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# The corrosion resistance and microstructure of UBM system-deposited $\text{Nb}_x\text{Si}_y\text{N}_z$ thin films

## Resistencia a la corrosión y microestructura de recubrimientos de $\text{Nb}_x\text{Si}_y\text{N}_z$ depositadas con el sistema UBM

L. Velasco<sup>1</sup>, J. J. Olaya<sup>2</sup>, R. Rodríguez-Baracaldo<sup>3</sup>

### ABSTRACT

$\text{Nb}_x\text{Si}_y\text{N}_z$  thin film nanostructure was grown using the unbalanced magnetron sputtering (UBM) technique with varying Si content. Corrosion resistance was evaluated by potentiodynamic polarisation technique in a 3% NaCl solution. Microstructure was analysed by X-ray diffraction (XRD), scanning electron microscopy (SEM) and laser scanning microscopy. Chemical composition was ascertained by X-ray fluorescence (XRF) technique. The results showed that deposition rates increased with higher Si content. A microstructural change was observed for greater than 5% Si content through the transition from a crystalline to an amorphous structure in the thin films. Corrosion test results demonstrated that the thin films having the highest silicon content had better corrosion resistance.

**Keywords:** Corrosion, diffraction, spectroscopy, fluorescence, microstructure, microscopy, race track, x ray, thin film, sputtering, polarisation.

### RESUMEN

En este trabajo se produjeron recubrimientos nanoestructurados de  $\text{Nb}_x\text{Si}_y\text{N}_z$  sobre acero inoxidable AISI 304 mediante la técnica del UBM (unbalanced magnetron - sputtering con magnetron desbalanceado), variando el contenido de Si, y se evaluó su resistencia frente al fenómeno corrosivo por medio de la técnica de polarización potenciodinámica en una solución al 3% de NaCl. La microestructura de los recubrimientos se analizó por medio de XRD (X ray diffraction - difracción de rayos X), SEM (scanning electron microscopy - microscopía electrónica de barrido) y microscopía láser confocal. La composición química se identificó con la técnica XRF (X ray fluorescence - fluorescencia de rayos X). Como resultado las tasas de depósito se incrementaron con la adición de Si, además se observó un cambio en la microestructura para contenidos superiores a 5% de Si, mediante la transición de un recubrimiento cristalino a amorfo. Finalmente, los resultados de corrosión sugieren que los recubrimientos con un alto contenido de silicio tienen un mejor comportamiento frente a la corrosión del sistema.

**Palabras clave:** Corrosión, Difracción, Espectroscopia, Fluorescencia, Microestructura, Microscopia, race track, Rayos X, Recubrimientos, Sputtering, Polarización.

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### Introduction

Several techniques for depositing thin films have been used in recent years; one such is physical vapour deposition (PVD) which efficiently improves materials' mechanical, electrical, optical, and chemical properties (Bhushan *et al.*, 2001; Yang *et al.*, 2008; Kumar and Kaur, 2009; Li *et al.*, 2009; Vyas *et al.*, 2010). Several PVD studies have focused on producing ternary thin films supported on transition metal, silicon and nitrogen (Me-Si-N), improving thin film performance and the development of new materials, as mentioned in Ti-Si-N (Ding *et al.*, 2004; Ribeiro *et al.*, 2004), V-Si-N (Veprek, 1997), W-Si-N (Fu, Shen *et al.*, 2005; Fu, Zhou *et al.*, 2005) and Nb-Si-N production (Murakami, Sasaki *et al.*, 2001; Dong *et al.*, 2006; Sandu *et al.*, 2006; Song *et al.*, 2007; Wang *et al.*, 2007).

The unbalanced magnetron (UBM) sputtering technique stands out among PVD processes; it leads to obtaining dense structures at low temperatures and improves adherence, which can increase the performance of a coating/substrate system when it is affected by high rates of wear, fatigue and corrosion (Kelly and Arnell, 2000; Safi, 2000; Karthikeyan *et al.*, 2010).

Some studies of NbN thin films produced through the UBM technique have shown good performance in improving steel corrosion resistance (Fenker *et al.*, 2003; Rodil *et al.*, 2007; Olaya *et al.*, 2008; Ramirez *et al.*, 2011). Other studies have focused on the fabrication of Nb-Si-N thin films through PVD techniques and have evaluated their mechanical and electrical properties (Murakami *et al.*, 2001; Dong *et al.*, 2006; Sandu *et al.*, 2006; Song *et al.*, 2007; Wang *et al.*, 2007). However, no studies have been found regarding Nb-Si-N thin film corrosion behaviour. Considering

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this background, the present investigation was aimed at producing  $\text{Nb}_x\text{Si}_y\text{N}_z$  thin films, varying silicon content. Corrosion resistance was studied regarding microstructure and chemical composition.

### Experimental procedure

$\text{Nb}_x\text{Si}_y\text{N}_z$  thin films were deposited using UBM sputtering. Argon and nitrogen gas flow set at 9 standard cubic centimeters per minute (sccm) and 3 sccm, respectively, were used to generate plasma at  $6 \times 10^{-1}$  Pa working pressure and 300 mA constant current. A co-sputtering system was for producing the thin films, using Si sheets on a 10 cm diameter niobium target, with 35 rpm substrate holder rotation. Si content in the coating was varied by adding a number of sheets (6x6x2mm) to the area of greatest target erosion, called the race track (as shown in Figure 1).

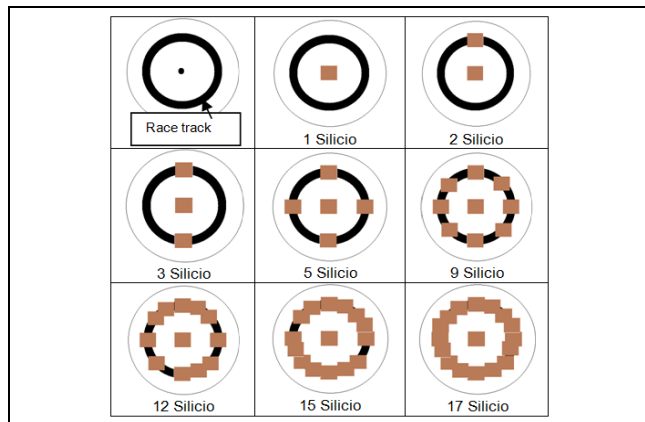


Figure 1. Si sheets on the niobium target race track

The substrates were prepared to a mirror finish and cleaned with isopropanol and acetone solutions in ultrasound. The target was cleaned before deposition by 5 minutes' sputtering; an  $\text{Nb}_x\text{Si}_y$  film was deposited to improve thin film adhesion. Deposition rates were studied by Dektak 150 profilometer using 200 micron displacement and 1 mg force in scanning mode (peak assignment) and 6 Å accuracy. The structural study involved X-ray diffraction (XRD) using an X-PertPro analytical system for grazing incidence and Bragg-Brentano configurations and monochromatised  $\text{CuK}\alpha$  radiation ( $1.540998 \text{ Å}$ ) working at 45 kV and 40 mA. Morphology was determined with a scanning electron microscope (FEI QUANTA 200 SEM) using high vacuum and 30 KV voltage. The surface was observed by confocal laser scanning microscope (LSM 600).

Chemical composition was evaluated using a fluorescence X-ray spectrometer (Philips PW MagixPro – 2440) with a rhodium tube, at 4KW maximum power. Corrosion resistance was evaluated by potentiodynamic polarisation tests using Gamry 600 equipment, following ASTM G5 recommendations (2004). A 3% NaCl solution was used as electrolyte, -0.3 V initial potential, 0.4 V final potential, 0.5 mV/s scan rate and  $0.196 \text{ cm}^2$  exposed area. A 45 minute solution settling time after sample immersion was allowed for all tests. The corrosion current was evaluated by Tafel extrapolation and porosity rate was determined using equation 1 (Ahn *et al.*, 2004)

$$P = \frac{R_{ps}}{R_{pc}} * 10^{-1} \left| \frac{\Delta E_{corr}}{\beta_a} \right| \quad (1)$$

where  $R_{ps}$  was AISI 304 uncoated stainless steel substrate polarisation resistance,  $R_{pc}$  coating polarisation resistance,  $\Delta E_{corr}$  the

difference between coating and substrate corrosion potential and  $\beta_a$  the anodic Tafel slope obtained by Tafel extrapolation technique.

### Results and Discussion

Deposition rates were evaluated for obtaining  $\sim 1.1 \mu\text{m}$  thickness thin films. Figure 2 shows the deposition rate results for  $\text{Nb}_x\text{Si}_y\text{N}_z$  thin films, depending on the number of Si layers. A gradual increase in deposition rate was observed when Si was added; this phenomenon has been studied by others (Depla *et al.*, 2006; Eufinger *et al.*, 2006; Depla *et al.*, 2009). This could have been related to increased target polarisation due to secondary electrons emitted by silicon sheets. Such electrons are located on target surface and thus do not interact with the gas, thereby increasing the voltage and accelerating the ions bombarding the target surface.

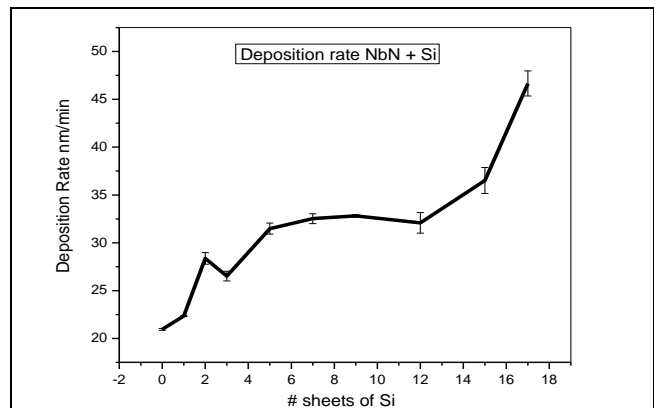


Figure 2.  $\text{Nb}_x\text{Si}_y\text{N}_z$  thin film deposition rates regarding Si layers

Figure 3 shows  $\delta\text{NbN}$  cubic phase XRD spectra with mixed orientation in directions (111) and (200), located at  $34.66^\circ$  and  $40.83^\circ$ . The figure shows a peak at  $37.02^\circ$  corresponding to Nb FCC phase, having (111) orientation. The NbN peaks may have been related to 01-071-0162 in the database and the Niobium peak to reference 01-088-2330. The other peaks corresponded to AISI-SAE 304 steel substrate; however, it should be pointed out that no peak related to silicon or silicon nitride was found, although it was co-deposited. Therefore, amorphous phase formation was likely and has been reported by others (Fu *et al.*, 2005; Dong *et al.*, 2006; Sandu *et al.*, 2006; Song *et al.*, 2007).

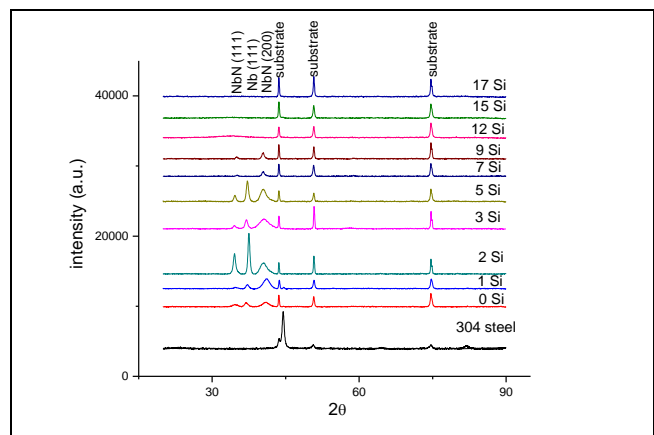


Figure 3.  $\text{Nb}_x\text{Si}_y\text{N}_z$  XRD profile

The thin films diagrams having higher silicon content showed that substrate and NbN crystalline phase peaks disappeared, i.e. the thin films exhibited an amorphous phase.

X-ray fluorescence chemical composition analysis showed Nb and Si in the thin film, and Fe, Cr and Ni in the substrate. Figure 4 shows that silicon content increased and niobium content decreased when the number of target sheets increased. This could have been related to a decrease in X-ray diffraction peak intensity. An increase in Si could have promoted the creation of a nanocomposite  $\text{Si}_3\text{N}_4$  reducing the amount of NbN in the thin film (Murakami *et al.*, 2001; Dong *et al.*, 2006; Sandu *et al.*, 2006; Song *et al.*, 2007; Wang *et al.*, 2007).

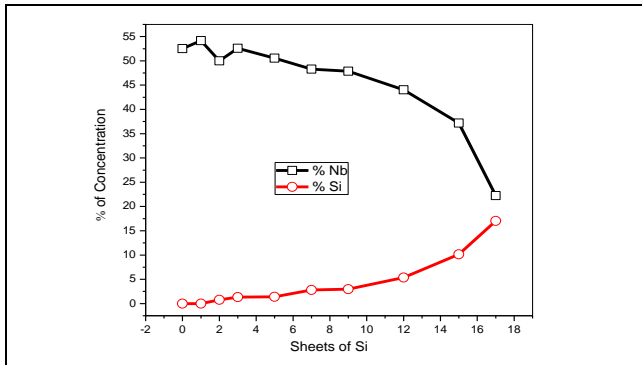


Figure 4. Nb and Si concentration in the thin films obtained

Figure 5 shows SEM images having a homogeneous, compact, low roughness surface copied to substrate topography, as analysed in other studies (Ahn *et al.*, 2002; Liu *et al.*, 2003; Liu *et al.*, 2003). The Figure shows small, isolated areas of delamination in thin films having higher Si content. This could have been attributed to increased residual stress because, as observed in XRD spectra, there was movement to the left of the NbN peak on the plane (111).

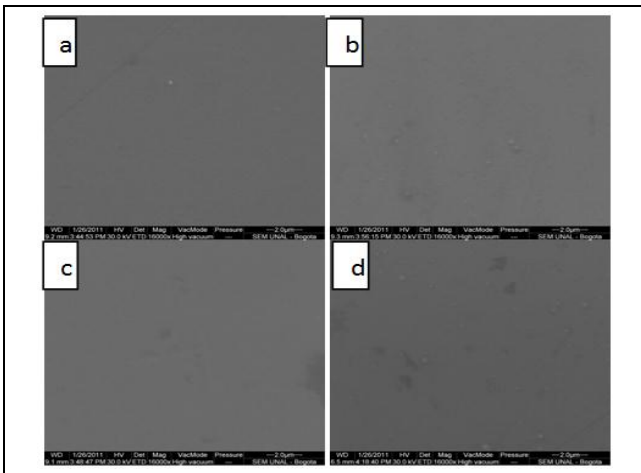


Figure 5. SEM micrographs of (a) 0% Si, (b) 0.7% Si, (c) 2.7 % Si, (d) 16.5% Si

Figure 6 gives a cross-section of the thin films obtained; it shows a structure having columnar growth fitting well to the "T" area in the Thornton model, as described by Ohring (2001) and Martin (2010); however, columnar grain morphology was not observed for higher Si concentrations.

Figure 7 (a-c) shows corrosion using the potentiodynamic polarisation technique. The thin films had better corrosion resistance than AISI-SAE 304 stainless steel. This could be checked by analysis showing that thin film corrosion potential was more positive and the polarisation curves showed leftward movement on the horizontal axis.

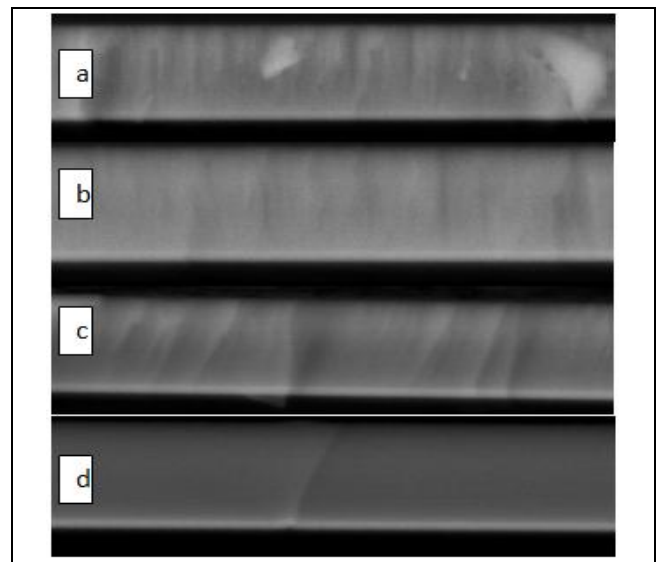


Figure 6. SEM micrograph cross-section of (a) 0% Si, (b) 0.7% Si, (c) 2.7% Si and (d) 10% Si

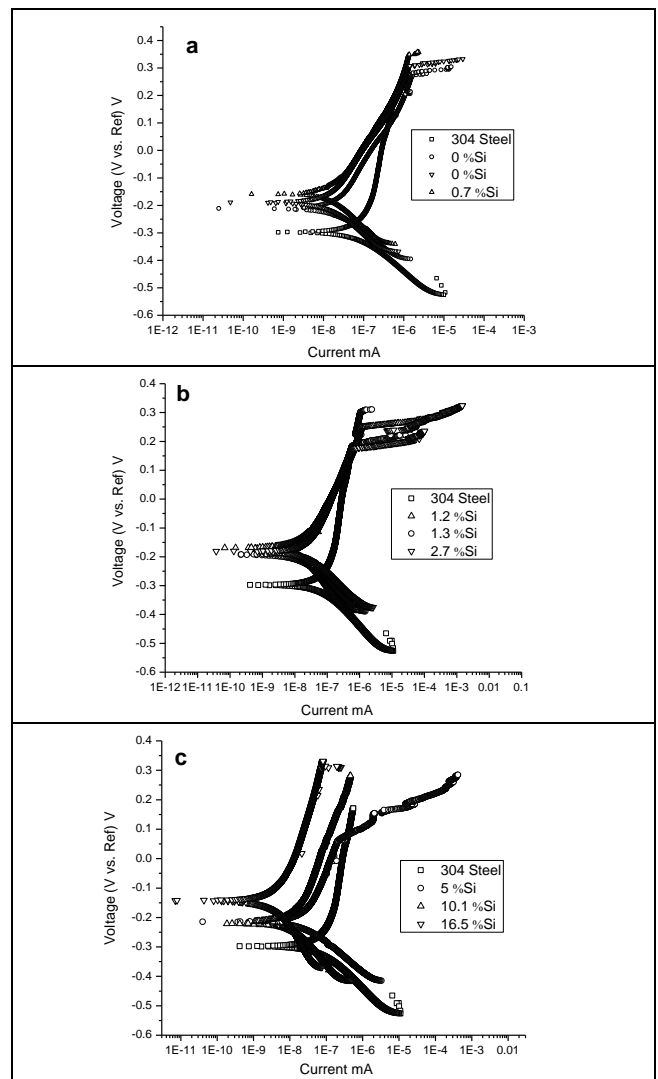


Figure 7. Potentiodynamic polarisation curves. (a), (b) and (c)  $\text{Nb}_x\text{Si}_y\text{N}_z$  thin films

Figure 8 gives corrosion current values calculated by the Tafel extrapolation method and porosity index. The Figure shows a decrease in the corrosion current in the thin films having low Si content; however, the corrosion current had a value similar to that for the substrate for medium Si content. The samples having the highest Si content had lower corrosion current values, indicating better protection against corrosion.

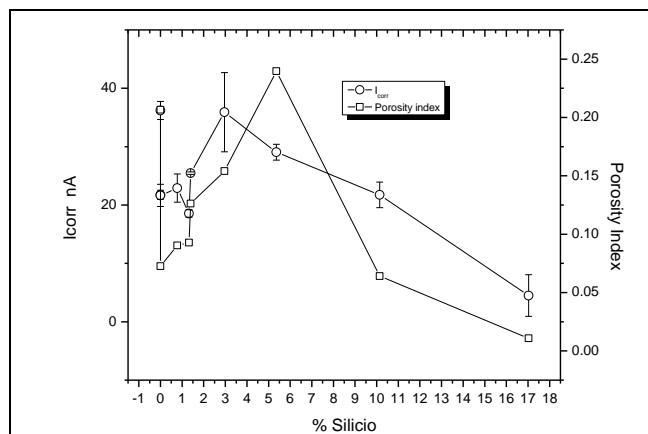


Figure 8. Corrosion current and porosity index regarding thin film Si content

The porosity index was lower in thin films having higher Si content and higher in thin films having medium Si content. These results fit well with the cross-section microstructure, i.e. columnar growth was inhibited in thin films having high Si content.

Thin film corrosion produced by PVD was due to corrosive solution diffusion in the substrate through the grain boundaries between columns and defects (such as pores). Coating degradation was increased by the galvanic coupling created between the substrate and the ceramic (Liu *et al.*, 2003; Galvele, 2005).

The final thin film surface did not show delamination or surface degradation; this can be seen in Figure 9, obtained with confocal laser microscopy, showing a low Si content coating. The Figure shows a smooth, compact surface free of corrosion products.

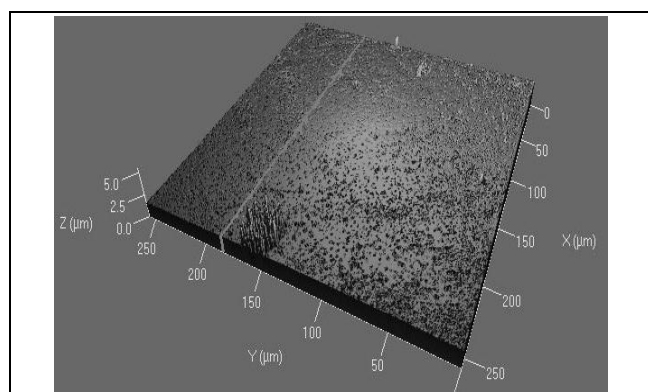


Figure 9.  $Nb_xSi_yN_z$  thin film surface with low Si content

## Conclusions

$Nb_xSi_yN_z$  thin films were successfully deposited and it was found that the deposition rate depended on the quantity of silicon in the niobium target.

Thin film microstructure was related to the quantity of Si deposited. They showed the NbN FCC phase at low quantity and an amorphous structure at high quantity.

The thin films' surface and cross-section had a compact, slightly rough structure. However, columns were only observed in samples having low Si content and they disappeared in samples having high Si content.

$Nb_xSi_yN_z$  thin films protected and improved stainless steel corrosion resistance. Surface morphology did not show significant degradation, suggesting that such thin films could be used as a corrosion barrier coating. It should be noted that samples having higher Si content had the best protection against corrosion.

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