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Dyna, vol. 78, núm. 168, 2011, pp. 53-57
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Medellín, Colombia

Available in: http://www.redalyc.org/articulo.oa?id=49622401006
ELECTRICAL PROPERTIES OF Cr/CrN NANO-MULTILAYERS PRODUCED BY THE UNBALANCED MAGNETRON SPUTTERING TECHNIQUE

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Received for review November 24th, 2009; accepted December 2nd, 2010; final version December 23rd, 2010

ABSTRACT: Chromium nitride (CrN) films have been applied to several steels as protective coatings against wear and corrosion due to their excellent mechanical properties and corrosion resistance, and in the electronic field these films are commonly used due to their low electrical resistivity. However, it has been found that multilayers combining metal/ceramic films could enhance mechanical and electrical properties compared with their monolayer counterparts, due to the higher amount and interaction between interfaces. In this work, Cr/CrN nano-multilayers have been produced through the unbalanced magnetron sputtering technique with three different degrees of unbalance, in order to study the influence of this parameter on electrical properties. Cr/CrN multilayers with approximately 1 µm of total thickness and a bilayer period (Λ) of 200 nm, 100 nm, and 20 nm were produced at room temperature on H13 steel and silicon (100); and their microstructure and electrical properties as a function of the magnetic field were evaluated. The phase formation was characterized through x-ray diffraction, and results presented (111) and (200) preferred orientations for all the multilayers. Cross section images were obtained through scanning electron microscopy and a multilayer structure can be clearly seen.

KEYWORDS: Multilayers, unbalanced magnetron sputtering, UBM, Cr/CrN, resistivity

1. INTRODUCTION

Chromium/chromium nitride multilayer coatings have received attention in recent years due to their high level of hardness and corrosion resistance [1-5] which are higher than those of their monolayer counterparts, especially because the interfaces present in multilayers act as barriers to crack propagation and dislocation movement, and the re-nucleation presented in these

structures reduces pores resulting in better corrosion resistance [6-8]. Cr and CrN multilayer coatings could also find an application as materials for low-resistivity diffusion barriers because the presence of interfaces would block diffusion through grain boundaries [7] and the grain size reduction which is common for this kind of structures [9,10] would form long diffusion paths through grain boundaries.
Physical vapor deposition (PVD) techniques are commonly used to produce high quality coatings at the nanometer scale [11-14], especially the techniques based on sputter deposition. The unbalanced magnetron (UBM) sputtering technique has gained attention due to its superior performance compared to conventional balanced magnetron [15]. With UBM, the level of unbalance of the magnetron varies the magnetic field in such way that the field lines are not confined to the target region but are also directed towards the substrate resulting in a high ionic current on the substrate and a high flux of coating atoms [16]. The ionic bombarding produced on the substrate modifies adatoms mobility [17] during film growth and hence the film properties are also modified [18].

The level of unbalance of a magnetron can be estimated using a coefficient of geometrical unbalance \( K_G \), according to [19]:

\[
K_G = \frac{Z(B_{z=0})}{2R}
\]

Where \( R \) is the average radius of the erosion zone and \( Z \) \( (B_{z=0}) \) is the distance from the target surface to the point on the axis of the magnetron where the magnetic field changes its direction [19], that is, where \( B_z \) component takes a value of zero.

In this study, Cr/CrN nano-multilayers were produced using the UBM technique by varying the level of unbalance of the magnetron, and its influence on the in-plane resistivity was studied in order to evaluate this kind of structure for low-resistivity barrier diffusion applications.

2. EXPERIMENTAL SETUP

2.1. Multilayer deposition

The nano-multilayers of Cr/CrN were deposited by means of the UBM technique in a vacuum chamber that has an unbalanced magnetron GENCOA sputter VT 100 which allows for one to vary the magnetic field through the variation in the number of turns \( (N_V) \) of a millimeter screw which changes the distance between the magnets assembly and the target. An increment in \( N_V \) corresponds to enlarging the distance between the central magnet and the target and, consequently, modifying the magnetic field configuration. The average radius of the erosion zone \( (R) \) and \( Z(B_{z=0}) \) shown in equation (1) were measured by using a portable teslameter Phywe with a Hall effect probe, and \( K_G \) was calculated according to these data as a function of \( N_V \). The coefficient of geometrical unbalance varied inversely with the level of unbalance of the magnetron: a high \( K_G \) value implied a low level of unbalance of the magnetron and vice versa. The multilayers were produced with three different \( K_G \) values (\( K_G = 1.32, 1.16, \) and \( 0.87 \)) as shown in Table 1.

The magnetron current-voltage characteristic was estimated to determine variations in efficiency with the unbalance coefficient. A sputtering system has a current-voltage \( (I-V) \) characteristic that behaves as \( I = c V^n \) (at constant pressure) [20]. Exponent \( n \) reflects how well the electrons are confined by the magnetic trap in the race track. An optimum magnetron should give an \( n \)-value which is typically around 5–9 [20]. Figure 1(a) shows the current-voltage characteristic for argon-nitrogen discharge using a Cr target and the \( n \)-values (Fig. 1[b]) as a function of \( K_G \) were determined according to the current-voltage values. Figure 1(b) illustrates that the efficiency of the magnetron increases for low \( K_G \) values, this means, a higher electron density is reached for \( K_G = 0.87 \) (and therefore a higher level of unbalance of the magnetron), while lower electron density is obtained for \( K_G = 1.32 \).
Commercial AISI H13 tool steel of 0.32-0.45 C, 0.8-1.20 Si, 0.20-0.50 Mn, 4.75-5.5 Cr, 0.8-1.20 V, 1.10-1.75 Mo, Fe balance (wt%) composition, and silicon (100) were used as substrates. Steel samples were polished using sandpaper from 100 to 1200, pretreated by quenching (1000-1025 ºC) and tempering (175-315 ºC) and finally, they were mirror polished. Before introducing the substrates in the deposition chamber, they were ultrasonically cleaned in acetone and alcohol in sequence and dried in flowing compressed air.

Multilayers were produced with a bilayer period of 200 nm, 100 nm, and 20 nm, and approximately 1 µm of total thickness. The base pressure was less than 9x10^-4 Pa. All the multilayers were grown at room temperature and the sample target distance was set to 5 cm while Ar and N\textsubscript{2} flow rates were set to 9 standard cubic centimeters per minute (sccm) and 3 sccm, respectively. The substrate was floating without any external bias. Deposition conditions are summarized in Table 1.

### 2.2. Multilayers Characterization

Identification of crystallographic phases and preferential orientations of the multilayers was done by x-ray diffraction (XRD) using an XPertPro Panalytical system under conditions of 6º grazing incident, 90º/s spinning velocity and monochromatized CuKa radiation. The cross-sectional morphology of the multilayers grown on Si (100) was studied using a FEIKUANTA 200 scanning electron microscope (SEM).

The four point probe (FPP) method was used to obtain in-plane resistivity of the multilayers. Sheet resistance values were taken and resistivity was calculated according to the expression [21,22]:

\[
\rho = R_s \cdot t
\]

Where \( \rho \) is the resistivity (\( \mu \text{W-cm} \)), \( R_s \) is the sheet resistance (ohms per square), and \( t \) is the multilayer thickness. The FPP was placed in contact with the film surface and the current was applied across the outer two probes while voltage drop was measured across the two inner probes. Four assumptions that are important for consistent good measurements were taken into account [23]: 1) the spacing between probe tips was the same between each probe tip, 2) the contact pressure on all four probe tips was uniform, 3) the edge of the sample was at least 10 times the spacing from the nearest probe tip, and 4) the thickness of the sample was less than 4 times the spacing between probe tips.

### Table 1. Deposition conditions: period (\( \Lambda \)), unbalance coefficient (\( K_G \)), working pressure (\( P_w \)), discharge power (\( P \)), discharge current (\( I \)), thickness (\( t \))

<table>
<thead>
<tr>
<th>Sample</th>
<th>( \Lambda ) (nm)</th>
<th>( K_G )</th>
<th>( P_w ) ( (\times 10^3 \text{ mbar}) )</th>
<th>( P/W )/I(mA)</th>
<th>( t ) (nm)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Cr/CrN-1</td>
<td>200</td>
<td>1.32</td>
<td>2.6/4.7</td>
<td>140/137</td>
<td>988</td>
</tr>
<tr>
<td>Cr/CrN-2</td>
<td>100</td>
<td>1.32</td>
<td>2.4/4.8</td>
<td>140/137</td>
<td>949</td>
</tr>
<tr>
<td>Cr/CrN-3</td>
<td>20</td>
<td>1.32</td>
<td>2.3/5.1</td>
<td>141/137</td>
<td>975</td>
</tr>
<tr>
<td>Cr/CrN-4</td>
<td>200</td>
<td>1.16</td>
<td>2.4/4.8</td>
<td>150/147</td>
<td>998</td>
</tr>
<tr>
<td>Cr/CrN-5</td>
<td>100</td>
<td>1.16</td>
<td>2.4/4.8</td>
<td>151/148</td>
<td>995</td>
</tr>
<tr>
<td>Cr/CrN-6</td>
<td>20</td>
<td>1.16</td>
<td>2.3/4.9</td>
<td>152/147</td>
<td>1018</td>
</tr>
<tr>
<td>Cr/CrN-7</td>
<td>200</td>
<td>0.87</td>
<td>2.4/4.4</td>
<td>187/182</td>
<td>970</td>
</tr>
<tr>
<td>Cr/CrN-8</td>
<td>100</td>
<td>0.87</td>
<td>2.4/4.6</td>
<td>183/179</td>
<td>992</td>
</tr>
<tr>
<td>Cr/CrN-9</td>
<td>20</td>
<td>0.87</td>
<td>2.3/4.9</td>
<td>183/179</td>
<td>1110</td>
</tr>
</tbody>
</table>

### 3. RESULTS AND DISCUSSION

#### Structural characterization

Results for high angle XRD are shown in Fig. 2 for multilayers grown with \( \Lambda = 200 \) nm. The SEM results show a clearly defined layered structure for multilayers with \( \Lambda = 200 \) nm (Fig. 3[a]) and \( \Lambda = 100 \) nm (Fig. 3[b]). For multilayers with \( \Lambda = 20 \) nm (not shown), it was not possible to obtain a clear image due to the resolution of...
the microscope used. The in-plane resistivity results are shown in Fig. 4. As can be seen, lower resistivity values were found for multilayers grown with $K_G = 0.87$. This could be due to the higher plasma efficiency reached in this configuration, where electrons are confined to the target region and they are lost in fewer amounts to the chamber walls producing dense plasma on the substrate region.

In turn, the ionization efficiency in plasma results in considerably higher ion currents at the substrate, and therefore, the ion flux increases as the degree of unbalance increases [24]. The ion bombardment induces adatom mobility producing microstructural changes and therefore denser coatings with fewer defects. These microstructural changes have been studied for different coatings such as Al, Zr, W [25], and TiN [26], among others.

Resistivity in a thin film arises due to electron scattering by phonons, point defects, impurities, grain boundaries, and film surfaces and interfaces [27]. As denser films (fewer defects inside grains) are produced for $K_G = 0.87$, lower resistivity values are obtained. As in the in-plane measurement the applied current passes through the lower resistivity layers (i.e. Cr layers), there is no noteworthy influence of the interfaces on the resistivity (Cr has a bulk resistivity of 13 $\mu\Omega\text{-cm}$ while CrN has a bulk resistivity of 640 $\mu\Omega\text{-cm}$ [28]).

The resistivity reached a value of approximately 225 $\mu$W-cm for all the multilayers grown with $K_G = 1.16$, and higher resistivity values were found for the multilayer grown with $K_G = 1.32$ and $\Lambda = 20$ nm, where lower plasma efficiency is presented.

4. CONCLUSIONS

In this work, Cr/CrN nano-multilayers were produced through the unbalanced magnetron sputtering
technique with three different levels of unbalance, and the influence of this parameter on electrical properties was evaluated. Results show that a higher degree of unbalance of the magnetron produces lower resistivity for all the multilayer periods, which could indicate that denser films are produced due to the increase in mobility as a result of the higher plasma efficiency reached in this configuration.

ACKNOWLEDGMENTS

This research has been financially supported by the Instituto Colombiano para el desarrollo de la Ciencia y la Tecnología Francisco José de Caldas–COLCIENCIAS, through project 1101-479-22003 CT 531-2008, the Fundación Para la Promoción de la Ciencia y la Tecnología, through a project under contract 200814 and the Dirección de Investigación de la Universidad Nacional de Colombia sede Bogotá, through project 11109.

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