



Ingeniería e Investigación

ISSN: 0120-5609

revii_bog@unal.edu.co

Universidad Nacional de Colombia
Colombia

Gallardo-Alvarado, J.; Pérez-González, L.
Kinematics of an actuating mechanism for a telescoping antenna
Ingeniería e Investigación, vol. 35, núm. 1, abril, 2015, pp. 5-11
Universidad Nacional de Colombia
Bogotá, Colombia

Available in: <http://www.redalyc.org/articulo.oa?id=64338498002>

- How to cite
- Complete issue
- More information about this article
- Journal's homepage in redalyc.org

redalyc.org

Scientific Information System
Network of Scientific Journals from Latin America, the Caribbean, Spain and Portugal
Non-profit academic project, developed under the open access initiative

Kinematics of an actuating mechanism for a telescoping antenna

Cinemática de un mecanismo actuador para una antena telescópica

J. Gallardo-Alvarado¹ and L. Pérez-González²

ABSTRACT

In this work the position, velocity and acceleration analyses of a four-degrees-of-freedom serial manipulator are approached mainly by means of the theory of screws. Closed-form solutions are easily obtained for the displacement analysis of the mechanism owing the decoupled action of the generalized coordinates, while the input-output equations of velocity and acceleration of the manipulator are systematically obtained by means of the theory of screws. A case study is included with the purpose to exemplify the application of the method.

Keywords: Serial manipulator, Kinematics, Screw Theory.

RESUMEN

En este trabajo los análisis de posición, velocidad y aceleración de un manipulador serial de cuatro grados de libertad se abordan principalmente por medio de la teoría de tornillos. El análisis de posición es resuelto en forma cerrada debido a la acción desacoplada de las coordenadas generalizadas mientras que las ecuaciones entrada salida de velocidad y aceleración del manipulador son obtenidas sistemáticamente por medio de la teoría de tornillos. Con el propósito de ejemplificar el método se proporciona un caso de estudio.

Palabras clave: Manipulador serial, Cinemática, Teoría de Tornillos.

Received: June 13th 2014

Accepted: October 16th 2014

Introduction

Screw theory is a trusted and confident mathematical resource to address the spatial kinematics of rigid body. In 1830 Chasles introduced the concept of twist motion of a rigid body which was deeply developed by Poincaré while the notion of screw coordinates was introduced by Plücker. Formally, the mathematical framework was developed by Ball (1900) with the purpose to approach the kinematics and statics of rigid body. Two decades later von Mises (1924a, 1924b) published his *Motor Calculus* where the general equations of motion of rigid body are established based on the so-called motor product. Applications of screw theory concerned mainly with the so-called first-order analysis of rigid body have been widely reported in the literature ranging from projective geometry, screw systems, statics, synthesis, theory of extension and so far. However, the acceleration analysis using exclusively screw theory was unlooked for many years due, perhaps, to the difficulty to express in screw form the accelerator introduced by Brand (1947) and applied by Sugimoto (1989, 1990) in the kinematics of robot manipulators. Thus it is not surprising that for a long time some kinematicians have assumed that screw theory cannot be employed to handle the higher-order kinematics of mechanisms. In fact, by the time it was believed that screw theory

will be confined to the first-order analysis of rigid body. It was almost two decades ago when Rico and Duffy (1996) published a remarkable contribution entitled "An application of screw algebra to the acceleration analysis of serial chains" that screw theory was recognized as a viable option to approach the higher-order kinematic analyses of open and closed chains. However, even though the rigorous mathematical procedures employed in such contribution, the material exposed was bitterly disappointed by some kinematicians who claim that screw theory would not be extended to the acceleration analysis.

In this work as a little proof of the potential of screw theory in the analysis of open chains, the infinitesimal kinematics of a four-degrees-of-freedom serial manipulator is investigated by resorting to screw theory. For the sake of completeness, the displacement analysis of the robot is also included. Numerical examples are included in order to show the application of the method.

Preliminary Screw Theory

As a consideration for readers unfamiliar with the theory of screws, this section is devoted to review some elementary concepts of it. In Plücker coordinates a screw, notated as $\$$, is a six-

¹ Jaime Gallardo-Alvarado. Doctor en Ciencias en Ingeniería Eléctrica, Instituto Tecnológico de la Laguna, México. Affiliation: Instituto Tecnológico de Celaya, México. E-mail: jaime.gallardo@itcelaya.edu.mx

² Luciano Pérez-González. Maestro en Ingeniería Mecánica, ITESM, Campus Monterrey, México. Affiliation: Instituto Tecnológico de Celaya, México.

E-mail: luciano.perez@itcelaya.edu.mx

How to cite: Gallardo-Alvarado, J., & Pérez-González, L. (2015). Kinematics of an actuating mechanism for a telescoping antenna. *Ingeniería e Investigación*, 35(1), 5-11. DOI: <http://dx.doi.org/10.15446/ing.investig.v35n1.44000>

dimensional vector given by $\$ = (s, s_O)$, where s is named the primal of the screw, $P(\$) = s$, and denotes the direction of the line. Usually the primal part is a unit vector of course along the instantaneous screw axis (ISA). While s_O is named the dual part of the screw, $D(\$) = s_O$, and involves the moment produced by vector s around the reference pole O . The vector s_O is calculated as follows

$$s_O = hs + s \times r \quad (1)$$

Therein h is the pitch of the screw while r is a vector directed from an arbitrary point of the ISA to the reference pole O . Conveniently, the reference pole is chosen as the origin of the reference frame in order to simplify the Plücker coordinates. In a revolute joint the pitch h vanishes yielding $\$ = (s, s \times r)$, while in a prismatic joint the pitch goes to infinity yielding $\$ = (0, s)$. Furthermore, any lower kinematic pair may be modeled combining revolute and/or prismatic joints, e.g. a spherical joint may be modeled as three concurrent revolute joints while a cylindrical joint is modeled as the combination of one prismatic joint with one revolute joint.

The Lie algebra $se(3)$ of the Euclidean group $SE(3)$ is the set of elements of the form $\$ = (s, s_O)$. Let $\$1 = (s_1, s_{O1})$, $\$2 = (s_2, s_{O2})$ and $\$3 = (s_3, s_{O3})$ be three elements of the Lie algebra $se(3)$. Furthermore, consider that $\mu_1, \mu_2, \mu_3 \in \mathbb{R}$. Concerned with the contribution, the Lie algebra supports the following operations

Addition, $\$1 + \$2 = (s_1 + s_2, s_{O1} + s_{O2})$

Multiplication by a scalar, $\mu\$ = (\mu s, \mu s_O)$

Lie product, $[\$1 \$2] = (s_1 \times s_2, s_1 \times s_{O2} - s_2 \times s_{O1})$

Furthermore, the Lie products has the following properties

Nilpotent, $[\$1 \$1] = 0$

Distributive, $[\$1 \mu_2 \$2 + \mu_3 \$3] = \mu_2 [\$1 \$2] + \mu_3 [\$1 \$3]$

$$[\mu_1 \$1 + \mu_2 \$2 \$3] = \mu_1 [\$1 \$3] + \mu_2 [\$2 \$3]$$

Jacobi identity, $[\$1 [\$2 \$3]] + [\$3 [\$1 \$2]] + [\$2 [\$3 \$1]] = 0$

The representation of the kinematic states of a rigid body, as observed from another body or reference frame, has been a topic that has attracted the attention of kinematicians since many years ago. In fact, it dates back to the pioneering contribution of Ball (1900). The velocity state, or twist about a screw, of rigid body was defined by Ball (1900) as a six-dimensional vector given by

$$V_O = \begin{bmatrix} \omega \\ v_O \end{bmatrix} \quad (2)$$

where ω is the angular velocity vector of the body while v_O is the linear velocity vector of a point O embedded to it. Almost four decades after the contribution of Ball, a representation of the acceleration state of rigid body was proposed by Brand (1947) as follows

$$A_O = \begin{bmatrix} \alpha \\ a_O - \omega \times v_O \end{bmatrix} \quad (3)$$

where α denotes the angular acceleration of the vector while a_O denotes the linear acceleration vector of point O .

It is interesting to note that the primal part of the acceleration state is obtained directly as the time derivative of the primal part of the velocity state, i.e.

$$P(A_O) = \frac{d(P(V_O))}{dt} = \frac{d(\omega)}{dt} = \alpha \quad (4)$$

Thus, at this moment a natural question arises, why don't occur the same for the dual part of the acceleration state? The answer to this query can be found in the heart of the theory of helicoidal vector fields, for details the reader is referred to Gallardo-Alvarado et al (2008).

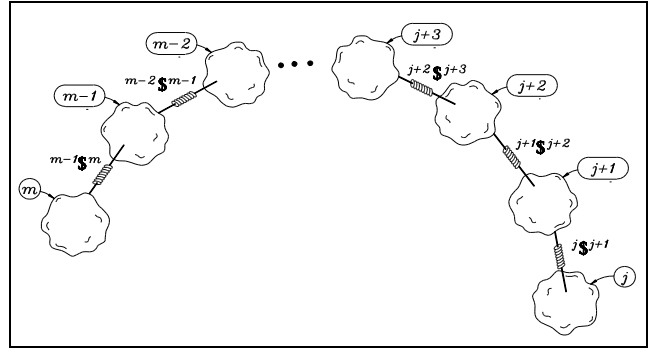


Figure 1. Open serial kinematic chain.

Consider an open kinematic chain as shown in Fig. 1, where adjacent bodies are connected by means of infinitesimal screws also known as helical pairs. The velocity state of the end-effector m as measured from the base link j may be expressed in screw form, see for instance Sugimoto and Duffy (1982), as a linear combination of the involved screws as follows

$${}^j V^m = \sum_{i=j}^{m-1} {}_i \omega_{i+1} {}^i \$^{i+1} \quad (5)$$

where ${}_i \omega_{i+1}$ denotes the i^{th} joint-rate velocity between adjacent bodies i and $i+1$. By the time, the usefulness of Eq. (5) in robot kinematics was immediately recognized by engineers and scientists; however its extension to the acceleration analysis remained as an open problem for more than one decade. Certainly, the difficulty to express in screw form the acceleration state of kinematic chains was considered as one of the main drawbacks of the theory of screws. It was in 1996 when Rico and Duffy (1996) introduced the following equation

$${}^j A^m = \sum_{i=j}^{m-1} {}_i \dot{\omega}_{i+1} {}^i \$^{i+1} + L \quad (6)$$

where ${}_i \dot{\omega}_{i+1}$ denotes the i^{th} joint-rate acceleration between adjacent bodies, i.e. ${}_i \dot{\omega}_{i+1} = d(\frac{{}_i \omega_{i+1}}{dt})$, while L was named the Lie screw of acceleration and it is calculated according to the joint-rate velocities of the serial chain as follows

$$L = [{}_j \omega_{j+1} {}^j \$^{j+1} \quad {}_{j+1} \omega_{j+2} {}^{j+1} \$^{j+2} + \dots + {}_{m-1} \omega_m {}^{m-1} \$^m] + [{}_{j+1} \omega_{j+2} {}^{j+1} \$^{j+2} \quad {}_{j+2} \omega_{j+3} {}^{j+2} \$^{j+3} + \dots + {}_{m-1} \omega_m {}^{m-1} \$^m] + \dots + [{}_{m-2} \omega_{m-1} {}^{m-2} \$^{m-1} \quad {}_{m-1} \omega_m {}^{m-1} \$^m] \quad (7)$$

For clarity, unlike the equation of velocity state in screw-form, in the contribution the six-dimensional vector L is written explicitly. Equation (6) was named by Rico and Duffy (1996) as the reduced

acceleration state. After the publication of that theoretical paper, screw theory was recognized, unfortunately only by a reduced number of kinematicians, as a viable option to approach not only the acceleration analysis but also the jerk analysis (Rico et al, 1999) and the hyper-jerk analysis of robot manipulators (Gallardo-Alvarado, 2014). Equation (7) has been proved successfully in a wide variety of parallel manipulators. The relevant results of such analyses were reported in several indexed journals by the author of this contribution, see for instance Gallardo-Alvarado et al (2011), Gallardo-Alvarado (2012), Gallardo-Alvarado and García-Murillo (2013). In this occasion in order to show the viability of the theory of screws in the kinematic analysis of robot manipulators, a four-degrees-of-freedom open kinematic chain is chosen as the robot under study.

Description of the Mechanism

The topology of the robot manipulator under study, and its geometric scheme, is outlined in Fig. 2.

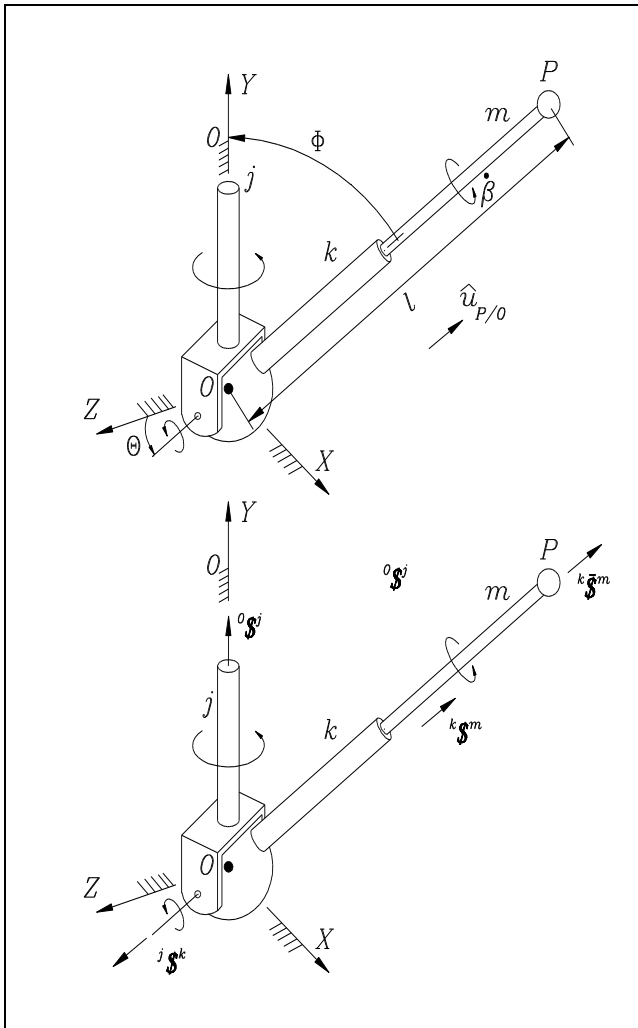


Figure 2. Telescoping antenna and its geometric scheme.

The spatial mechanism is composed of an extendible limb l formed with two bodies labeled k and m connected by means of a cylindrical joint where the translation of body m with respect to body k is represented by means of the screw ${}^k\$_m$ while the rotation between the same bodies is represented by means of the screw ${}^k\$_m$. Furthermore, the orientation of the limb is controlled

through the angles \varnothing and θ . On the other hand, in order to improve the performance of the original telescoping antenna, an additional freedom was added to the mechanism through the rotational angle β between bodies m and k . In other words the prismatic joint of the original mechanism was replaced with a cylindrical joint. The generalized coordinate β is added to the manipulator with the purpose to increase the mobility of a possibly body attached to body m , e.g. a gripper.

Displacement Analysis

Let XYZ be a reference frame with associated unit vectors $\hat{i}\hat{j}\hat{k}$. Furthermore, let $P = (Px, Py, Pz)$ be the control point of the manipulator.

The inverse displacement analysis is formulated as follows. Given the coordinates of point P it is required to determine the orientating angles θ and \varnothing , and the length l of the antenna. The length l is directly computed as

$$l = \sqrt{Px^2 + Py^2 + Pz^2} \quad (8)$$

After, the angle \varnothing is obtained in the range $(0, \pi)$ as

$$\varnothing = \arccos(Py/l) \quad (9)$$

In order to find the angle θ consider that the revolute joint connecting bodies j and k constraints the position of point P in such a way that

$$\hat{w} \cdot \hat{u}_{P/O} = 0 \quad (10)$$

Where $\hat{w} = \sin(\theta)\hat{i} + \cos(\theta)\hat{k}$ and $\hat{u}_{P/O}$ is a unit vector pointed from O to P while the dot (\cdot) denotes the dot product of usual three-dimensional vectorial algebra. Thus it follows that the angle θ must satisfy the relationship $\tan(-\theta) = Pz/Px$. Hence in terms of the standard arctan function, whose range is $(-\frac{\pi}{2}, \frac{\pi}{2})$, the angle θ is obtained as

$$\begin{aligned} \theta = & \\ & -\arctan\left(\frac{Pz}{Px}\right) \quad Px > 0; \\ & -\arctan\left(\frac{Pz}{Px}\right) - \pi \quad Pz \geq 0, Px < 0; \\ & -\arctan\left(\frac{Pz}{Px}\right) + \pi \quad Pz < 0, Px < 0; \\ & -\frac{\pi}{2} \quad Pz > 0, Px = 0; \\ & \frac{\pi}{2} \quad Pz < 0, Px = 0; \\ & \text{undefined} \quad Px = Pz = 0 \end{aligned} \quad (11)$$

On the other hand, the forward displacement analysis consists of finding the coordinates of point P given the generalized coordinates \varnothing , θ and l . This analysis is straightforward. Indeed

$$\begin{aligned} Px &= l \sin(\varnothing) \cos(\theta), \quad Py = l \cos(\varnothing), \\ Pz &= -l \sin(\varnothing) \sin(\theta) \end{aligned} \quad (12)$$

According to Eq. (12) it is possible to conclude that there are coupled motions of the generalized coordinates l , \varnothing and θ in order to obtain a specific position for point P .

Velocity Analysis of the Serial Manipulator

Let ${}^0\omega^m$ be the angular velocity vector of the end-effector m as measured from the base link 0 and let v_O be the velocity of a point of the body m which is instantaneously coincident with the origin of the reference frame XYZ . According to Eq. (5) the velocity state of body m as measured from body 0, the vector ${}^0V_O^m$, is given in screw form as follows

$$\dot{\theta} {}^0\$^j + \dot{\phi} {}^j\$^k + \dot{\beta} {}^k\$^m + \dot{l} {}^k\bar{\$}^m = {}^0V_O^m \quad (13)$$

Where, taking into account that point O is chosen as the reference pole, in Plücker coordinates the infinitesimal screws of the robot are computed as

$${}^0\$^j = \begin{bmatrix} 0 \\ 1 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}, {}^j\$^k = \begin{bmatrix} \sin(\theta) \\ 0 \\ \cos(\theta) \\ 0 \\ 0 \\ 0 \end{bmatrix}, {}^k\$^m = \begin{bmatrix} \sin(\phi) \cos(\theta) \\ \cos(\phi) \\ -\sin(\phi) \sin(\theta) \\ 0 \\ 0 \\ 0 \end{bmatrix},$$

$${}^k\bar{\$}^m = \begin{bmatrix} 0 \\ 0 \\ 0 \\ \sin(\phi) \cos(\theta) \\ \cos(\phi) \\ -\sin(\phi) \sin(\theta) \end{bmatrix}$$

On the other hand, in order to satisfy the rank of the Jacobian matrix spanned by the infinitesimal screws two virtual, or imaginary, prismatic joints, along the X and Z axes passing through point O , are added to the serial manipulator. Hence Eq. (13) becomes into

$$\dot{\theta} {}^0\$^j + \dot{\phi} {}^j\$^k + \dot{\beta} {}^k\$^m + \dot{l} {}^k\bar{\$}^m + v_1 {}^1\$^1 + v_2 {}^2\$^2 = {}^0V_O^m \quad (14)$$

Where $v_1 = v_2 = 0$ provided that these joint-rates are associated to virtual prismatic pairs. The screws $\1 and $\2 are given in Plücker coordinates as follows

$${}^1\$^1 = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 1 \\ 0 \\ 0 \end{bmatrix}, {}^2\$^2 = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 1 \end{bmatrix}$$

After, Eq. (14) may be rewritten in a compact form as follows

$$J_q \dot{Q} = J_x {}^0V_O^m \quad (15)$$

Where $J_q = [{}^0\$^j \quad {}^j\$^k \quad {}^k\$^m \quad {}^k\bar{\$}^m \quad {}^1\$^1 \quad {}^2\$^2]$ is called the screw-coordinate Jacobian matrix of the manipulator while J_x is the identity matrix of order 6. Furthermore vector $\dot{Q} = [\dot{\theta} \quad \dot{\phi} \quad \dot{\beta} \quad \dot{l} \quad v_1 \quad v_2]^T$ is named the first-order driver of the robot. Equation (15) is called the input-output equation of velocity of the manipulator.

The forward velocity analysis consists of finding the velocity state ${}^0V_O^m$ given a set of generalized speeds $\{\dot{\theta} \quad \dot{\phi} \quad \dot{\beta} \quad \dot{l}\}$. It is evident that this analysis is free of singularities since $\det(J_x) = 1$ for any posture of the mechanism. On the other hand, the inverse velocity analysis of the manipulator consists of finding the generalized speeds given the six-dimensional vector ${}^0V_O^m$. Unlike, the forward velocity analysis, the inverse velocity analysis is not free of singular

configurations. In fact, taking into account that $\det(J_q) = -\sin(\phi) \cos(\phi)$, the manipulator falls into a singularity when $\sin(\phi) \cos(\phi) = 0$, e.g. when $\phi = 0$ or $\phi = \pi/2$. It is worth to note that the generalized coordinate θ is not responsible to fall-escape the manipulator from singular postures, if the manipulator confirms, as concluded by Waldron et al (1985), that in a serial manipulator the kinematic pair connecting the open chain to the base link is not responsible of the feasible singularities of the serial manipulator. On the other hand, it is evident that the manipulator at hand cannot perform arbitrary velocity states owing the loss freedoms of it, consider for instance that the coordinates P_x and P_z are related through Eq. (10). Finally, according to Eq. (13) the angular velocity ${}^0\omega^m$ results in

$${}^0\omega^m = [\dot{\theta} \sin(\theta) + \dot{\beta} \sin(\phi) \cos(\theta)]\hat{i} + [\dot{\theta} + \dot{\beta} \cos(\phi)]\hat{j} + [\dot{\phi} \cos(\theta) - \dot{\beta} \sin(\phi) \sin(\theta)]\hat{k} \quad (16)$$

While the velocity vector ${}^0v_O^m$ is obtained as

$${}^0v_O^m = \dot{l} \sin(\phi) \cos(\theta) \hat{i} + \dot{l} \cos(\phi) \hat{j} - \dot{l} \sin(\phi) \sin(\theta) \hat{k} \quad (16)$$

Furthermore, using elementary kinematics the velocity of point P is computed as

$${}^0v_P^m = {}^0v_O^m + {}^0\omega^m \times r_{P/O} \quad (17)$$

where $r_{P/O}$ is a vector pointed from point O to point P . Hence one obtains

$${}^0v_P^m = [-\dot{\theta} \sin(\phi) \sin(\theta) - \dot{\phi} \cos(\theta) \cos(\phi) + \dot{l} \sin(\phi) \cos(\theta)]\hat{i} + [\dot{\theta} \sin(\phi) + \dot{l} \cos(\phi)]\hat{j} + [-\dot{\theta} \sin(\phi) \cos(\theta) + \dot{\phi} \sin(\theta) \cos(\phi) - \dot{l} \sin(\phi) \sin(\theta)]\hat{k} \quad (18)$$

Equations (17) and (18) indicate that given the velocity state of the end-effector, taking point P as the reference pole, there are six equations available to compute the four generalized speeds of the robot. The limitations of mobility of the manipulator are evident owing the dependency between such equations. In fact the end-effector of the robot cannot undergo arbitrary velocity states. For example, concerned with the velocity of point P the architecture of the manipulator is such, see Eq. (10), that $\hat{w} \cdot r_{P/O} = 0$. Hence upon the time derivative of such constraint it follows that Eq. (18) is restricted to satisfy the expression $v_x \cos \theta = v_z \sin \theta$. The available motions of the antenna may be easily explained if one consider that the orientation of the antenna is controlled by means of the three independent angles θ , ϕ and β and therefore the knob can adopt arbitrary orientations as observed from the base link while, according to the limitations of the manipulator, only one translation of point P can be selected freely.

Acceleration Analysis of the Serial Manipulator

Let ${}^0a^m$ be the angular acceleration vector of the end-effector m as measured from the base link 0 and let ${}^0a_O^m$ be the acceleration of a point of the body m which is instantaneously coincident with the origin of the reference frame XYZ . According to Eq. (6), the reduced acceleration state of body m as measured from body 0, the vector ${}^0A_O^m$, is given in screw form as follows

$$\ddot{\theta} {}^0\$^j + \ddot{\phi} {}^j\$^k + \ddot{\beta} {}^k\$^m + \ddot{l} {}^k\bar{\$}^m + \dot{v}_1 {}^1\$^1 + \dot{v}_2 {}^2\$^2 + L = {}^0A_O^m \quad (19)$$

Where the Lie screw of acceleration, see Eq. (7), is given by

$$L = [\dot{\theta} \ 0 \ \$^j \ \dot{\phi} \ \$^k + \dot{\beta} \ \$^m + \dot{l} \ \$^{\bar{m}} + v1 \ \$^1 + v2 \ \$^2] + [\dot{\phi} \ \$^k \ \dot{\beta} \ \$^m + \dot{l} \ \$^{\bar{m}} + v1 \ \$^1 + v2 \ \$^2] + [\dot{\beta} \ \$^m \ \dot{l} \ \$^{\bar{m}} + v1 \ \$^1 + v2 \ \$^2] + [\dot{l} \ \$^{\bar{m}} \ v1 \ \$^1 + v2 \ \$^2] + [v1 \ \$^1 \ v2 \ \$^2] \quad (20)$$

Furthermore, due to the fact that the joint-rate velocities $v1$ and $v2$ vanish, then the Lie screw of acceleration is reduced to

$$L = [\dot{\theta} \ 0 \ \$^j \ \dot{\phi} \ \$^k + \dot{\beta} \ \$^m + \dot{l} \ \$^{\bar{m}}] + [\dot{\phi} \ \$^k \ \dot{\beta} \ \$^m + \dot{l} \ \$^{\bar{m}}] + [\dot{\beta} \ \$^m \ \dot{l} \ \$^{\bar{m}}] \quad (21)$$

After, the input-output equation of acceleration of the manipulator may be re-written, see Eq. (19), as follows

$$J_q \ddot{Q} + L = {}^0A_O^m \quad (22)$$

where $\ddot{Q} = [\ddot{\theta} \ \ddot{\phi} \ \ddot{\beta} \ \ddot{l} \ \ddot{v}1 \ \ddot{v}2]^T$ is called the second-order driver matrix of the manipulator. Evidently it follows that $\ddot{v}1 = \ddot{v}2 = 0$ owing that these joint-rate accelerations are associated to fictitious kinematic pairs.

Once the velocity analysis of the manipulator was solved, the forward acceleration analysis of the kinematic chain consists of finding the reduced acceleration state ${}^0A_O^m$ given a set of generalized accelerations $\{\ddot{\theta} \ \ddot{\phi} \ \ddot{\beta} \ \ddot{l}\}$. On the other hand, the inverse acceleration analysis consists of finding the generalized accelerations given the six-dimensional vector ${}^0A_O^m$. Both analyses may be solved by means of Eq. (22). Furthermore, after a few computations, the primal part of the reduced acceleration state ${}^0A_O^m$ is obtained as

$${}^0a^m = P({}^jA_O^m) = [\ddot{\phi} \sin(\theta) + \ddot{\beta} \sin(\phi) \cos(\theta) + \ddot{\theta} \dot{\phi} \cos(\theta) - \ddot{\theta} \dot{\beta} \sin(\phi) \sin(\theta) - \ddot{\phi} \dot{\beta} \cos(\phi) \cos(\theta)]\hat{i} + [\ddot{\theta} + \ddot{\beta} \cos(\phi) + \ddot{\phi} \dot{\beta} \sin(\phi)]\hat{j} + [\ddot{\theta} \cos(\theta) - \ddot{\beta} \sin(\phi) \sin(\theta) - \ddot{\theta} \dot{\phi} \sin(\theta) - \ddot{\theta} \dot{\beta} \sin(\phi) \cos(\theta) + \ddot{\phi} \dot{\beta} \cos(\phi) \sin(\theta)]\hat{k} \quad (23)$$

while the corresponding dual part of the six-dimensional vector ${}^0A_O^m$ is obtained as

$$D({}^0A_O^m) = [\ddot{l} \sin(\phi) \cos(\theta) - \dot{l} \dot{\theta} \sin(\phi) \sin(\theta) - \dot{l} \dot{\phi} \cos(\phi) \cos(\theta)]\hat{i} + [\ddot{l} \cos(\phi) + \dot{l} \dot{\theta} \sin(\phi)]\hat{j} + [-\dot{l} \sin(\phi) \sin(\theta) - \dot{l} \dot{\theta} \sin(\phi) \cos(\theta) + \dot{l} \dot{\phi} \cos(\phi) \sin(\theta)]\hat{k} \quad (24)$$

Thus according to Eq. (3), the acceleration of point O fixed in body m as observed from the base link 0 is given by

$${}^0a_O^m = D({}^0A_O^m) + {}^0\omega^m \times {}^0v_O^m \quad (25)$$

Finally, using elementary kinematics the acceleration of point P , fixed in body m as observed from body 0, is calculated as

$${}^0a_P^m = {}^0a_O^m + {}^0a^m \times r_{P/O} + {}^0\omega^m \times ({}^0\omega^m \times r_{P/O}) \quad (26)$$

Numerical Example

In order to show the application of the method, in this section a case study is reported.

The first part of the example is devoted to the forward kinematics of the mechanism. To this end, using thorough the numerical example SI units, consider that in the reference configuration the generalized coordinates of the manipulator are given by $\theta = \pi/9$, $\phi = \pi/10$, $l = 0.75m$. Furthermore, consider that upon the home position of the manipulator we have a constant angular velocity $\dot{\beta} = 3$ while the generalized coordinates of the manipulator are commanded to follow periodical functions given by

$$\theta(t) = \sin(t) \cos(t), \phi(t) = \sin(t), l(t) = \sin(t)/5 \quad (27)$$

where the time t is confined to the interval $0 < t < 2\pi$. Thus in the home position of the robot when $t = 0$, the coordinates of point P are obtained as $P = (0.217, 0.713, -0.079)$. With these data it is required to determine the temporal behavior of point P . The involved equations in the solution of the forward position, velocity and acceleration analyses were translated into a Maple12 sheet. The relevant plots thus obtained are provided in Fig. 3.

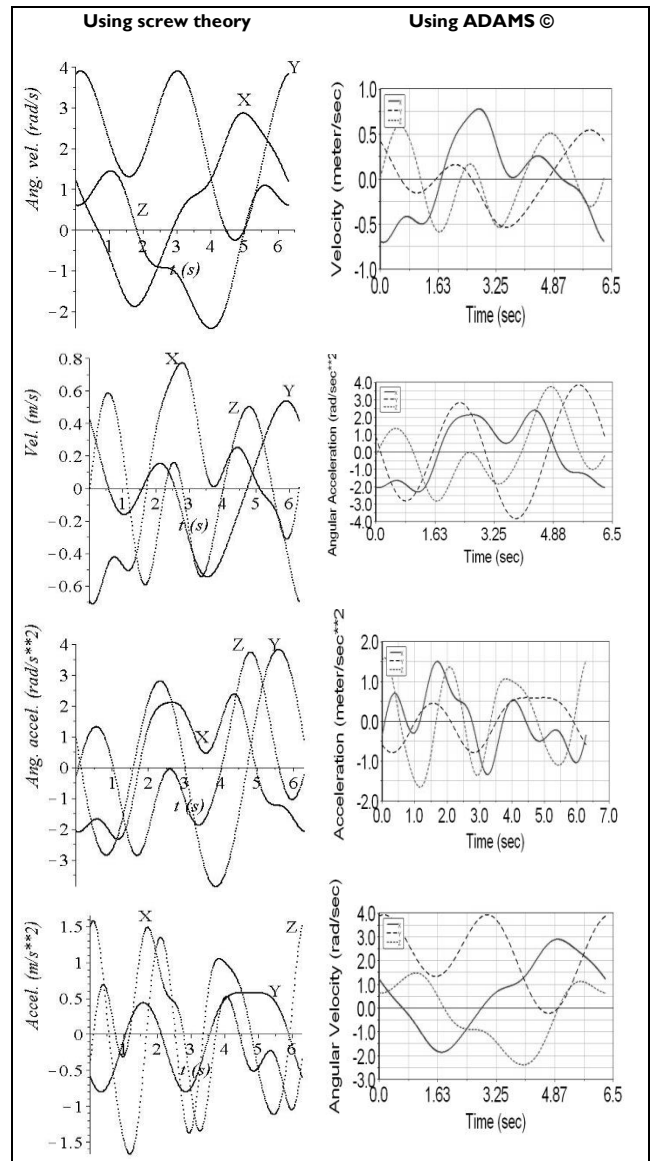


Figure 3. Time history of the forward kinematics of the knob (point P).

Furthermore, in order to verify the numerical results obtained via screw theory, the forward kinematics of the numerical example was carried-out by means of a different approach such is the application of commercially available software like ADAMS®. For a rapid comparison between both strategies the plots generated with ADAMS® were added to Fig. 3. The virtual prototype is shown in Fig. 4.

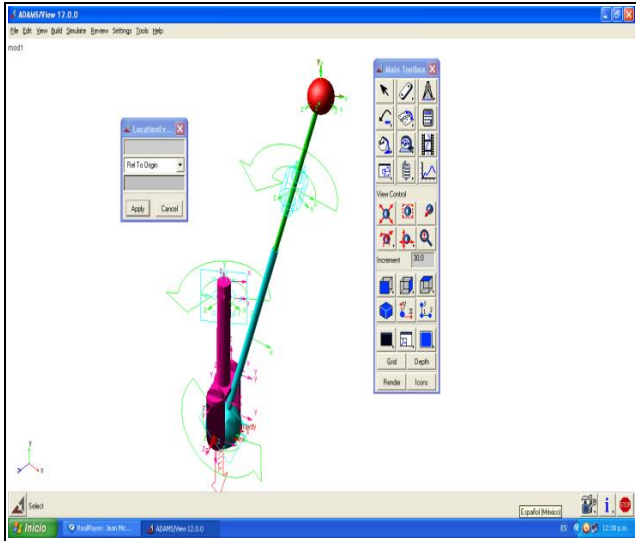


Figure 4. Virtual prototype of the manipulator realized with ADAMS®.

The next part of the exercise is dedicated to the inverse kinematics of the manipulator. To this end, it must be taken into proper account that the manipulator at hand is a limited-dof serial manipulator, i.e. the vectors contained in the velocity state are dependent vectors each other. Thus, it is necessary to select properly the task assigned to the end-effector. One feasible selection is to assume that point P can adopt arbitrary positions with respect to the base link. With these assumptions in mind it is desired that upon the home position of the antenna, i.e. when $P = (0.217, 0.713, -0.079)$, point $P = (P_x, P_y, P_z)$ is commanded to follow periodical functions given by

$$\begin{aligned} P_x &= 0.217 + 0.15 \sin(t), \quad P_y = 0.713 - 0.125 \sin(t), \quad P_z = -0.079 + 0.175 \sin(t) \end{aligned} \quad (28)$$

keeping a constant orientation of body m with respect to body k , e.g. $\beta = 0$. With these data it is required to compute the generalized coordinates, and their time derivatives, that allow the manipulator to perform the assigned task.

The extendible length l is computed directly from Eq. (8) while the angles ϕ and θ are calculated, respectively, by means of Eqs. (9) and (11). Furthermore, the generalized speeds and accelerations are obtained based on the first and second time derivatives of Eqs. (28). Figure 5 shows the plots of the obtained simulations.

In order to exemplify the mobility limitations of the manipulator concerned with the virtual prototype realized with ADAMS® the following trajectories were imposed to point P of the knob: three rotations $+P_x$, three rotations $+P_y$, three rotations $+P_z$. All the imposed trajectories were successfully performed by the manipulator. However, when additional conditions were assigned to point P , e.g. three rotations $+P_x + P_y$, the simulations with ADAMS® fail invariably.

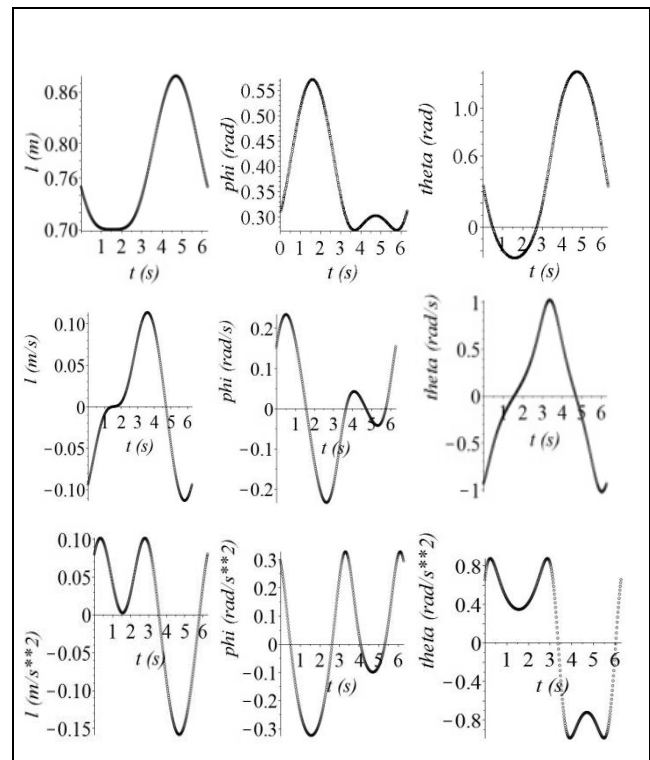


Figure 5. Time history of the inverse kinematics of the numerical example.

Conclusions

"Unfortunately, screw theory is usually explained following descriptive definitions rather than short axiomatic lines of reasoning", Minguzzi (2013).

"Screw theory allows simple geometrical interpretation, but it is restricted to speed and infinitesimal displacement analysis", Legnani et al (1996).

Comments like the above given can be found in the specialized literature. In this work, the kinematics of a four-degrees-of-freedom serial manipulator employed as an actuating mechanism for a telescoping antenna is investigated by means of the theory of screws. Simple equations in closure form are easily obtained to solve the displacement analysis of the manipulator. After, the input-output equations of velocity and acceleration are systematically obtained by resorting to the theory of screws. Numerical examples, which were successfully verified with the aid of special software like ADAMS®, are provided in order to show the application of the method. This work is a proof that screw theory is not an "old-fashioned" mathematical resource confined to the so-called first-order kinematics of rigid body.

References

- Ball, R. S. (1900). *The Theory of Screws*. Cambridge University Press.
- Brand, L. (1947). *Vector and Tensor Analysis*. John Wiley & Sons.
- Rico, J. M., & Duffy, J. (1996). An application of screw algebra to the acceleration analysis of serial chains. *Mechanism and Machine Theory*, 31(4), 445-457.
- Rico, J. M., Duffy, J., & Gallardo, J. (1999). Screw theory and higher order kinematic analysis of open serial and closed chains. *Mechanism and Machine Theory*, 34(4), 559-586.

- Gallardo-Alvarado, J. (2012). Jerk analysis of a six-degrees-of-freedom three-legged parallel manipulator. *Robotics and Computer-Integrated Manufacturing*, 28, 220-226.
- Gallardo-Alvarado, J. (2014). Hyper-jerk analysis of robot manipulators. *Journal of Intelligent and Robotic Systems*, 74(3-4), 625-641.
- Gallardo-Alvarado, J., & García-Murillo, M. A. (2013). A parallel manipulator inspired by the original Stewart platform. *Institution of Mechanical Engineers, Part C: Journal of Mechanical Engineering Science*, 227(4), 831-844.
- Gallardo, J., Lesso, R., Rico, J. M., & Alici, G. (2011). The kinematics of modular spatial hyper-redundant manipulators formed from RPS-type limbs. *Robotics and Autonomous Systems*, 59(1), 12-21.
- Gallardo-Alvarado, J., Mendoza-Orozco, H., & Rodríguez-Castro, R. (2008). Finding the jerk properties of multibody systems using helicoidal vector fields. *Institution of Mechanical Engineers, Part C: Journal of Mechanical Engineering Science*, 222(11), 2217-2229.
- Legnani, G., Casolo, F., Righettini, P., & Zappa, B. (1996). A homogeneous matrix approach to 3D kinematics and dynamics-I. *Theory, Mechanism and Machine Theory*, 31(5), 573-587.
- Minguzzi, E. (2013). A geometrical introduction to screw theory. *European Journal of Physics*, 34, 613-622.
- Sugimoto, K. (1989). Computational scheme for dynamic analysis of parallel manipulators. *ASME Journal of Mechanisms, Transmissions, and Automation in Design*, 111, 29-33.
- Sugimoto, K. (1990). Existencia criteria for overconstrained mechanisms. An extension of motor algebra. *ASME Journal of Mechanical Design*, 112(3), 295-298.
- Sugimoto, K., & Duffy, J. (1982). Application of linear algebra to screw systems. *Mechanism and Machine Theory*, 17(1), 73-83.
- Von Mises, R. (1924). Motorrechnung, ein neues hilfsmittel der mechanik. *Zeitschrift für Angewandte Mathematik und Mechanik*, 4(2), 155-181.
- Von Mises, R. (1924). Anwendungen der motorrechnung. *Zeitschrift für Angewandte Mathematik und Mechanik*, 4(3), 193-213.
- Waldron, K. J., Wang, S. L., & Bolin, S. J. (1985). A study of the Jacobian matrix of serial manipulators. *ASME Journal of Mechanisms, Transmissions, and Automation in Design*, 107(2), 230-238.