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Evaluation of the use of a vegetable oil in distribution transformers

Evaluación del uso de un aceite vegetal en transformadores de distribución

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RESUMEN

Desde los inicios de los transformadores inmersos en líquido refrigerante, el fluido empleado por tradición ha sido el aceite de origen mineral. Sin embargo, en las últimas décadas se han unido esfuerzos en la búsqueda de alternativas que tengan un menor impacto en el medio ambiente y que a su vez satisfagan los requerimientos técnicos de aislamiento y refrigeración en los transformadores. Actualmente se encuentran en el mercado aceites aislantes de origen vegetal que pueden tener un menor impacto ambiental durante su uso y disposición final; no obstante, su elevado costo y su poco tiempo de uso han limitado su aplicación masiva.

En este trabajo se presenta la evaluación del comportamiento térmico de dos transformadores de distribución de diferente potencia inmersos en aceite dieléctrico de origen vegetal y se compara su desempeño con el de dos transformadores constructivamente iguales inmersos en aceite mineral. Los resultados obtenidos revelan que los transformadores cumplen con los requerimientos de la normatividad existente.

Palabras clave: Transformadores de distribución, aceite mineral, aceite vegetal, ester natural, MEF, medición de temperatura, comportamiento térmico.

ABSTRACT

Since the start of transformers immersed in refrigerating liquid, the fluid traditionally used has been mineral oil. However, in recent decades, efforts have been joined in the search for alternatives with a lower environmental impact and which also satisfy the technical requirements of insulation and refrigeration in the transformers. Currently, insulating vegetable oils are available in the market, which may have lower environmental impact during their use and final disposition; nevertheless, their high cost and short time of use have limited their massive application.

This work presents the thermal behavior evaluation of two distribution transformers at different powers immersed in dielectric vegetable oil, comparing their performance with that of two constructively equal transformers immersed in mineral oil. The results obtained reveal that the transformers comply with the requirements of existing standards.

Keywords: Distribution transformers, mineral oil, vegetable oil, natural ester, FEM, temperature measurement, thermal behavior.

INTRODUCTION

Currently, transformers immersed in liquid mainly employ mineral oils given their proven good service performance and their relatively low cost when compared to other alternatives present in the market. However, mineral oils have certain limitations like their low flashpoint, which conditions its use in indoor environments, and its low biodegradation, which may cause a high environmental impact during its use or final disposition.

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In recent years, the environmental aspect has become important and development of clean and technically functional technologies is of high demand. With the development of vegetable oils for use in electrical equipment, an alternative appears with advantages regarding safety and the environment [1-5]. Nonetheless, many questions arise when adopting this new technology: Is it necessary to redesign the transformer? How is the final disposition of these oils handled? Are these fluids compatible with the transformer's internal materials? Are they viable from the economic point of view? In this respect, several studies have been undertaken, mainly by manufacturers of these oils and by some research institutions and universities [6-15].

In the thermal evaluation, the literature shows a higher oil temperature rise in transformers immersed in vegetable oil [2]. This higher temperature rise would suggest a lower useful lifespan than for transformers with mineral oil; however, given that paper degrades much slower in the presence of vegetable oil these transformers could have an equal or greater useful lifetime than those immersed in mineral oil [5]. The possibility exists of overloading transformers that use vegetable oil. This fact is substantiated in that under nominal load conditions these transformers have a useful life that could be longer than that for those submerged in mineral oil, which would permit overloading the transformer at a given level and maintaining the same useful life as that of a transformer submerged in mineral oil [5-9].

In Colombia, research was conducted by Universidad del Valle in association with an electric sector company, which evaluated the thermal behavior of two conventional-type distribution, single-phase transformers immersed in dielectric vegetable oil and physical, chemical, and spectral tests were conducted, as well as experiments of oil accelerated aging, designed to analyze possible changes in the structure of the oil molecules [13].

This article presents the results of the thermal evaluation of the two distribution transformers submerged in Envirotemp® FR3TM vegetable oil.

EXPERIMENTATION

This research used four single-phase distribution transformers with two different powers (15 kVA

and 37.5 kVA) constructed by Rymel Ltd. These transformers have designs normally employed in Colombia. For each power rating, there was a transformer immersed in vegetable oil and another immersed in mineral oil; these were instrumented with optical fiber sensors. The instrumentation in the distribution transformers was conducted exclusively for investigative purposes (given its high costs) and it is not widely reported in the literature [16].

Based on prior experiences by the High-Voltage Research Group (GRALTA for its name in Spanish), in the instrumentation of a distribution transformer using thermocouples, five temperature measurement zones were defined; one located above the bottom of the tank, another below the upper oil level, two on the windings (high voltage and low voltage), and one in the core. The transformers were instrumented with sensors placed in previously selected points [16] (Figure 1); all the measurements, except for that of the core, were made with optical fiber sensors. To determine the placement of the sensors, also considering the technical viability of their installation, we had the thermal profiles of the transformer obtained through simulation with the finite elements ANSYS 11 software (Figures 2 and 3).

The transformers were evaluated through temperature elevation tests via the simulated-load method (short circuit) [17]; a total of 41 tests were run. To measure temperature with the optical fiber sensors we used a Neoptix Omniflex optical fiber system, we also used a platform developed in Labview, permitting the automation and control of the tests. Measurement of electrical variables and their incorporation onto the platform was carried out with Dranetz Encore 61000 equipment.



Figure 1. Instrumented distribution transformer.

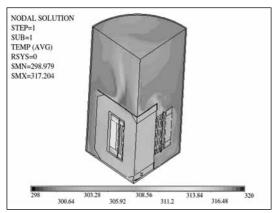


Figure 2. Thermal profiles in steady state of the 15-kVA transformer submerged in mineral oil.

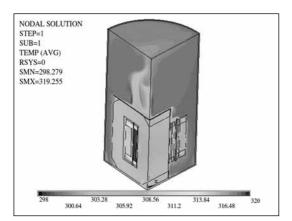


Figure 3. Thermal profiles in steady state of the 15-kVA transformer submerged in vegetable oil.

RESULTS AND DISCUSSION

The thermal behavior of the transformers evaluated in this research was conducted with respect to the temperature rise in the oil, windings, and in the hottest spot, under conditions of simulated load.

Magneto-thermal simulation via MEF

Among the main concerns at the start of the project were the temperature differences reached in the transformer under operation upon replacing mineral oil for vegetable oil because of the higher viscosity of vegetal oil. With this in mind, we conducted steady-state simulations implementing the geometry of a 15 kVA transformer. The results of the simulations are shown in Figure 2 (mineral oil) and Figure 3 (vegetable oil). It can be noted

that the maximum temperature in the mineral oil is de 317 K (44 $^{\circ}$ C) and in the vegetable oil is 319 K (46 $^{\circ}$ C), which shows a maximum temperature rise of approximately 2 $^{\circ}$ C, agreeing with that obtained experimentally.

Simulated load at constant reference Thermal behavior of oil

For the transformers evaluated, the oil temperature rise was higher in the transformers submerged in vegetable oil; however, the greatest difference was noted for the 37.5 kVA transformers where it was approximately 5 °C. Figure 4 shows the result of the oil temperature rise obtained for each of the transformers analyzed.

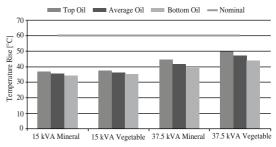


Figure 4. Oil temperature rise.

The oil temperature rise was smaller than the one specified by international standards. (60 °C) [18]. This may be explained because in Colombia big tanks are normally used to maintain the recommended electrical distances for their voltage levels; hence, they can be denominated "cold transformers". This situation would permit the use of vegetable oil without need for modifying transformer design.

Thermal behavior of the winding

The winding temperature rise was obtained by measuring winding resistance and from direct measurement by the optical fiber sensors placed in zones of interest defined by thermal simulations. Figure 5 shows the winding temperature rise in the transformers studied.

The difference between calculated values and those measured directly in the winding is because the calculation method estimates a temperature average, while the direct measurement shows a specific value. Values for the winding nominal average rise ($\Delta\theta W/A$,R) both for the transformer submerged in mineral oil as for that in vegetable

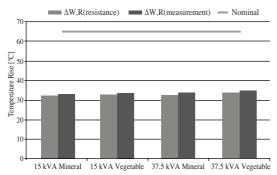


Figure 5. Nominal average winding temperature rise.

oil are below the 65 °C specified by national and international standards. However, somewhat higher temperature values are noted for the transformers submerged in vegetable oil.

Thermal behavior of the hottest spot

To estimate the hottest spot temperature rise, direct measurement may be used, whose implementation is usually not viable because of the amount of sensors required and because of their installation during the transformer manufacturing process. This investigation conducted thermal simulations by analyzing via finite elements to find higher temperature zones and then instrument the transformer during its manufacture. Figure 6 shows the record of temperatures and Figure 7 shows the hot spot temperature rise obtained from different IEC and IEEE criteria.

Values for hot-spot elevation ($\Delta\theta$ H/A,R) are below the 80 °C specified by national and international standards. Greater hot-spot elevations are found in transformers submerged in vegetable oil; however, the difference does not surpass 3 °C compared to transformers submerged in mineral oil.

Tables 1 and 2 show the results of calculating the hot-spot elevation on oil by using IEC and IEEE criteria. For IEC, we used an H=1.1 factor, for the calculation we considered the higher temperature winding (U-X). For IEEE, we calculated the temperature average of the windings and added 15 °C to this value. The value from direct measurement was obtained in the high-voltage winding.

Two-level simulated load

The thermal behavior of the transformers submerged in vegetable oil was also evaluated by using twolevel load curves characterized by a preload and an overload during a 4-hour period. The preload was

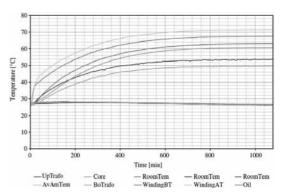


Figure 6. Temperatures recorded in a 15 kVA transformer immersed in vegetable oil, test was performed at 100% power rating.

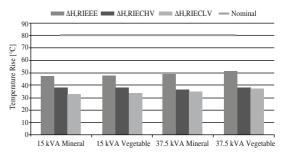


Figure 7. Nominal elevation of the hot spot per IEC and IEEE criteria.

Table 1. Calculation of the hot-spot elevation for the 15-kVA transformer.

Type of Oil	x-n	N-X	Average	$\Delta\theta_{ m H}$ IEC	$\Delta\theta_{ m H}$ IEEE	$\Delta \theta_{ m H}$ measured
Vegetable	30.7	34.1	32.4	33.8	47,4	53.6
Mineral	30.5	34.6	32.5	33.5	47.5	52.3

Table 2. Calculation of the hot-spot elevation for the 37.5-kVA transformer.

Type of Oil	x-n	X-n	Average	$\Delta\theta_{ m H}$ IEC	$\Delta \theta_{ m H}$ IEEE	$\Delta \theta_{ m H}$ measured
Vegetable	34.2	38.4	36.3	37.6	51.3	60.0
Mineral	31.7	36.6	34.1	34.8	49.1	53.8

conducted at 70% and the overload at 125% of the power rating. In these experiments, we observed the thermal behavior in the upper part of the oil and in the high-voltage winding because these

zones presented the greatest temperature rises in experiments of simulated load at constant reference. Figures 8 and 9 show the evolution of temperature in a 37.5-kVA transformer submerged in vegetable oil and mineral oil.

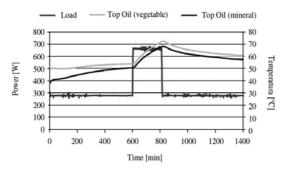


Figure 8. Thermal behavior of the upper level of oil in the 37.5-kVA transformers for two-level load.

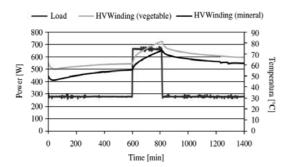


Figure 9. Thermal behavior in the high-voltage winding in the 37.5-kVA transformers for a two-level load.

Upon ending the overload, a maximum 72 °C temperature value is present in the upper level of the oil and of 81 °C in the winding for the transformer submerged in vegetable oil. It was noted the measured temperature data are higher for the transformer submerged in vegetable oil. A difference of 4 °C was noticed between maximum temperature values in oil and of 8 °C for the windings. These results show that the temperature rise is greatest in the transformers submerged in vegetable oil. In spite of that, the temperature rises are within the nominal values suggested by national and international standards

Notwithstanding, to corroborate the normal operation from the dielectric point of view, it is necessary to revise the design of transformers, given that the physical, chemical, and dielectric properties of vegetable oil are different. The difference in the electric constants of the mineral and vegetable oils lead to the electric field distributions not being the same and perhaps the minimum distances required for their normal operation are not fulfilled.

CONCLUSIONS

Distribution transformers immersed in vegetable oil presented greater temperature rises compared to those immersed in mineral oil. The greatest temperature difference does not surpass 10%. In spite of that, the temperature rises are within the nominal values suggested by national and international standards, therefore may be stated that the distribution transformers evaluated do not present inconveniences from the thermal point of view.

The results obtained are valid for the transformers tested; hence, it possible to have different results in other designs. Nevertheless, the distribution transformers tested may be considered as typical in Colombia for being "cold transformers".

We recommend submitting of transformers to dielectric tests like impulse voltage, applied voltage, and induced voltage.

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