^2}$$
 (5)

where N is the number of analyses,  $x_i$  is the value of each individual analyses  $x_i$  to  $x_N$ , and  $x_m$  is the arithmetic mean of all analyses. Whereas the SD is independent of the number of analyses, the standard error SE:

$$SE = \frac{\sigma}{\sqrt{N}}$$
 (6)

decreases with the number of analyses N taken. The external reproducibility (2 SD $_{\rm analysed}^{\wedge 2}$ ) is represented by the standard deviation obtained by repeated analysis of standard zircon GJ-1 which were run during the analytical session (generally  $\sim 0.8\%$  for  $^{207}\text{Pb}/^{206}\text{Pb}$ , and  $\sim 1\%$  for  $^{206}\text{Pb}/^{238}\text{U}$ ). The within-run precision (2 SE $_{\rm analysed}^{\wedge 2}$ ) is the standard error calculated for each analysis. The resulting errors are  $2\sigma$  standard deviations.

Zircon U-Ph isotonic analyses may require a correc

al. 2003). For minerals with a low common Pb as, for example, zircon, we use a correction based amount of non-radiogenic  $^{204}$ Pb. The counts per of  $^{204}$ Pb (including a correction for  $^{204}$ Hg) are deduce the amount of non-radiogenic, common and  $^{207}$ Pb, given a common Pb composition for the model of Stacey and Kramers (1975). With the tion  $f_c$  of common  $^{206}$ Pb and  $^{207}$ Pb so obtained:

$$f_c \,=\, \frac{Pb_c}{Pb_t} \,=\, \frac{Pb_c}{Pb_c + Pb_r}$$

where Pb<sub>c</sub> is the value (in counts per second) of counts, Pb<sub>t</sub> the total Pb, and Pb<sub>r</sub> the radiogenic Pb, being <sup>206</sup>Pb or <sup>207</sup>Pb, respectively, we use the reships:

$$\frac{^{206}Pb}{^{238}U_{radiogenic}} \, = \, \frac{^{206}Pb}{^{238}U_{total}} \times (1-f_c), \label{eq:equation_prob}$$

and

$$\frac{207 \text{Pb}}{235 \text{LL}} = \frac{207 \text{Pb}}{235 \text{LL}}$$



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of Andersen (2002) to arrive at common Pb-corrected  $^{206}\text{Pb}/^{238}\text{U}$  and  $^{207}\text{Pb}/^{235}\text{U}$  isotopic ratios. The necessity for a correction is judged from the  $^{204}\text{Pb}$  signal intensity. Values smaller than  $\sim 25$  cps (blank-corrected), resulting in  $^{206}\text{Pb}/^{204}\text{Pb}$  ratios well beyond 3000, suggest an insignificant common Pb content which would not recognizably effect the calculated ages. All zircons analysed in this study met this condition, and therefore did not require a correction.

#### STANDARDS AND SAMPLES

Three international zircon standards were analysed, using each one as an external standard and correcting the remaining two against it. This yields a set of 6 isotope ratio and age data which are compared with the certified values of the standards (see Table I). The standards are: (i) GJ-1 zircon standard provided by the ARC National Key Centre for Geochemical Evolution and Metallogeny of Continents (GEMOC), Australia. This is a gem-quality zircon crystal of about 0.7 cm in diameter which was broken and prepared for analysis. Its reference age after Jackson et al. (2004) is: <sup>207</sup>Pb/<sup>206</sup>Pb age  $= 608.6 \pm 1.1$  Ma,  $^{206}$ Pb/ $^{238}$ U age  $= 600.4 \pm 1.8$  Ma,  $^{207}\text{Pb}/^{235}\text{U}$  age = 602.1  $\pm$  3.0 Ma; (ii) Temora 2, provided by Lance Black, Geoscience Australia, Australia, which comes from the Middledale gabbroic diorite in eastern Australia; the zircon crystals have a size of about 300–500  $\mu$ m and, prior to sample preparation, the concentrate was hand-picked to obtain a high-purity zircon concentrate. Its reference age after Black et al. (2004) is:  ${}^{207}\text{Pb}/{}^{206}\text{Pb}$  age = 419.1  $\pm$  9.1 Ma,  ${}^{206}\text{Pb}/{}^{238}\text{U}$  age  $= 416.2 \pm 1.1 \text{ Ma}, \frac{207 \text{Pb}}{235} \text{U age} = 416.7 \pm 1.7 \text{ Ma};$ (iii) FC1 zircon concentrate provided by Richard Armstrong, Australian National University, Canberra, Australia; the crystals have sizes of approximately 50- $100\mu m$ , and were hand-picked prior to sample preparation; they were extracted from the Duluth Complex in the U.S.A. Its reference age (Paces and Miller 1993) is:  $^{207}\text{Pb}/^{206}\text{Pb}$  age = 1098.9 Ma,  $^{206}\text{Pb}/^{238}\text{U}$  age =

For an additional test of the method, two zircon samples from our own laboratory which had previously

 $1099.9 \text{ Ma}, \frac{207}{\text{Pb}}/\frac{235}{\text{U}} \text{ age} = 1100.0 \text{ Ma}.$ 

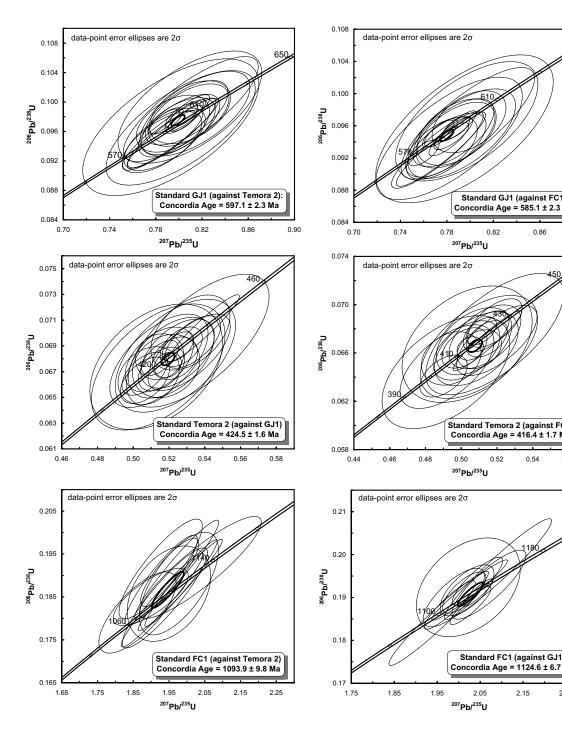
of the Neoproterozoic Goiás magmatic arc which has previously been dated at  $630 \pm 5$  Ma  $(2\sigma)$  by U-Pb ID-TIMS in our laboratory (Laux et al. 2005). Its average  $^{207}\text{Pb}/^{206}\text{Pb}$  TIMS age is  $633.3 \pm 5.7$  Ma. The other sample (EC69A) has much older zircon crystals and went through a more complex geological history. They were extracted from a migmatized hornblende- and biotite-bearing tonalite from an Archean nucleus of the São José do Campestre Massif in the Borborema Province, NE Brazil. The zircons yielded an upper intercept age of  $3065 \pm 12$  Ma determined by SHRIMP analysis (Dantas et al. unpublished data).

#### RESULTS

Between 13 and 23 analyses were run for the standards GJ1, Temora 2 and FC1. Figure 4 shows the ages obtained for each standard normalized against one another in a Concordia diagram, and Table I summarizes the data obtained. The concordance between the values obtained and the referenced standard data of the <sup>207</sup>Pb/<sup>206</sup>Pb,  $^{206}\text{Pb}/^{238}\text{U}$  and  $^{207}\text{Pb}/^{235}\text{U}$  age data is well satisfactory. We obtained precisions of 1.9 to 3.7% ( $2\sigma$  standard deviation) for the  $^{207}$ Pb/ $^{206}$ Pb,  $^{206}$ Pb/ $^{238}$ U and  $^{207}$ Pb/ $^{235}$ U age data, depending on the isotope system and on the particular standard. The accuracy was calculated as the percentage of deviation between the analysed Concordia age and the referenced <sup>207</sup>Pb/<sup>206</sup>Pb age. The Concordia age, following Ludwig (2003) is, "the most-probable age for a data-point (or weighted-mean data-point) on a Concordia diagram, where the true location of the data point is assumed to fall precisely on the Concordia curve". Because not all referenced standards provide the error correlation coefficient to calculate that age, their referenced <sup>207</sup>Pb/<sup>206</sup>Pb age was used. The accuracy so obtained varies between 0.6 and 3.8% ( $2\sigma$  standard deviation).

The majority of the 23 analyses obtained for the natural sample HD66 (Table II) were taken as multiple analyses on different localities of individual grains. They are all concordant (Fig. 5), yielding a Concordia age of  $627.6 \pm 1.3$  Ma, which is identical within error to the TIMS age of  $630 \pm 5$  Ma. None of the zir-







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TABLE I
Referenced and determined ages (by LA-ICP-MS) of the zircon standards GJ1, Temora 2 and FC1.

Sample	Standard	No. of anal.	207Pb*/ 206Pb* age (Ma) referenced	Error (2σ) (Ma)	207Pb*/ 206Pb* age (Ma) analysed	Error $(2\sigma)$ $(Ma)$	Prec. (2σ) (%)	206Pb*/ 238U age (Ma) referenced	Error $(2\sigma)$ $(Ma)$	206 <sub>Pb*/</sub> 238 <sub>U</sub> age (Ma) analysed	Error $(2\sigma)$ $(Ma)$	Prec. (2σ) (%)
GJ1	Temora 2	23	608.6	1.1	598.4	6.3	2.8	600.4	1.8	598.3	20.2	2.7
GJ1	FC1	20	608.6	1.1	583.7	6.1	2.4	600.4	1.8	584.0	19.8	2.3
Temora 2	GJ1	23	419.1	9.1	424.8	16.5	2.9	416.2	1.1	424.9	12.9	2.8
Temora 2	FC1	20	419.1	9.1	414.9	16.6	3.5	416.2	1.1	414.9	12.6	3.5
FC1	Temora 2	13	1098.9	n.r.	1111.6	5.5	3.7	1099.9	n.r.	1109.9	30.4	3.4
FC1	GJ1	13	1098.9	n.r.	1127.8	4.8	2.9	1099.9	n.r.	1127.2	25.5	2.7

Sample	Standard	No. of anal.	207 <sub>Pb*/</sub> 235 <sub>U</sub> age (Ma) referenced	Error (2σ) (Ma)	207 <sub>Pb*/</sub> 235 <sub>U</sub> age (Ma) analysed	Error (2σ) (Ma)	Prec. (2σ) (%)	Concordia age (Ma) determined	Error (2σ) (Ma)	Accuracy (%)
GJ1	Temora 2	23	602.1	3.0	596.7	15.9	1.6	597.1	2.3	1.9
GJ1	FC1	20	602.1	3.0	587.7	15.7	1.9	585.1	2.3	3.9
Temora 2	GJ1	23	416.7	1.7	426.6	10.8	2.8	424.5	1.6	1.3
Temora 2	FC1	20	416.7	1.7	415.9	10.6	3.7	416.4	1.7	0.6
FC1	Temora 2	13	1100.0	n.r.	1098.0	24.7	2.6	1093.9	9.8	0.5
FC1	GJ1	13	1100.0	n.r.	1123.3	21.9	2.2	1124.6	6.7	2.3

Referenced values from: GJ1 (Jackson et al. 2004), Temora 2 (Black et al. 2004), FC1 (Paces and Miller 1993). Precision (Prec.):  $2\sigma$  precision for the number of analyses, "n.r." = not reported. All errors are  $2\sigma$  standard deviations. Accuracy: Percentage of deviation between analysed concordia age and referenced  $^{207}$ Pb/ $^{206}$ Pb age.

weighted average of 24  $^{207}$ Pb/ $^{206}$ Pb ages resulted in a  $^{207}$ Pb/ $^{206}$ Pb age of 628.7  $\pm$  6.0 Ma, compared with the TIMS  $^{207}$ Pb/ $^{206}$ Pb age of 633.3  $\pm$  5.7 Ma.

Sample EC69A shows a more complex zircon population, as seen from 24 SHRIMP (Table III) and 35 LA-ICP-MS analyses (Table IV). Most of the LA-ICP-MS analyses were taken as multiple shots on individual zircon grains. None of the zircons required a common Pb correction. The ICP-MS analyses display various groups of zircons plotting on supposedly different Discordia lines (Fig. 6). The youngest upper intercept age, defined by four discordant and three concordant analytical points, yields the age of  $3045 \pm 24$  Ma, which agrees within error with the SHRIMP age of  $3065 \pm 12$  Ma. However, various older zircon populations were encountered in the sample. One is defined by 17 discordant zircon analyses which yield an upper

ulations may relate to 3.4–3.5 Ga ages reported from the same area by Dantas et al. (2004). Another group of five highly discordant zircon analyses with extremely low <sup>206</sup>Pb/<sup>238</sup>U ratios may represent still another, even older geological event. Three analyses on grain 14 (see Table IV, but not included in Fig. 6) yielded one concordant and two nearly concordant data with ages between 540 and 570 Ma. They represent another event of resetting of the isotope system during the Neoproterozoic/Cambrian Brasiliano cycle. Therefore, the Discordias of all older zircon populations were anchored to 558 Ma, which is the mean of these three analyses.

#### DISCUSSION AND CONCLUSIONS

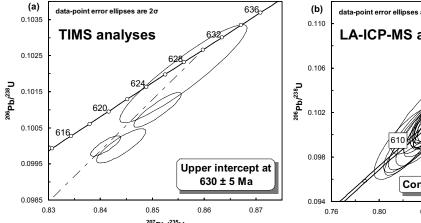
A comparison of the LA-ICP-MS results of the natural sample HD66 with TIMS analyses shows a fine confor-

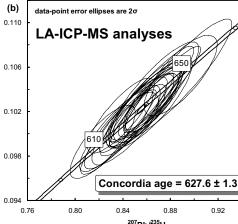


TABLE II
TIMS and LA-ICP-MS analyses of sample HD66.

						TIM	S						
	207 <sub>Pb*/</sub>	$2\sigma$	207 <sub>Pb*/</sub>	2σ	206 <sub>Pb*/</sub>	2σ		207 <sub>Pb/</sub>	2σ	207 <sub>Pb*/</sub>	2σ	206 <sub>Pb*/</sub>	2
Analysis	206 <sub>Pb*</sub>	error	235 <sub>IJ</sub>	error	238 <sub>IJ</sub>	error	ρ	206 <sub>Pb</sub>	error	235 <sub>U</sub>	error	$^{238}\mathrm{U}$	er
	PD-	(%)		(%)		(%)		age	(Ma)	age	(Ma)	age	(N
1	0.0609	0.16	0.841	0.28	0.100	0.23	0.82	637.0	3.5	619.7	1.3	614.4	1.
2	0.0609	0.24	0.844	0.46	0.100	0.39	0.84	636.0	5.3	621.4	2.1	614.4	2.
3	0.0608	0.20	0.851	0.44	0.101	0.39	0.89	634.0	4.3	625.2	2.1	620.3	2.
4	0.0606	0.44	0.856	1.17	0.102	1.09	0.93	626.0	9.5	627.9	5.5	626.1	6.
LA-ICP-MS													
1	0.06112	1.6	0.8864	2.5	0.10499	2.5	0.91	643.5	33.9	644.4	11.9	643.6	15
2	0.06054	2.2	0.8511	1.6	0.10147	1.6	0.63	622.8	46.3	625.2	7.4	623.0	9.
3a	0.06068	1.0	0.8566	2.8	0.10230	2.8	0.94	627.9	22.4	628.2	12.9	627.9	16
3b	0.06054	1.2	0.8474	2.7	0.10147	2.7	0.93	623.0	26.1	623.2	12.5	623.0	16
3c	0.06082	1.1	0.8658	2.0	0.10316	2.0	0.90	632.8	22.5	633.3	9.5	632.9	12
4	0.06116	1.5	0.8885	1.9	0.10525	1.9	0.76	645.0	31.2	645.5	9.2	645.1	11
5a	0.06094	2.0	0.8666	2.2	0.10385	2.2	0.86	637.2	42.8	633.7	10.5	636.9	13
5b	0.06090	1.7	0.8637	2.4	0.10358	2.4	0.92	635.7	37.2	632.1	11.0	635.3	14
6a	0.06080	1.9	0.8653	2.3	0.10303	2.3	0.77	632.1	39.7	633.0	10.9	632.2	14
6b	0.06076	1.6	0.8642	1.7	0.10283	1.7	0.75	630.8	33.1	632.4	7.8	631.0	10
6c	0.06077	2.0	0.8632	2.5	0.10284	2.5	0.82	630.9	41.9	631.8	11.8	631.0	15
7a	0.06085	1.0	0.8671	1.9	0.10333	1.9	0.94	633.9	21.0	634.0	8.9	633.9	11
7b	0.06079	1.1	0.8637	1.7	0.10296	1.7	0.87	631.7	24.0	632.1	7.9	631.7	10
7c	0.06083	1.2	0.8662	1.6	0.10319	1.6	0.89	633.1	26.6	633.5	7.6	633.1	9.
8a	0.06049	1.1	0.8441	2.1	0.10114	2.1	0.90	621.0	23.5	621.4	9.5	621.1	12
8b	0.06059	1.3	0.8657	2.2	0.10188	2.2	0.83	624.6	27.7	633.2	10.1	625.4	12
8c	0.06069	1.7	0.8571	2.2	0.10236	2.2	0.82	628.2	35.9	628.6	10.1	628.2	13
9	0.06056	1.6	0.8524	2.5	0.10161	2.5	0.83	623.6	34.3	626.0	11.4	623.8	14
10a	0.06018	2.1	0.8231	2.6	0.09928	2.6	0.80	610.2	44.8	609.8	11.7	610.2	14
10b	0.06046	1.8	0.8424	2.4	0.10097	2.4	0.88	620.0	38.4	620.5	10.9	620.1	14
10c	0.06051	2.1	0.8484	2.9	0.10127	2.9	0.85	621.7	45.7	623.8	13.5	621.9	17
11a	0.06035	1.4	0.8346	2.3	0.10028	2.3	0.86	616.1	29.3	616.1	10.7	616.1	13
11b	0.06057	1.4	0.8485	1.8	0.10162	1.8	0.76	623.9	30.3	623.8	8.4	623.9	10

Note: Analyses with letters (a, b, c) indicate analyses on the same zircon grain. All errors are  $2\sigma$  standard deviations.





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TABLE III
SHRIMP data of sample EC69A.

Analysis         206 <sub>Pb*</sub> error (%)         235 <sub>U</sub> error (%)         238 <sub>U</sub> error (%)         238 <sub>U</sub> error (%)         206 <sub>Pb*</sub> error age (Ma)         235 <sub>U</sub> age (Ma)         error age (Ma)         238 <sub>U</sub> age (Ma)         230 <sub>U</sub> age (Ma) <th< th=""><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th>_</th><th>207</th><th></th><th>207</th><th></th><th>206</th><th></th></th<>								_	207		207		206	
Analysis         206pb*         error (%)         235 U         error (%)         238 U         error (%)         206pb         error dage (Ma)         235 U         error dage (Ma)         238 U         error dage (Ma)         238 U         error dage (Ma)         238 U         error (Ma)         238 U         237 U         237 U         238 U         237 U         238 U		207Pb*/	1σ	207Pb*/	$1\sigma$	206Pb*/	$1\sigma$		<sup>207</sup> Pb/	$1\sigma$	<sup>207</sup> Pb*/	$1\sigma$	<sup>206</sup> Pb*/	$1\sigma$
Columb   C	Analysis			1	error		error	ρ	<sup>206</sup> Pb	error	235U	error	238U	error
2         0.22398         0.26         17.02         1.6         0.5512         1.5         0.99         3010         4.2         2936         15.5         2830         34           3         0.22960         0.59         18.61         1.6         0.5877         1.4         0.92         3049         9.6         3022         15.5         2980         33           4a         0.17531         0.17         5.20         1.5         0.2153         1.5         0.99         2609         2.8         1853         12.9         1257         17           4b         0.23401         0.24         17.90         1.5         0.5547         1.5         0.99         3080         3.9         2984         14.5         2845         35           5         0.22896         0.20         18.83         1.5         0.5964         1.4         0.99         3045         3.2         3033         14.6         3015         33           6         0.23269         0.11         18.40         1.4         0.5734         1.4         1.09         3071         1.7         3011         13.6         2922         33           7         0.22065         0.33         15.63<			(%)	_	(%)		(%)		age	(Ma)	age	(Ma)	age	(Ma)
3         0.22960         0.59         18.61         1.6         0.5877         1.4         0.92         3049         9.6         3022         15.5         2980         33           4a         0.17531         0.17         5.20         1.5         0.2153         1.5         0.99         2609         2.8         1853         12.9         1257         17           4b         0.23401         0.24         17.90         1.5         0.5547         1.5         0.99         3080         3.9         2984         14.5         2845         35           5         0.22896         0.20         18.83         1.5         0.5964         1.4         0.99         3045         3.2         3033         14.6         3015         33           6         0.23269         0.11         18.40         1.4         0.5734         1.4         1.00         3071         1.7         3011         13.6         2922         33           7         0.22065         0.33         15.63         1.5         0.5139         1.5         0.98         2986         5.4         2854         14.4         2673         33           8a         0.22978         0.36         17.77	1	0.23187	0.16	18.88	1.4	0.5904	1.4	0.99	3065	2.6	3036	13.6	2991	34
4a         0.17531         0.17         5.20         1.5         0.2153         1.5         0.99         2609         2.8         1853         12.9         1257         17           4b         0.23401         0.24         17.90         1.5         0.5547         1.5         0.99         3080         3.9         2984         14.5         2845         35           5         0.22896         0.20         18.83         1.5         0.5964         1.4         0.99         3045         3.2         3033         14.6         3015         33           6         0.23269         0.11         18.40         1.4         0.5734         1.4         1.00         3071         1.7         3011         13.6         2922         33           7         0.22065         0.33         15.63         1.5         0.5139         1.5         0.98         2986         5.4         2854         14.4         2673         33           8a         0.22975         0.22         18.74         1.5         0.5909         1.4         0.99         3071         3.2         3070         13.6         3069         34           9         0.22789         0.36         17.77	2	0.22398	0.26	17.02	1.6	0.5512	1.5	0.99	3010	4.2	2936	15.5	2830	34
4b         0.23401         0.24         17.90         1.5         0.5547         1.5         0.99         3080         3.9         2984         14.5         2845         35           5         0.22896         0.20         18.83         1.5         0.5964         1.4         0.99         3045         3.2         3033         14.6         3015         33           6         0.23269         0.11         18.40         1.4         0.5734         1.4         1.00         3071         1.7         3011         13.6         2922         33           7         0.22065         0.33         15.63         1.5         0.5139         1.5         0.98         2986         5.4         2854         14.4         2673         33           8a         0.222995         0.22         18.74         1.5         0.5909         1.4         0.99         3052         3.5         3029         14.6         2993         34           8b         0.23278         0.20         19.57         1.4         0.6098         1.4         0.99         3071         3.2         3070         13.6         3069         34           9         0.22789         0.36         17.	3	0.22960	0.59	18.61	1.6	0.5877	1.4	0.92	3049	9.6	3022	15.5	2980	33
5         0.22896         0.20         18.83         1.5         0.5964         1.4         0.99         3045         3.2         3033         14.6         3015         33           6         0.23269         0.11         18.40         1.4         0.5734         1.4         1.00         3071         1.7         3011         13.6         2922         33           7         0.22065         0.33         15.63         1.5         0.5139         1.5         0.98         2986         5.4         2854         14.4         2673         33           8a         0.222995         0.22         18.74         1.5         0.5909         1.4         0.99         3052         3.5         3029         14.6         2993         34           8b         0.23278         0.20         19.57         1.4         0.6098         1.4         0.99         3071         3.2         3070         13.6         3069         34           9         0.22789         0.36         17.77         1.5         0.5654         1.4         0.97         3037         5.8         2977         14.5         2889         33           10         0.22748         0.34         16.	4a	0.17531	0.17	5.20	1.5	0.2153	1.5	0.99	2609	2.8	1853	12.9	1257	17
6         0.23269         0.11         18.40         1.4         0.5734         1.4         1.00         3071         1.7         3011         13.6         2922         33           7         0.22065         0.33         15.63         1.5         0.5139         1.5         0.98         2986         5.4         2854         14.4         2673         33           8a         0.22995         0.22         18.74         1.5         0.5909         1.4         0.99         3052         3.5         3029         14.6         2993         34           8b         0.23278         0.20         19.57         1.4         0.6098         1.4         0.99         3071         3.2         3070         13.6         3069         34           9         0.22789         0.36         17.77         1.5         0.5654         1.4         0.97         3037         5.8         2977         14.5         2889         33           10         0.22748         0.34         16.34         1.5         0.5210         1.4         0.97         3034         5.5         2897         14.5         2703         31           11         0.23340         0.41         19.	4b	0.23401	0.24	17.90	1.5	0.5547	1.5	0.99	3080	3.9	2984	14.5	2845	35
7         0.22065         0.33         15.63         1.5         0.5139         1.5         0.98         2986         5.4         2854         14.4         2673         33           8a         0.22995         0.22         18.74         1.5         0.5909         1.4         0.99         3052         3.5         3029         14.6         2993         34           8b         0.23278         0.20         19.57         1.4         0.6098         1.4         0.99         3071         3.2         3070         13.6         3069         34           9         0.22789         0.36         17.77         1.5         0.5654         1.4         0.97         3037         5.8         2977         14.5         2889         33           10         0.22748         0.34         16.34         1.5         0.5210         1.4         0.97         3034         5.5         2897         14.5         2703         31           11         0.23340         0.41         19.46         1.6         0.6047         1.5         0.96         3076         6.6         3065         15.6         3049         37           12         0.22859         0.26         15	5	0.22896	0.20	18.83	1.5	0.5964	1.4	0.99	3045	3.2	3033	14.6	3015	33
8a         0.22995         0.22         18.74         1.5         0.5909         1.4         0.99         3052         3.5         3029         14.6         2993         34           8b         0.23278         0.20         19.57         1.4         0.6098         1.4         0.99         3071         3.2         3070         13.6         3069         34           9         0.22789         0.36         17.77         1.5         0.5654         1.4         0.97         3037         5.8         2977         14.5         2889         33           10         0.22748         0.34         16.34         1.5         0.5210         1.4         0.97         3034         5.5         2897         14.5         2703         31           11         0.2340         0.41         19.46         1.6         0.6047         1.5         0.96         3076         6.6         3065         15.6         3049         37           12         0.22859         0.26         15.47         1.5         0.4907         1.4         0.98         3042         4.2         2845         14.4         2574         30           13         0.22691         0.13         17	6	0.23269	0.11	18.40	1.4	0.5734	1.4	1.00	3071	1.7	3011	13.6	2922	33
8b         0.23278         0.20         19.57         1.4         0.6098         1.4         0.99         3071         3.2         3070         13.6         3069         34           9         0.22789         0.36         17.77         1.5         0.5654         1.4         0.97         3037         5.8         2977         14.5         2889         33           10         0.22748         0.34         16.34         1.5         0.5210         1.4         0.97         3034         5.5         2897         14.5         2703         31           11         0.23340         0.41         19.46         1.6         0.6047         1.5         0.96         3076         6.6         3065         15.6         3049         37           12         0.22859         0.26         15.47         1.5         0.4907         1.4         0.98         3042         4.2         2845         14.4         2574         30           13         0.22691         0.13         17.89         1.4         0.5719         1.4         1.00         3030         2.1         2984         13.6         2915         32           14         0.23221         0.14         1	7	0.22065	0.33	15.63	1.5	0.5139	1.5	0.98	2986	5.4	2854	14.4	2673	33
9         0.22789         0.36         17.77         1.5         0.5654         1.4         0.97         3037         5.8         2977         14.5         2889         33           10         0.22748         0.34         16.34         1.5         0.5210         1.4         0.97         3034         5.5         2897         14.5         2703         31           11         0.23340         0.41         19.46         1.6         0.6047         1.5         0.96         3076         6.6         3065         15.6         3049         37           12         0.22859         0.26         15.47         1.5         0.4907         1.4         0.98         3042         4.2         2845         14.4         2574         30           13         0.22691         0.13         17.89         1.4         0.5719         1.4         1.00         3030         2.1         2984         13.6         2915         32           14         0.23221         0.14         19.22         1.4         0.6003         1.4         1.00         3067         2.2         3053         13.6         3031         34           15         0.22759         0.23         1	8a	0.22995	0.22	18.74	1.5	0.5909	1.4	0.99	3052	3.5	3029	14.6	2993	34
10         0.22748         0.34         16.34         1.5         0.5210         1.4         0.97         3034         5.5         2897         14.5         2703         31           11         0.23340         0.41         19.46         1.6         0.6047         1.5         0.96         3076         6.6         3065         15.6         3049         37           12         0.22859         0.26         15.47         1.5         0.4907         1.4         0.98         3042         4.2         2845         14.4         2574         30           13         0.22691         0.13         17.89         1.4         0.5719         1.4         1.00         3030         2.1         2984         13.6         2915         32           14         0.23221         0.14         19.22         1.4         0.6003         1.4         1.00         3067         2.2         3053         13.6         3031         34           15         0.22759         0.23         17.75         1.5         0.5655         1.5         0.99         3035         3.7         2976         14.5         2889         35           16         0.23251         0.09	8b	0.23278	0.20	19.57	1.4	0.6098	1.4	0.99	3071	3.2	3070	13.6	3069	34
11         0.23340         0.41         19.46         1.6         0.6047         1.5         0.96         3076         6.6         3065         15.6         3049         37           12         0.22859         0.26         15.47         1.5         0.4907         1.4         0.98         3042         4.2         2845         14.4         2574         30           13         0.22691         0.13         17.89         1.4         0.5719         1.4         1.00         3030         2.1         2984         13.6         2915         32           14         0.23221         0.14         19.22         1.4         0.6003         1.4         1.00         3067         2.2         3053         13.6         3031         34           15         0.22759         0.23         17.75         1.5         0.5655         1.5         0.99         3035         3.7         2976         14.5         2889         35           16         0.23251         0.09         18.21         1.4         0.5680         1.4         1.00         3069         1.4         3001         13.6         2900         33           17         0.23087         0.12	9	0.22789	0.36	17.77	1.5	0.5654	1.4	0.97	3037	5.8	2977	14.5	2889	33
12         0.22859         0.26         15.47         1.5         0.4907         1.4         0.98         3042         4.2         2845         14.4         2574         30           13         0.22691         0.13         17.89         1.4         0.5719         1.4         1.00         3030         2.1         2984         13.6         2915         32           14         0.23221         0.14         19.22         1.4         0.6003         1.4         1.00         3067         2.2         3053         13.6         3031         34           15         0.22759         0.23         17.75         1.5         0.5655         1.5         0.99         3035         3.7         2976         14.5         2889         35           16         0.23251         0.09         18.21         1.4         0.5680         1.4         1.00         3069         1.4         3001         13.6         2900         33           17         0.23087         0.12         18.37         1.4         0.5772         1.4         1.00         3058         1.9         3009         13.6         2937         33           18         0.22915         0.32	10	0.22748	0.34	16.34	1.5	0.5210	1.4	0.97	3034	5.5	2897	14.5	2703	31
13         0.22691         0.13         17.89         1.4         0.5719         1.4         1.00         3030         2.1         2984         13.6         2915         32           14         0.23221         0.14         19.22         1.4         0.6003         1.4         1.00         3067         2.2         3053         13.6         3031         34           15         0.22759         0.23         17.75         1.5         0.5655         1.5         0.99         3035         3.7         2976         14.5         2889         35           16         0.23251         0.09         18.21         1.4         0.5680         1.4         1.00         3069         1.4         3001         13.6         2900         33           17         0.23087         0.12         18.37         1.4         0.5772         1.4         1.00         3058         1.9         3009         13.6         2937         33           18         0.22915         0.32         17.01         1.5         0.5382         1.4         0.98         3046         5.1         2935         14.5         2776         32           19         0.21750         0.68	11	0.23340	0.41	19.46	1.6	0.6047	1.5	0.96	3076	6.6	3065	15.6	3049	37
14         0.23221         0.14         19.22         1.4         0.6003         1.4         1.00         3067         2.2         3053         13.6         3031         34           15         0.22759         0.23         17.75         1.5         0.5655         1.5         0.99         3035         3.7         2976         14.5         2889         35           16         0.23251         0.09         18.21         1.4         0.5680         1.4         1.00         3069         1.4         3001         13.6         2900         33           17         0.23087         0.12         18.37         1.4         0.5772         1.4         1.00         3058         1.9         3009         13.6         2937         33           18         0.22915         0.32         17.01         1.5         0.5382         1.4         0.98         3046         5.1         2935         14.5         2776         32           19         0.21750         0.68         15.98         1.6         0.5327         1.5         0.91         2962         11         2876         15.4         2753         34           20         0.22271         0.44         1	12	0.22859	0.26	15.47	1.5	0.4907	1.4	0.98	3042	4.2	2845	14.4	2574	30
15         0.22759         0.23         17.75         1.5         0.5655         1.5         0.99         3035         3.7         2976         14.5         2889         35           16         0.23251         0.09         18.21         1.4         0.5680         1.4         1.00         3069         1.4         3001         13.6         2900         33           17         0.23087         0.12         18.37         1.4         0.5772         1.4         1.00         3058         1.9         3009         13.6         2937         33           18         0.22915         0.32         17.01         1.5         0.5382         1.4         0.98         3046         5.1         2935         14.5         2776         32           19         0.21750         0.68         15.98         1.6         0.5327         1.5         0.91         2962         11         2876         15.4         2753         34           20         0.22271         0.44         15.34         1.5         0.4996         1.4         0.96         3000         7.1         2837         14.4         2612         30           21         0.23329         0.19         1	13	0.22691	0.13	17.89	1.4	0.5719	1.4	1.00	3030	2.1	2984	13.6	2915	32
16         0.23251         0.09         18.21         1.4         0.5680         1.4         1.00         3069         1.4         3001         13.6         2900         33           17         0.23087         0.12         18.37         1.4         0.5772         1.4         1.00         3058         1.9         3009         13.6         2937         33           18         0.22915         0.32         17.01         1.5         0.5382         1.4         0.98         3046         5.1         2935         14.5         2776         32           19         0.21750         0.68         15.98         1.6         0.5327         1.5         0.91         2962         11         2876         15.4         2753         34           20         0.22271         0.44         15.34         1.5         0.4996         1.4         0.96         3000         7.1         2837         14.4         2612         30           21         0.23329         0.19         19.00         1.4         0.5906         1.4         0.99         3075         3.1         3042         13.6         2992         34	14	0.23221	0.14	19.22	1.4	0.6003	1.4	1.00	3067	2.2	3053	13.6	3031	34
17         0.23087         0.12         18.37         1.4         0.5772         1.4         1.00         3058         1.9         3009         13.6         2937         33           18         0.22915         0.32         17.01         1.5         0.5382         1.4         0.98         3046         5.1         2935         14.5         2776         32           19         0.21750         0.68         15.98         1.6         0.5327         1.5         0.91         2962         11         2876         15.4         2753         34           20         0.22271         0.44         15.34         1.5         0.4996         1.4         0.96         3000         7.1         2837         14.4         2612         30           21         0.23329         0.19         19.00         1.4         0.5906         1.4         0.99         3075         3.1         3042         13.6         2992         34	15	0.22759	0.23	17.75	1.5	0.5655	1.5	0.99	3035	3.7	2976	14.5	2889	35
18         0.22915         0.32         17.01         1.5         0.5382         1.4         0.98         3046         5.1         2935         14.5         2776         32           19         0.21750         0.68         15.98         1.6         0.5327         1.5         0.91         2962         11         2876         15.4         2753         34           20         0.22271         0.44         15.34         1.5         0.4996         1.4         0.96         3000         7.1         2837         14.4         2612         30           21         0.23329         0.19         19.00         1.4         0.5906         1.4         0.99         3075         3.1         3042         13.6         2992         34	16	0.23251	0.09	18.21	1.4	0.5680	1.4	1.00	3069	1.4	3001	13.6	2900	33
19     0.21750     0.68     15.98     1.6     0.5327     1.5     0.91     2962     11     2876     15.4     2753     34       20     0.22271     0.44     15.34     1.5     0.4996     1.4     0.96     3000     7.1     2837     14.4     2612     30       21     0.23329     0.19     19.00     1.4     0.5906     1.4     0.99     3075     3.1     3042     13.6     2992     34	17	0.23087	0.12	18.37	1.4	0.5772	1.4	1.00	3058	1.9	3009	13.6	2937	33
20     0.22271     0.44     15.34     1.5     0.4996     1.4     0.96     3000     7.1     2837     14.4     2612     30       21     0.23329     0.19     19.00     1.4     0.5906     1.4     0.99     3075     3.1     3042     13.6     2992     34	18	0.22915	0.32	17.01	1.5	0.5382	1.4	0.98	3046	5.1	2935	14.5	2776	32
21 0.23329 0.19 19.00 1.4 0.5906 1.4 0.99 3075 3.1 3042 13.6 2992 34	19	0.21750	0.68	15.98	1.6	0.5327	1.5	0.91	2962	11	2876	15.4	2753	34
	20	0.22271	0.44	15.34	1.5	0.4996	1.4	0.96	3000	7.1	2837	14.4	2612	30
22 0 22929 0 10 17 43 1 4 0 5513 1 4 1 0 0 3047 1 6 2959 13 5 2830 32	21	0.23329	0.19	19.00	1.4	0.5906	1.4	0.99	3075	3.1	3042	13.6	2992	34
22   0.22525   0.10   17.15   1.1   0.3315   1.1   1.00   3017   1.0   2535   13.3   2030   32	22	0.22929	0.10	17.43	1.4	0.5513	1.4	1.00	3047	1.6	2959	13.5	2830	32

Note that the errors are  $1\sigma$  errors. The majority of shots were taken as single shots on zircon grains.

that there was no Pb loss in the zircons (no discordant zircons), in contrast to three out of four TIMS analyses (Fig. 5a). It is most probable, that weathered or otherwise isotopically disturbed surfaces of the zircons are responsible for the discordant U-Pb TIMS data, since the zircons were not abraded before digestion to remove possible alterations or disturbances. The LA-ICP-MS method avoids this by polishing of the zircon grains before analysis, and by a *laser* pre-ablation which cleans the uppermost part of the mineral surface.

The LA-ICP-MS analyses of the natural sample EC69A show a complex history of zircon growth and lead loss. Three concordant zircon analyses together

dant zircon analyses which, although being discordant, indicate a complex history of crystallization and partial resetting. In that particular case, the internal structure of the zircons would have to be imaged by cathodoluminescence or back-scattered electron techniques prior to analysis, for ensuring an unequivocal interpretation of the various age populations. The analyses presented here show, nevertheless, that it is possible to detect an even complex geological history from a set of only 10–15 zircon grains, by high spatial resolution LA-ICP-MS analysis.

The LA-MC-ICP-MS method presented here is designed for rapid analysis of large sample sets, which



TABLE IV LA-ICP-MS data of sample EC69A.

	EA-ICI - MS data of sample ECOA.												
	<sup>207</sup> Pb*/	$2\sigma$	<sup>207</sup> Pb*/	$2\sigma$	206 <sub>Pb*/</sub>	$2\sigma$		<sup>207</sup> Pb/	$2\sigma$	<sup>207</sup> Pb*/	$2\sigma$	<sup>206</sup> Pb*/	
Analysis	206 <sub>Pb*</sub>	error	235 <sub>U</sub>	error	238 <sub>U</sub>	error	ρ	<sup>206</sup> Pb	error	<sup>235</sup> U	error	<sup>238</sup> U	
		(%)		(%)		(%)		age	(Ma)	age	(Ma)	age	
1	0.18772	0.4	18.40	6.2	0.55912	6.2	0.99	2722	7.2	3011	57.9	2863	
2a	0.12520	1.7	15.34	12.8	0.43386	12.8	0.99	2032	29.4	2836	115	2323	
2b	0.13026	2.3	15.21	7.3	0.44414	7.3	0.96	2101	40.1	2828	67.6	2369	
3a	0.14210	2.6	16.13	4.2	0.47461	4.2	0.82	2253	44.5	2885	39.0	2504	
3b	0.11516	13.4	10.85	15.2	0.37785	15.2	0.98	1882	224	2510	133	2066	
3c	0.15040	1.5	17.38	4.8	0.49850	4.8	0.99	2351	24.9	2956	44.9	2607	
4a	0.17586	0.8	17.33	4.5	0.53625	4.5	0.99	2614	12.6	2953	42.0	2768	
4b	0.17187	1.6	16.36	10.7	0.52396	10.7	0.98	2576	26.4	2898	97.7	2716	
5	0.14147	6.7	14.30	15.0	0.46184	15.0	0.98	2245	111	2770	133	2448	
6	0.13705	6.1	17.42	5.8	0.47611	5.8	0.43	2190	102	2958	53.8	2510	
7a	0.10342	7.7	15.16	5.8	0.37870	5.8	0.93	1686	136	2825	53.6	2070	
7b	0.12225	0.9	16.12	3.6	0.43484	3.6	0.98	1989	16.4	2884	34.1	2328	
7c	0.12528	4.6	15.74	6.5	0.43896	6.5	0.92	2033	79.9	2861	60.3	2346	
8a	0.16852	3.5	18.26	5.1	0.53185	5.1	0.80	2543	57.0	3003	47.8	2749	
8b	0.14777	1.2	17.80	1.5	0.49492	1.5	0.92	2320	20.7	2979	14.2	2592	
8c	0.09571	2.3	13.34	14.1	0.33741	14.1	0.99	1542	42.7	2704	125	1874	
9a	0.09655	7.2	17.69	9.3	0.36624	9.3	0.93	1559	129	2973	85.7	2012	
9b	0.07537	13.3	16.89	14.7	0.28108	14.7	0.41	1078	246	2929	132	1597	
9c	0.08637	4.9	16.78	4.0	0.32480	4.0	0.25	1346	91.0	2922	38.0	1813	
9d	0.08336	8.0	16.41	7.6	0.31092	7.6	0.11	1278	148	2901	70.4	1745	
10a	0.23273	1.0	19.28	2.5	0.60829	2.5	0.98	3071	15.8	3056	23.4	3063	
10b	0.23732	0.9	19.18	2.1	0.61117	2.1	0.96	3102	14.4	3051	20.3	3075	
10c	0.21793	1.7	18.07	3.4	0.58752	3.4	0.98	2965	26.9	2993	32.1	2979	
11a	0.13695	3.3	14.30	4.7	0.45064	4.7	0.95	2189	55.6	2770	43.3	2398	
11b	0.14320	1.6	16.17	8.6	0.47580	8.6	0.99	2266	27.5	2887	78.8	2509	
11c	0.18069	1.5	18.19	3.5	0.54860	3.5	0.96	2659	23.9	3000	33.0	2819	
12a	0.09062	3.6	15.42	4.1	0.33203	4.1	0.57	1439	67.9	2842	38.3	1848	
12b	0.12647	1.2	15.27	1.7	0.43256	1.7	0.76	2049	20.3	2832	15.8	2317	
12c	0.09022	9.4	13.17	8.0	0.31563	8.0	0.78	1430	170	2692	73.0	1768	
13a	0.12573	3.9	16.94	4.6	0.44200	4.6	0.61	2039	66.8	2931	42.7	2360	
13b	0.14744	3.8	17.27	5.1	0.48892	5.1	0.65	2316	63.4	2950	48.1	2566	
13c	0.13245	4.5	16.69	6.4	0.45527	6.4	0.78	2131	75.9	2917	59.4	2419	
14a	0.05842	0.8	0.7476	6.4	0.08864	6.4	0.99	545.7	16.9	566.8	27.6	547.5	
14b	0.05902	1.1	0.7526	2.9	0.09212	2.9	0.97	567.9	23.8	569.8	12.5	568.0	
14c	0.05882	0.8	0.7486	1.5	0.09090	1.5	0.93	560.3	17.8	567.4	6.6	560.9	

Note that the errors are  $2\sigma$  errors. The majority of shots were taken as multiple shots on zircon grains.

which may always be a source of sample contamination. for the <sup>207</sup>Pb/<sup>206</sup>Pb, <sup>206</sup>Pb/<sup>238</sup>U and <sup>207</sup>Pb/<sup>235</sup>U in the state of the st

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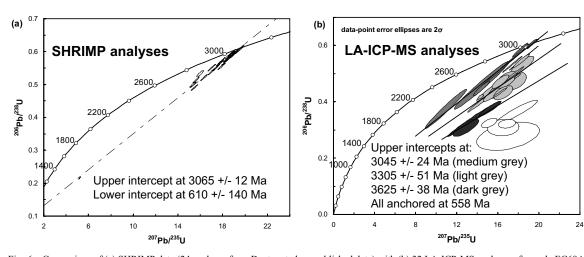


Fig. 6 – Comparison of (a) SHRIMP data (24 analyses from Dantas et al. unpublished data) with (b) 32 LA-ICP-MS analyses of sample EC69A. An upper intercept age of  $3045 \pm 24$  Ma, defined by three concordant and four discordant analyses, is within error of the SHRIMP age of  $3065 \pm 12$  Ma. The Discordia lines obtained by LA-ICP-MS are archored at 558 Ma. See Tables III and IV for full analyses.

#### ACKNOWLEDGMENTS

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#### RESUMO

A determinação de idades através do decaimento dos isótopos radioativos <sup>235</sup>U e <sup>238</sup>U para os isótopos radiogênicos <sup>207</sup>Pb e <sup>206</sup>Pb, respectivamente, utilizando o mineral zircão (ZrSiO<sub>4</sub>), é amplamente aplicada para decifrar processos geológicos. Um novo método tem sido desenvolvido nos últimos anos, a ablação a *laser* multi-coletor espectrometria de massas com plasma indutivamente acoplado (LA-MC-ICP-MS), superando o laborioso trabalho anteriormente necessário em outros métodos, na preparação de amostras, e permite obtenção de razões isotópicas com alta resolução espacial de micrômetros. O presente estudo descreve os procedimentos analíticos e os métodos usados na redução de dados que estão sendo aplicados no Laboratório de Geocropologia da Universidade de

exatidão de 0.6 a 3.8% ( $2\sigma$  desvio padrão) para as razões isotópicas de Pb e U dos padrões. Também foram obtidas idades pelo método LA-ICP-MS de duas amostras de zircões naturais, que já foram datadas anteriormente por outros métodos analíticos. A comparação dos resultados mostra uma boa conformidade das idades obtidas, dentro dos limites de erro. Os dados demonstram o grande potencial do método analítico para análises isotópicas rápidas, precisas e exatas de U-Pb, numa escala de micrômetros.

**Palavras-chave:** geocronologia, isótopos U-Pb, LA-MC-ICP-MS, zircão, datação.

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