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PREDICTION OF BENDING PROPERTIES FOR BEECH LUMBER USING STRESS WAVE METHOD

Ergun Guntekin^{1,*}, Serhat Ozkan¹, Tugba Yilmaz¹

ABSTRACT

In this study; bending properties of beech wood (*Fagus orientalis*) were predicted using stress – wave method and compared with static bending tests. First, lumbers which were different in length and cross section were weighed and dimensions were measured. Then, moisture contents were obtained via moisture meter. By using the density, moisture, and dimensions of the samples in MTG Timber Grader device, dynamic modulus of elasticity values were determined. And then, samples were subjected to 3 point bending test. Modulus of elasticity and bending strengths were calculated using load – deformation curves. Regression models were developed to interpret relationships between dynamic modulus elasticity and bending properties. Results showed that there is a high regression coefficient (0,86) between dynamic modulus of elasticity and static modulus of elasticity. Regression coefficient between dynamic modulus of elasticity and static bending strength was measured as (0,72) and regression coefficient between static modulus of elasticity and static bending strength was measured as (0,74). Results indicate that bending properties of beech wood lumber can be predicted using stress wave method.

Keywords: *Fagus orientalis*, bending properties, stress wave.

INTRODUCTION

Most strength properties and modulus of elasticity (MOE) of wood have a positive linear relationship, so that strength properties of wood may be estimated by MOE. MOE of wood can be determined by static or nondestructive evaluation (Yang *et al.* 2008).

Nondestructive evaluation (NDE) of wood has drawn attention, especially with regard to mechanical grading. A large number of investigations exists dealing with the determination of the MOE and its correlation with modulus of rupture in bending. Static and dynamic MOE determinations were compared by number of papers which good correlations have been reported between the two MOE values (Ross and Pellerin 1994, Divós and Tanaka 2005). Vibration, stress wave and ultrasonic wave velocity are particularly important in obtaining the MOE. Ultrasonic wave velocity has more advantages over other techniques in practical terms (Esteban *et al.* 2009). Stress-wave-based NDE methods have been investigated extensively during the past few decades and have shown promise for predicting the mechanical properties of wood based materials. Stress wave base methods have been applied and good correlations have been achieved in the case of detecting defects on standing trees (Wang *et al.* 2004), determining bending properties of small diameter logs (Wang *et al.* 2001), wood-derived products such as laminated veneer lumber (Ross *et al.* 1998), glued-laminated wood (Yang *et al.* 2008), reconstituted wood products (Han *et al.* 2005), diagnosing components of timber structures (Clausen *et al.* 2001).

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The beech (*Fagus orientalis*) is one of the most important commercial hardwood species in Turkish forestry, and covers a total of 1 335 786 ha, about 6.43% of Turkey's forests (Bektas *et al.* 2002). Its wood has been used in variety of applications including construction and furniture making. The purpose of this study was to predict bending properties of beech wood lumber using stress wave method.

MATERIALS AND METHODS

Total of 106 pieces of beech (*Fagus orientalis* Lipsky) lumbers which were approximately 50 x 70 mm in cross section and 2 meter in length were supplied from a commercial manufacturer. All the lumbers were Grade 1 according to TS EN 975-1 (2000). After the lumber had been delivered to the laboratory, they were conditioned at 65% relative humidity and 23 °C, moisture content (MC) was measured using dielectric type moisture meter, dimensions were measured and weighed. Apparent density was calculated. After the measurements, dynamic MOE values of the lumber were determined by employing Timber Grader MTG, which works on a principle of stress wave (Rozema 2007). Following dynamic measurement, static bending properties were measured using center point bending test in accordance with ASTM D 198 (ASTM 2002) as shown in figure 1. Samples depth to span (h/L) ratios varied between 0.0308 and 0.058. Apparent MOE and bending strength of the samples were evaluated from load-deformation curves obtained. The following equations were utilized to calculate MOE and bending strength:

$$\text{Bending Strength} = \frac{3PL}{2bh^2}$$

$$\text{MOE} = \frac{\Delta FL^3}{\Delta d 4bh^3}$$

Where:

P = maximum load (N),

L = span (mm),

h = specimen height (mm),

b = specimen width (mm),

ΔF = load at elastic region (N),

Δd = corresponding deformation at elastic region (mm).

Statistical analysis was performed in order to interpret relationship between dynamic MOE and bending properties.



Figure 1. Static testing of beech lumbers using center point bending test.

RESULTS AND DISCUSSION

Some physical and mechanical parameters of the lumbers measured are presented in table 1. The results indicated that the values of the dynamic MOE were significantly higher than static MOE in bending of the lumber because they include no shear. The relationship between static and dynamic MOE is shown in figure 2. The relationship between bending strength and dynamic MOE is shown in figure 3. The relationship between static MOE and bending strength is presented in figure 4.

Table 1. Average measured values of the lumbers tested.

| Property | Mean | Max. | Min. | Coefficient of Variation |
|------------------------------|-------|--------|-------|--------------------------|
| Moisture (%) | 9,05 | 14,8 | 5,8 | 11,27 |
| Density (kg/m ³) | 590 | 710 | 460 | 8,47 |
| Frequency (Hz) | 1270 | 1513 | 849 | 10,78 |
| Dynamic MOE (MPa) | 10764 | 15341 | 5763 | 20,48 |
| Static MOE (MPa) | 10110 | 14704 | 5554 | 19,03 |
| Bending Strength (MPa) | 90,54 | 127,14 | 47,64 | 18,32 |

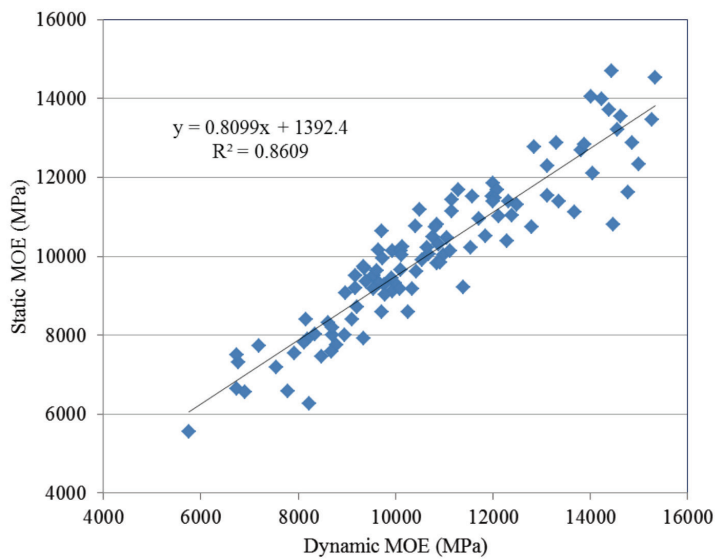


Figure 2. Relationship between static and dynamic MOE of beech lumbers.

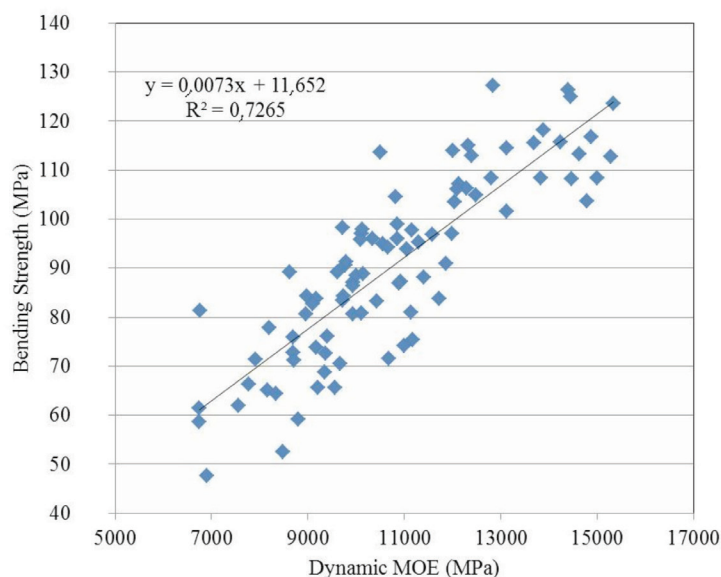


Figure 3. Relationship between bending strength and dynamic MOE of beech lumbers.

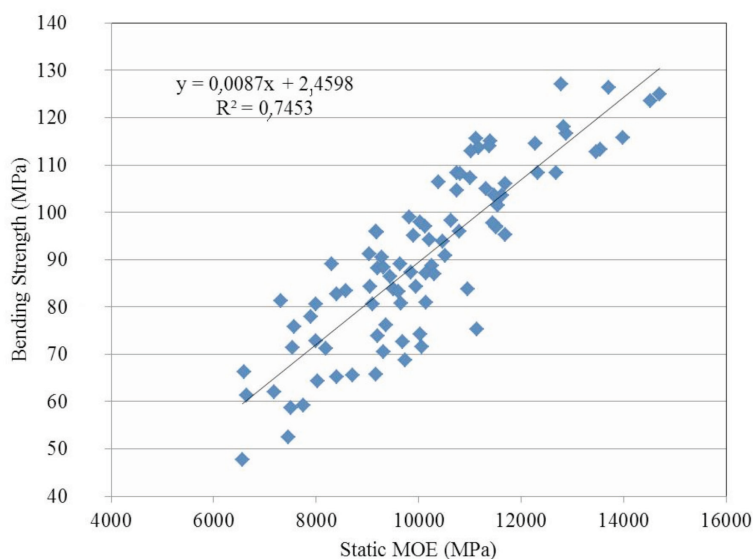


Figure 4. Relationship between bending strength and static MOE of beech lumbers.

Density values of the beech lumbers ranged from 460 to 719 kg/m³ with an average of 590. This value is on lower side of the average density values (589 – 669 kg/m³) for clear beech samples at 12 % MC reported by Bektas *et al.* (2002).

Bending strength of the clear beech wood samples at 12 % MC ranged between 87 and 123 MPa in the literature depending upon density, age and the location of growth (Guler and Bektas 2000). Bending strength of the beech wood used in the study is 90,54 MPa. Average MOE of the samples tested in this study is 10110 MPa, and it is close to the average MOE values (6600 to 16000 MPa) reported by Guler and Bektas (2000) for beech wood in the literature.

Several studies have reported that values of dynamic MOE are higher than those obtained using static bending tests (Teles *et al.* 2011, Passialis and Adamopoulos 2002, Barrett *et al.* 2008). The lower static MOE values were expected because static measurement includes shear deflection whereas MTG results are shear free MOE values (Barrett *et al.* 2008). In non-destructive evaluation of wood, r^2 values are usually depend on the methods, species used, moisture content, type of samples tested, and etc. Results of nondestructive testing on wood were summarized by Ross and Pellerin (1994). They have stated that r^2 values can be as high as 0,98 and 0,88 for clear wood species and dimension lumber, respectively. Divos and Tanaka (2005) reported that r^2 values between static and dynamic MOE values can be between 0,9 and 0,96, and dynamic MOE values are usually 10% higher than the static MOE values. Biechele *et al.* (2010) have reached r^2 values of 0,80 and 0,97 for spruce timber using stress wave and transverse vibration methods, respectively while Teles *et al.* (2011) have reported r^2 values of 0,84 and 0,94 for tropical hardwood species using same methods. Ravenshorst and Kuilen (2006) evaluated bending properties of thirty different hardwood species using both destructive and non-destructive testing. They have reached a coefficient of determination of 0,62 and 0,85 for bending strength and bending elasticity, respectively. Krzosek *et al.* (2008) tested Polish grown structural pine lumber employing several nondestructive methods including MTG. They have reported a coefficient of determination of 0,84 for bending stiffness. Similar coefficient of determination value has been reported by Guntekin *et al.* (2013) for bending stiffness of Turkish Red pine.

CONCLUSIONS

First grade beech lumbers were tested in order to evaluate bending properties using both nondestructive and destructive methods. Samples had an average density of 0,59 kg/m³ and an average MC of 9,05 %. The coefficient of determination between dynamic and static MOE is 0,8609. Coefficient of determination between dynamic MOE and static bending strength was measured as 0,7265 and coefficient of determination between static MOE and static bending strength was measured as 0,7453. Coefficient of determination between dynamic MOE and bending strength is very close to coefficient of determination between static MOE and bending strength. It can be concluded that bending properties of beech wood can be estimated using stress wave method.

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